

NATIONAL RADIO ASTRONOMY OBSERVATORY
COMPUTER DIVISION
INTERNAL REPORT

DOPSET:

A Computer Program to Calculate Doppler-Corrected Reference
Frequencies for Spectral Line and Pulsar Observations

by

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I. INTRODUCTION

Observations of spectral lines and pulsars require corrections for the motion of the telescope with respect to the source. Generally, we reference these velocities to the Local Standard of Rest for line observations and to the Solar System Barycentre for pulsar observations. This program, written in Fortran IV for an IBM 360 computer, computes the relevant velocities and frequencies using an input and output format convenient for most radio astronomical applications. It employs subroutines written by J. A. Ball (Lincoln Laboratory, Tech. Note 1969-42) to precess coordinates to the date of observation and to compute the velocity of the telescope with respect to the relevant rest frame.

For spectral line observations, up to four local oscillator settings for different rest frequencies and/or velocity offsets may be calculated at one time. For pulsars, the apparent pulsar period and a related timing frequency--used when synchronizing equipment to the pulsar--are calculated, along with as many as two LO settings for associated spectral line observations such as observations of hydrogen line absorption against pulsars. The program permits uniform variation of the pulsar rest period with time.

The following sections describe the input and output formats of the program and discuss the accuracy of the calculated velocities. An abridged set of instructions is printed on the first page of output each time the program is run (see page 10).

II. INPUT

Data input is organized as data sets, one data set being required for each source. In general, data which does not change from one source

to the next, such as telescope coordinates, need not be re-entered with each data set. However, if part of the data on a given card is to be changed, all of the data on that card must be re-entered. Many parameters are preset within the program. For instance, site coordinates are preset for the NRAO 140-foot telescope, and local time calculated is the U.S. Eastern Standard Time. These preset quantities may be readily changed to suit other observatories.

Each data set must start with a Source card containing the source name, coordinates and epoch of the coordinates. Subsequent input cards are identified by a letter in the first column:

S	:	Site card
L	:	Spectral line card
P	:	Pulsar card
D	:	Day card
Y	:	Year card
E	:	End card

The first data set must contain at least a D card and either an L card or a P card. Up to four L cards may be entered in a data set, unless a P card is entered when up to two L cards may be entered. Every data set must end with an E card. Cards between the source card and the E card may be in any order.

Input format for the first card is 5A4, 3F20.0, and for all subsequent cards A1, 1X, F18.0, 3F20.0. Note that all input numbers are assumed to be floating point, and decimal points must be entered unless the numbers are right justified. Input format for coordinates is HHMMSS.SS... or -DDMMSS.SS... for hours, minutes and seconds and degrees, minutes and seconds, respectively, with no spaces. Leading zeros may be omitted.

Detailed descriptions of the input data for each card are now given.

Source Card

Input data: Source name

Right ascension (hours, minutes, seconds)

Declination (degrees, minutes, seconds)

Epoch for coordinates (years)

The source name may have up to twenty characters. If the epoch is an integer number (e.g., 1960.0) the coordinates are assumed to refer to the mean place at the epoch given. If the epoch is not an integer (e.g., 1969.8, 1960.000001) the coordinates are assumed to refer to the apparent place at the epoch given. If the epoch is omitted (i.e., left blank) 1950.0 is assumed.

Site Card

Input data: Geodetic longitude (degrees, minutes, seconds)

Geodetic latitude (degrees, minutes, seconds)

Geodetic elevation above M.S.L. (m)

If a site card is not entered the coordinates of the NRAO 140-foot telescope are taken. To preset the program for a different telescope, the coordinates on card 502 and the elevation on card 194 should be altered.

Spectral Line Card

Input data: Rest frequency

Velocity offset from LSR, V_{off} (km/s)

Intermediate frequency

LO multiplier

The local oscillator reference frequency (LORF) is calculated assuming the Doppler-shifted line frequency f seen at the telescope is

$$f \equiv f_o \left(1 - \frac{v}{c}\right) = M \cdot \text{LORF} + f_{\text{IF}}$$

or

$$\text{LORF} = [f_o \left(1 - \frac{v}{c}\right) - f_{\text{IF}}]/M$$

where

f_o = rest frequency

v = velocity of source with respect to the telescope

f_{IF} = intermediate frequency

M = LO multiplier

The rest frequency and intermediate frequency must be entered in the same units and be such that the output frequency has sufficient significant digits. For example, for rest frequencies of 1-2 GHz, the rest frequency and intermediate frequency are generally entered in kHz. The intermediate frequency is positive when the signal frequency is above the LO.

