## NATIONAL RADIO ASTRONOMY OBSERVATORY Green Bank, West Virginia

## ELECTRONICS DIVISION INTERNAL REPORT NO. 324

# NRAO 43m Antenna Coordinates and Angular Limits (Version 4)

Glen Langston



## EDIR Memo#324

## NRAO 43m Antenna Coordinates and Angular Limits

Glen Langston  $NRAO\ Green\ Bank$  2012 September 14, version 4

#### **ABSTRACT**

This note records the measurements of the NRAO 43m Telescope coordinate location. The tracking limits are tabulated in Azimuth and Elevation limits due to the Hour Angle, Declination mounting structure. The lowest observable Elevation is tabulated for Azimuth values.

### Change Record

Revision	Date	Author	Sections/Pages Affected		
	Remarks				
1.0	2012-Sep-01	G. Langston	All		
	Initial version.				
2.0	2012-Sep-11	G. Langston	All		
	Add Mike Holstine's survey information and Rick Fisher's VLBI coordinates from the web				
3.0	2012-Sep-11	G. Langston	All		
	Clarify Coordinate definitions and add second measurement of the telescope position				
4.0	2012-Sep-14	G. Langston	Geocentric Coordinates		
	Jon Romney provided the latest VLBA correlator coordinates.				

#### 1. Background

The NRAO 43m telescope has participated in many world VLBI observations and from these observations the precise telescope coordinates have been determined. Also the physical coordinate of the telescope has been obtained from geodetic surveys. The telescope coordinates are obtained from both measurement methods.

The NRAO 43m telescope is the worlds largest equatorial mount telescope. The equatorial mount provides very good tracking capability for objects at the zenith. However the telescope has limited hour angle coverage and can not track low Elevation sources in the north.

The 43m telescope Hour Angle coverage is has different limits at different Declinations. The telescope structure is protected by limit switches that have different behaviors at different telescope Declinations.

#### 2. Geocentric Coordinates

Rick Fisher, of NRAO, documented the 140ft VLBI coordinates in the 1980s. The reference planes are the equator, the Greenwich Meridian, and the plane through the earth's axis and perpendicular to the Greenwich Meridian, call it the east-west plane. A telescope's rectangular coordinate components (x,y,z) are

X = 882880.0208m Distance from the east-west plane, Greenwich being positive x

Y = -4924482.4385m Eastward distance from the Greenwich Meridian

Z = 3944130.6438m Northward distance from the equator

Astronomical pointing of the telescope requires accurate knowledge the telescope location. The motion of the Green Bank site is relative to observations made at modified julian date EPOCH=50449 (1997 January 01), from the geodetic solutions from the Goddard Space Flight Center. The position was:

X = 882879.8868m DX/DT: -0.01380 m/yr

Y = -4924482.3042m DY/DT: 0.00020 m/yr

Z = 3944130.6915m DZ/DT: 0.00010 m/yr

The most recently available 43m coordinates were provided by Jon Romney, of NRAO, who reports the VLBA correlator uses the following coordinates. These coordinates should be used for calculations of the 43m position:

X = 882879.7266m DX/DT: -0.01487 m/yr

Y = -4924482.2950m DY/DT: 0.00057 m/yr

Z = 3944130.6925m DZ/DT: 0.00144 m/yr

The epoch for these coordinates was April 26, 2011 (MJD=54466). This date should be used for computation of 43m motion with time. The differences between coordinates may be taken as upper limits on the errors of measurement of position. These latter coordinates should be adopted for calculation of spacecraft ranges and range rates.

The correlator software includes a correction for the AXISOFF=14.9390m parameter, which is the vertical distance offset between the hour angle axis and the declination axis.

The astronomical longitude, latitude, and elevation of the telescope are -79 50' 06."365, +38 26' 12."448, and 0.88087 km, respectively. These coordinates were compared with the Geodetic survey markers near the telescope (See Fig. 1). Appendix A more historical measurements of the 43m position and includes a document containing measurements of the distance between survey markers and the telescope.

#### 3. Hour Angle Limits

The 43m drive system allows motion over the Hour Angle range -108.5 to 108.5 degrees. The drive system allows motion over the Declination range -46.9 to 88 degrees. However components of the telescope and structures near the telescope prevent telescope motion over this full range.

The hardware travel limits are set several degrees inward from the drive limits to assure the telescope can not travel at high speed through the limits. The motion is limited by contact switches that have a "hysteresis" of a few degrees. This hysteresis further prevents motion to a few degrees from the travel limits.

Table 1 lists a representative selection of Hour Angles and Declinations and the corresponding telescope Azimuths (Azimuth = 0 is North) and Elevations. The Hour Angle, Declination limits are provided by Tim Weadon.