The source velocity offset, V_{off} , is with respect to the local standard of rest (velocity of sun with respect to LSR is 20 km/s toward $18^{\text{h}}, +30^{\circ}$ (1900.0)).

If none of the L cards entered for a given source are changed for the next source, they need not be re-entered. However, if any changes are required then all L cards must be re-entered.

Pulsar Card

Input data: Period (sec)

 First derivative of period (sec/sec 10^{-15})

 Julian day to which period is referenced

 Timing factor

The period should be referred to the solar system barycentre; however for most applications the heliocentric period is adequate. The program computes the velocity of the telescope with respect to the heliocentre--planetary effects are not included. This is discussed further in the section on accuracy.

If no rate of change of period has been measured, enter zero for the first derivative and a reasonable value (say 2,440,000.0) for the Julian date.

The output timing frequency is calculated using

$$f_{\text{timing}} = \frac{F}{P_{\text{apparent}}}$$

where

F = timing factor

P_{apparent} = pulsar apparent period at the telescope.

To calculate P_{apparent} , the rest period of the pulsar at the time of observation is first calculated and then modified by the Doppler factor.

If a pulsar source precedes a spectral line source in the input deck, then at least one L card must be entered with the line source, otherwise it will be assumed to be a pulsar.

Day Card

Input data: Start day (EST)

End day (EST)

Minute step (min)

Hour angle range (hr)

A day card must be entered with the first source. The start and end days delimit the range for which calculations are made and are given

as day numbers (e.g., 193.5, 368.0) in Eastern Standard time. The time zone (5 hr W) is set on card 184 and may be changed if necessary. Day numbers entered may be negative or greater than 365 (366) to allow for calculations extending through New Year.

The minute step is the interval between times at which frequencies are calculated. If it is not entered (i.e., the field left blank) the preset value of 30.0 minutes is assumed. This preset value may be altered on card 752.

The hour angle range gives the interval on either side of transit for which frequencies are calculated. If it is not entered, frequencies are calculated when the source is above the horizon and when the hour angle is less than seven hours (as for the NRAO 140-foot telescope). The hour angle limit can be changed on card 182. If a zenith angle limit other than 90° is required it can be changed on card 178. If the hour angle range is entered on the D card the hour angle and zenith angle limits are over-ridden and negative elevation angles can be obtained.

Year Card

Data Input: Year, e.g., 1971.0

The year is preset on card 192 to 1970. If the preset year is required, no year card need be entered.

End Card

Data Input: No data

Each data set (i.e., source) must end with an E card.

III. OUTPUT

The output is grouped according to source and has one page of output per transit. Asterisks are printed on the page fold to mark each new source. A header page for each source lists all input or preset data, the LSR offset in frequency units and the precessed coordinates. For each transit the source name, precessed coordinates, rest frequencies, LSR and heliocentric velocity offsets, Eastern Standard day, date and UT day number for the first line of calculations are printed at the head of the page. For pulsars, the heliocentric period at transit and the corresponding Julian day are also listed.

Each line of printout gives the local sidereal time, Eastern Standard time, Universal time, hour angle (east and west), local oscillator reference frequencies for rest frequencies 1-4, telescope azimuth and elevation and velocity of the LSR with respect to the telescope. For pulsars, local oscillator columns 3 and 4 are replaced by the timing frequency and apparent pulsar period respectively. Unused columns are filled with asterisks.

Calculations are performed at rounded Universal times. When the Eastern Standard day changes, a new day and date line is printed, and if more than one page of printout is obtained per transit a space is left at the page fold.

IV. ACCURACY

The basic subroutine used in this program--DOP, written by J. A. Ball--computes the velocity of the telescope with respect to the heliocentre and the sun's motion with respect to the LSR, both projected on the source direction. This subroutine requires no change from year to year.

Its accuracy has been checked by comparing results with those calculated from a solar system ephemeris tape generated by Lincoln Laboratory of the Massachusetts Institute of Technology (kindly provided by Dr. I. I. Shapiro). Velocities given on the ephemeris tape are normally used for planetary radar observations and are much more accurate than those calculated by the subroutine. Comparison of velocities calculated for a source near the ecliptic for a wide range of days in 1970, 1971 and 1974 showed that the heliocentric velocity calculated by DOP has a maximum error of about 0.005 km/s.

Strictly, both spectral line and pulsar Doppler shift calculations should be referred to the solar system barycentre rather than the heliocentre. (Most spectral line velocities are additionally corrected to the LSR.) Data from the ephemeris tape for the same years as above showed that the maximum difference between velocities referred to the heliocentre and those referred to the barycentre was about 0.010 km/s. This therefore is the major error in the program. It is however only varying on a time scale of the order of years.

V. AVAILABILITY

The program is written in Fortran VI language for an IBM 360/50 computer. Copies of the listing, source deck or compiled deck may be obtained from either author. The compiled program is stored on disk at NRAO. See the NRAO standard write-up for details.

VI. SAMPLE INPUT AND OUTPUT

The following pages list two typical input data sets (1 line source and 1 pulsar), and some of the program output for those sets.

INPUT

G43.2+0.0 (W49 OH)	190751.8	090053.0	
D 127.	137.	10.	
L 1665401.	18.	150000.	6.
L 1667358.	18.	150000.	6.
L 1667358.	10.	150000.	6.
E			
0329+54	032911.08	542438.3	
P 0.71451855076	2.061	2440105.2292	818600.
S 795054.53	382545.48	798.5	
L 1665401.	20.	150000.	6.
D 127.	137.	20.	2.
E			

OUTPUT

```

INPUT CARD FORMATS FOR DCPSET ARE AS FOLLOWS:
SOURCE,RA,DEC,EPOCH
S, LONG, LAT, ELEV
L, RESTFQ, VELOFF, FREQIF, FREQMF
P, PERIOD, PDRV, ORIGIN, PULMF
D, STRIDY, ENDDY, MINSTP, DELHA
Y, NYR
E

THE ABOVE DATA CARD SET MUST BEGIN WITH A SOURCE CARD AND END
WITH AN E-CARD. EACH DATA SFT MAY HAVE AS MANY AS 4 L-CARDS AND NO P-CARDS,
OR 1 P-CARD AND AS MANY AS 2 L-CARDS. OUTPUT COLUMNS NOT REQUIRED WILL BE FILLED WITH ASTERISKS.

INPUT PARAMETERS ARE DEFINED AS FOLLOWS:
SOURCE
SOURCE NAME
RA
RIGHT ASCENSION(HHMMSS.S...)
DEC
DECLINATION(DDMMSS.S...)
EPOCH
EPOCH OF ABOVE(XXX.X...)
S
CODE FOR SITE CARD
LONG
SITE WEST LONGITUDE(DDMMSS.S.)
LAT
SITE LATITUDE(DDMMSS.S...)
ELEV
SITE ELEVATION IN METERS
L
CODE FOR LINE CARD
RESTFQ
LINE REST FREQUENCY
VELOFF
COPELER SHIFT FROM LSR(KM/S)
FREQIF
IF FREQUENCY AFTER MIXING ( + WHEN LO IS LESS THAN SIGNAL FREQUENCY)
FREQMF
LC FREQ=FREQMF*LORF
LORF= LOCAL OSCILLATOR REFERENCE FREQUENCY
P
CODE FOR PULSAR CARD
PERIOD
PULSAR PERIOD IN SECONDS
PDRV
FIRST DERIVATIVE OF PERIOD ( IN UNITS OF 10**-15 SEC/SEC)
ORIGIN
PERIOD EPOCH (JULIAN DAYS)
PULMF
MULT. FACTOR FOR TIMING PULSE
D
CODE FOR DATE CARD
STRIDY
FIRST OBSERVING DAY, EST
ENDDY
LAST OBSERVING DAY, EST
MINSTP
INTERVAL(MINUTES) BETWEEN CALC.
DELHA
HOUR ANGLE RANGE IN HOURS
Y
CODE FOR YEAR CARD
NYR
CURRENT YEAR FOR CALCULATIONS
E
CODE FOR END OF DATA SET

```

THE PROGRAM COMPUTES LORF ACCORDING TO THE FORMULA:

$$LORF = (RESTFQ * (1. - VELCFF/C) - FRFQIF) / FREQMF$$

THE PULSAR CALCULATIONS FLATE THE TIMING FREQUENCY TO THE PULSAR
MULTIPLYING FACTOR AND DOPPLER SHIFTED PERIOD BY:

$$PULFQ = PULMF / DOPPRC$$

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*****
*      WRITTEN BY R. N. MANCHESTER AND M. A. GORDON
*      JANUARY 1970
*      SUBROUTINES DOP, COORC, MOVE, JULDA BY J. A. RALL
*****

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DOPSET
FCR

LINE SOURCE G43.2+0.0 (W49 OH)

COORDINATES	RIGHT ASCENSION			DECLINATION			EPOCH
	H	M	S	D	M	S	
GIVEN	19	7	51.800	9	0	53.000	1950.00
PRECESSED	19	8	51.336	9	2	36.746	1970.36

LINE	RESTFREQUENCY	LSR VELOCITY OFFSET KM/S	LSR FREQUENCY OFFSET	MULTIPLIER	IF
1	1665401.0000	18.000	-99.9931	6.00	150000.00
2	1667358.0000	18.000	-100.1106	6.00	150000.00
3	1667358.0000	10.000	-55.6170	6.00	150000.00

UT STARTDAY = 127.21

ENDDAY = 137.21

MINUTE INTERVAL = 10

HOURLY ANGLE RANGE = 6.48 HOURS

TELESCOPE LONGITUDE = 79 50 9.470

LATITUDE = 38 26 15.540

ELEVATION = 816.80 METERS

RA	15	8	51.191	DEC	9	2	36.025	EPOCH	1970.35
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EASTERN STANDARD DAY WEDNESDAY 6 MAY 1970 UT DAY NUMBER 127

EASTERN STANARD CAY	THURSDAY	7 MAY	1970	LT DAY NUMBER	127
---------------------	----------	-------	------	---------------	-----

9	14	39	14	39	0	0	0	5	0	0	E	4	29	41	252588.2061	252514.3979	252521.8135	*****	97.04	23.25	-41.08442
11	14	49	11	49	0	10	0	5	10	0	E	4	19	39	252588.1990	252514.3908	252521.8064	*****	98.72	25.19	-41.0765
12	14	59	12	59	0	20	0	5	20	0	E	4	9	38	252588.1913	252514.3831	252521.7987	*****	100.44	27.13	-41.0682
14	15	9	14	59	0	30	0	5	30	0	E	3	59	36	252588.1831	252514.3748	252521.7904	*****	102.20	29.05	-41.0593
16	15	19	16	59	0	40	0	5	40	0	E	3	49	34	252588.1743	252514.3660	252521.7816	*****	104.02	30.97	-41.0499
17	15	29	17	59	0	50	0	5	50	0	E	3	39	32	252588.1650	252514.3567	252521.7723	*****	105.89	32.86	-41.0398
19	15	39	19	59	1	0	0	6	0	0	E	3	29	31	252588.1551	252514.3469	252521.7625	*****	107.83	34.74	-41.0292
21	15	49	21	59	1	10	0	6	10	0	E	3	19	30	252588.1448	252514.3365	252521.7521	*****	109.85	36.60	-41.0180
22	15	59	22	59	1	20	0	6	20	0	E	3	9	28	252588.1340	252514.3257	252521.7413	*****	111.94	38.44	-41.0063
24	16	9	24	59	1	30	0	6	30	0	E	2	59	26	252588.1227	252514.3144	252521.7300	*****	114.13	40.24	-40.9941
26	16	19	26	59	1	40	0	6	40	0	E	2	49	25	252588.1109	252514.3026	252521.7182	*****	116.42	42.02	-40.9814
27	16	29	27	59	1	50	0	6	50	0	E	2	39	23	252588.0988	252514.2904	252521.7060	*****	118.82	43.76	-40.9683
29	16	39	29	59	2	0	0	7	0	0	E	2	29	21	252588.0862	252514.2778	252521.6934	*****	121.35	45.46	-40.9547
31	16	49	31	59	2	10	0	7	10	0	E	2	19	20	252588.0732	252514.2648	252521.6804	*****	124.02	47.11	-40.9407
32	16	59	32	59	2	20	0	7	20	0	E	2	9	18	252588.0599	252514.2515	252521.6671	*****	126.84	48.71	-40.9263
34	17	9	34	59	2	30	0	7	30	0	E	1	59	16	252588.0462	252514.2378	252521.6534	*****	129.82	50.25	-40.9115
35	17	19	35	59	2	40	0	7	40	0	E	1	49	15	252588.0322	252514.2238	252521.6394	*****	132.99	51.72	-40.8964
37	17	29	37	59	2	50	0	7	50	0	E	1	39	13	252588.0180	252514.2095	252521.6251	*****	136.34	53.12	-40.8810
39	17	39	39	59	3	0	0	8	0	0	E	1	29	11	252588.0034	252514.1950	252521.6106	*****	139.89	54.43	-40.8653
40	17	49	40	59	3	10	0	8	10	0	E	1	19	10	252587.9886	252514.1802	252521.5958	*****	143.66	55.65	-40.8493

17	59	42	3	20	0	8	20	0	E	1	9	8	252587.5736	252914.1651	252921.5807	*****	147.64	56.75	-40.8331
18	9	44	3	30	0	8	30	0	E	0	59	7	252587.9584	252914.1499	252921.5655	*****	151.83	57.74	-40.8167
18	19	45	3	40	0	8	40	0	E	0	49	5	252587.9431	252914.1346	252921.5502	*****	156.24	58.6C	-40.8001
18	29	47	3	50	0	8	50	0	E	0	39	3	252587.9276	252914.1191	252921.5347	*****	160.83	59.32	-40.7834
18	39	49	4	0	0	9	0	0	E	0	29	2	252587.9120	252914.1034	252921.5190	*****	165.60	59.89	-40.7666
18	49	50	4	10	0	9	10	0	E	0	19	0	252587.8963	252914.0878	252921.5033	*****	170.50	60.30	-40.7496
18	59	52	4	20	0	9	20	0	E	0	8	8	252587.8806	252914.0720	252921.4876	*****	175.49	60.54	-40.7326
19	9	54	4	30	0	9	30	0	W	0	1	2	252587.8649	252914.0562	252921.4718	*****	180.53	60.60	-40.7156
19	19	55	4	40	0	9	40	0	W	0	11	4	252587.8491	252914.0405	252921.4561	*****	185.56	60.50	-40.6986
19	29	57	4	50	0	9	50	0	W	0	21	6	252587.8334	252914.0247	252921.4403	*****	190.54	60.23	-40.6816
19	39	58	5	0	0	10	0	0	W	0	31	7	252587.8177	252914.0090	252921.4246	*****	195.41	59.78	-40.6647
20	0	2	5	10	0	10	10	0	W	0	41	9	252587.8021	252913.9935	252921.4091	*****	200.14	59.18	-40.6479
20	10	3	5	20	0	10	20	0	W	0	51	11	252587.7867	252913.9780	252921.3936	*****	204.7C	58.44	-40.6312
20	20	5	5	30	0	10	30	0	W	1	1	12	252587.7714	252913.9626	252921.3782	*****	209.06	57.55	-40.6146
20	30	7	5	40	0	10	40	0	W	1	11	14	252587.7562	252913.9475	252921.3631	*****	213.21	56.53	-40.5983
20	40	8	5	50	0	10	50	0	W	1	21	15	252587.7412	252913.9325	252921.3481	*****	217.15	55.40	-40.5821
20	50	10	6	0	0	11	0	0	W	1	31	17	252587.7265	252913.9177	252921.3333	*****	220.87	54.16	-40.5662
21	0	12	6	10	0	11	10	0	W	1	41	19	252587.7120	252913.9032	252921.3188	*****	224.38	52.83	-40.5505
21	10	13	6	20	0	11	20	0	W	1	51	20	252587.6978	252913.8890	252921.3046	*****	227.69	51.42	-40.5352
21	20	15	6	30	0	11	30	0	W	2	1	22	252587.6839	252913.8750	252921.2906	*****	230.81	49.93	-40.5201
21	30	17	6	40	0	11	40	0	W	2	11	24	252587.6703	252913.8614	252921.277C	*****	233.76	48.38	-40.5054
21	40	18	7	0	0	11	50	0	W	2	21	25	252587.6570	252913.8481	252921.2637	*****	236.55	46.77	-40.4911
21	50	20	7	10	0	12	0	0	W	2	31	27	252587.6441	252913.8352	252921.2508	*****	239.19	45.11	-40.4772
22	0	21	7	20	0	12	10	0	W	2	41	29	252587.6316	252913.8227	252921.2383	*****	241.69	43.40	-40.4637
22	10	23	7	30	0	12	20	0	W	2	51	30	252587.6195	252913.8106	252921.2262	*****	244.07	41.65	-40.4506
22	20	25	7	40	0	12	30	0	W	3	1	32	252587.6078	252913.7989	252921.2145	*****	246.34	39.87	-40.4380
22	30	26	7	50	0	12	40	0	W	3	11	34	252587.5966	252913.7877	252921.2033	*****	248.50	38.05	-40.4259
22	40	28	8	0	0	13	0	0	W	3	21	35	252587.5859	252913.7769	252921.1925	*****	250.58	36.21	-40.4143
22	50	30	8	10	0	13	10	0	W	3	31	37	252587.5756	252913.7667	252921.1823	*****	252.58	34.35	-40.4032
23	0	31	8	20	0	13	20	0	W	3	41	38	252587.5659	252913.7569	252921.1725	*****	254.51	32.47	-40.3927
23	10	33	8	30	0	13	30	0	W	4	1	42	252587.5567	252913.7477	252921.1633	*****	256.37	30.57	-40.3827
23	20	35	8	40	0	13	40	0	W	4	11	43	252587.5480	252913.7390	252921.1546	*****	258.17	28.65	-40.3734
23	30	36	8	50	0	13	50	0	W	4	21	45	252587.5398	252913.7308	252921.1464	*****	259.93	26.72	-40.3646
23	40	38	9	0	0	14	0	0	W	4	31	47	252587.5323	252913.7233	252921.1389	*****	261.64	24.79	-40.3564
23	50	40	9	10	0	14	10	0	W	4	41	48	252587.5253	252913.7163	252921.1319	*****	263.31	22.84	-40.3489
0	0	41	9	20	0	14	20	0	W	4	51	50	252587.5189	252913.7098	252921.1254	*****	264.95	20.89	-40.3419
0	10	43	9	30	0	14	30	0	W	5	1	52	252587.5131	252913.7040	252921.1196	*****	266.56	18.93	-40.3357
0	20	44	9	40	0	14	40	0	W	5	11	53	252587.5079	252913.6988	252921.1144	*****	268.15	16.97	-40.3301
0	30	46	9	50	0	14	50	0	W	5	21	55	252587.5033	252913.6942	252921.1098	*****	269.72	15.00	-40.3251
0	40	48	10	0	0	15	0	0	W	5	31	57	252587.4993	252913.6869	252921.1059	*****	271.27	13.04	-40.3208
0	50	49	10	10	0	15	10	0	W	5	41	58	252587.4960	252913.6842	252921.1025	*****	272.81	11.08	-40.3172
1	0	51	10	20	0	15	20	0	W	5	52	0	252587.4933	252913.6821	252921.0958	*****	274.35	9.12	-40.3143
1	10	53	10	30	0	15	30	0	W	6	2	1	252587.4912	252913.6807	252921.0977	*****	275.88	7.16	-40.3121
1	20	54	10	40	0	15	40	0	W	6	12	3	252587.4898	252913.68C7	252921.0963	*****	277.42	5.21	-40.3105
1	30	56	10	50	0	15	50	0	W	6	22	5	252587.4890	252913.6799	252921.0955	*****	278.96	3.27	-40.3096
													252587.4888	252913.6797	252921.0953	*****	280.5C	1.33	-40.3094

CCPSET
FCR

PULSAR 0329+54

COORDINATES	RIGHT ASCENSION H M S	DECLINATION D M S	EPOCH
GIVEN	3 29 11.080	54 24 38.300	1950.00
PRECESSED	3 30 41.564	54 28 53.416	1970.36

PERIOD S	FIRST DERIVATIVE (S/S).E+15	ORIGIN(JULIAN DAYS)	PULSE RATE FACTOR
C.71451855076000	2.061000	2440105.225200	818600.00

LINE	REST FREQUENCY	LSR VELOCITY OFFSET KM/S	LSR FREQUENCY OFFSET	MULTIPLIER	IF
1	1665401.0000	20.000	-111.1034	6.00	150000.00

UT STARTDAY = 127.21

ENDDAY = 137.21

MINUTE INTERVAL = 20

HOUR ANGLE RANGE = 2.00 HOURS

TELESCOPE LONGITUDE = 79 50 54.530

LATITUDE = 38 25 45.480

ELEVATION = 758.50 METERS

PULSAR 0329+54

RA 3 20 41.530 DEC 54 28 54.125 EPCH 1970.35

REST FREQUENCY LSR VELOCITY OFFSET HELICENTRIC VELOCITY OFFSET
KM/S KM/S
LINE 1 1665401.00000 20.000 19.751

TRANSIT PERIOD IS C.714518659207 SECONDS AT JULIAN DAY NUMBER 2440714.242651

EASTERN STANDARD DAY THURSDAY 7 MAY 1970 LT DAY NUMBER 127

LST	EST	LT	HA	LC	FREQUENCY 1	LC	FREQUENCY 2	TIMING	PERIOD	AZIMUTH	ELEVATION	VELOCITY
H M S	H M S	H M S	H M S					FREQUENCY	SEC	DEG	DEG	KM/S
1 20 51	10 40	C 15 40	C E 2 5 49	252541.2990	*****	*****	*****	1145636.6107	C.71453722050	43.12	62.86	7.5790
1 40 55	11 00	C 16 00	C E 1 45 46	252541.2893	*****	*****	*****	1145636.5708	C.71453724583	40.17	65.48	7.5894
2 0 58	11 20	C 16 20	C E 1 25 43	252541.2790	*****	*****	*****	1145636.5280	C.71453727253	36.11	67.91	7.6006
2 21 1	11 40	C 16 40	C E 1 5 39	252541.2680	*****	*****	*****	1145636.4828	C.71453730069	30.68	70.08	7.6124
2 41 4	12 00	C 17 00	C E 0 45 36	252541.2566	*****	*****	*****	1145636.4358	C.71453733001	23.65	71.88	7.6247
3 1 8	12 20	C 17 20	C E 0 29 33	252541.2449	*****	*****	*****	1145636.3875	C.71453736014	14.96	73.18	7.6374
3 21 11	12 40	C 17 40	C E 0 9 25	252541.2330	*****	*****	*****	1145636.3384	C.71453739078	4.97	73.87	7.6502
3 41 14	13 00	C 18 00	C E 0 10 33	252541.2211	*****	*****	*****	1145636.2890	C.71453742157	354.48	73.85	7.6632
4 1 18	13 20	C 18 20	C E 0 30 36	252541.2092	*****	*****	*****	1145636.2395	C.71453745218	344.54	73.13	7.6760
4 21 21	13 40	C 18 40	C E 0 50 39	252541.1975	*****	*****	*****	1145636.1917	C.71453748228	335.94	71.79	7.6886
4 41 24	14 00	C 19 00	C E 1 10 42	252541.1861	*****	*****	*****	1145636.1448	C.71453751154	328.99	69.97	7.7009
5 1 27	14 20	C 19 20	C E 1 30 46	252541.1752	*****	*****	*****	1145636.0957	C.71453753963	323.64	67.79	7.7127
5 21 31	14 40	C 19 40	C E 1 50 49	252541.1649	*****	*****	*****	1145636.0571	C.71453756623	319.65	65.34	7.7238

PULSAR C229+54

RA 3 30 41.537 DEC 54 28 52.947 EPCCP 1970.35

REST FREQUENCY LSR VELOCITY OFFSET HELICENTRIC VELOCITY OFFSET
KM/S KM/S
LINE 1 1665401.00000 20.000 19.791

TRANSIT PERIOD IS C.714518659385 SECONDS AT JULIAN DAY NUMBER 2440715.239560

EASTERN STANDARD DAY FRIDAY 8 MAY 1970 LT DAY NUMBER 128

LST	EST	LT	HA	LC	FREQUENCY 1	LC	FREQUENCY 2	LC	TIMING	PERIOD	AZIMUTH	ELEVATION	VELOCITY
H M S	H M S	H M S	H M S						FREQUENCY	SEC	DEG	DEG	KM/S
1 24 48	10 40	C 15 40	C 5 53	252541.6651	*****	*****	*****	*****	1145638.1215	0.71453627861	42.62	63.39	7.1835
1 44 51	11 00	C 16 00	C 5 45	252541.6553	*****	*****	*****	*****	1145638.0811	0.71453630385	39.47	65.97	7.1941
2 4 54	11 20	C 16 20	C 5 46	252541.6449	*****	*****	*****	*****	1145638.0379	0.71453633080	35.16	68.36	7.2054
2 24 58	11 40	C 16 40	C 5 43	252541.6338	*****	*****	*****	*****	1145637.9924	0.71453635916	29.43	70.46	7.2173
2 45 1	12 00	C 17 00	C 5 40	252541.6224	*****	*****	*****	*****	1145637.9452	0.71453638860	22.07	72.18	7.2297
3 5 4	12 20	C 17 20	C 5 36	252541.6107	*****	*****	*****	*****	1145637.8968	0.71453641881	13.08	73.37	7.2424
3 25 8	12 40	C 17 40	C 5 33	252541.5988	*****	*****	*****	*****	1145637.8476	0.71453644544	2.52	73.92	7.2552
3 45 11	13 00	C 18 00	C 5 29	252541.5868	*****	*****	*****	*****	1145637.7984	0.71453648017	352.45	73.76	7.2681
4 5 14	13 20	C 18 20	C 5 23	252541.5750	*****	*****	*****	*****	1145637.7495	0.71453651065	342.73	72.91	7.2809
4 25 17	13 40	C 18 40	C 5 26	252541.5634	*****	*****	*****	*****	1145637.7016	0.71453654055	334.44	71.47	7.2934
4 45 21	14 00	C 19 00	C 5 14	252541.5521	*****	*****	*****	*****	1145637.6551	0.71453656955	327.82	69.57	7.3056
5 5 24	14 20	C 19 20	C 5 13	252541.5413	*****	*****	*****	*****	1145637.6106	0.71453659731	322.76	67.32	7.3172
5 25 27	14 40	C 19 40	C 5 14	252541.5312	*****	*****	*****	*****	1145637.5685	0.71453662353	319.00	64.84	7.3282

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NATIONAL RADIO ASTRONOMY OBSERVATORY
Charlottesville, Virginia

October 26, 1972

MEMORANDUM

TO: Users of DOPSET
FROM: M. A. Gordon *MB*
SUBJECT: Correction of Errors

Don Backer (NRAO) has found two errors in DOPSET which should be corrected. Both errors have been corrected in the NRAO library program.

DOPSET has been relocated in the NRAO program library. (Simply remove the //JOBLIB card from the JCL cards of your old deck.)

Error 1:

In subroutine DOP, the radius from the earth's center to the observer has been calculated using geocentric latitude rather than the correct geodetic latitude.¹ To correct this error, move the block of cards DPST 1628, 1630, 1632, 1634, and 1636 to the position immediately following card DPST 1650. Be certain to renumber these cards sequentially after repositioning.

Error 2:

In REAL FUNCTION EUT, card DPST 1364 contains an incorrect formula to compute mean sidereal time. The correct formula should read

$$DST=0.2783295623D0+(8640184.665D0*DT+0.0929D0*DT**2)/864.D2$$

The magnitude of this error has been approximately -25 ms.

See American Ephemeris and Nautical Almanac (1972) p. 517, 518.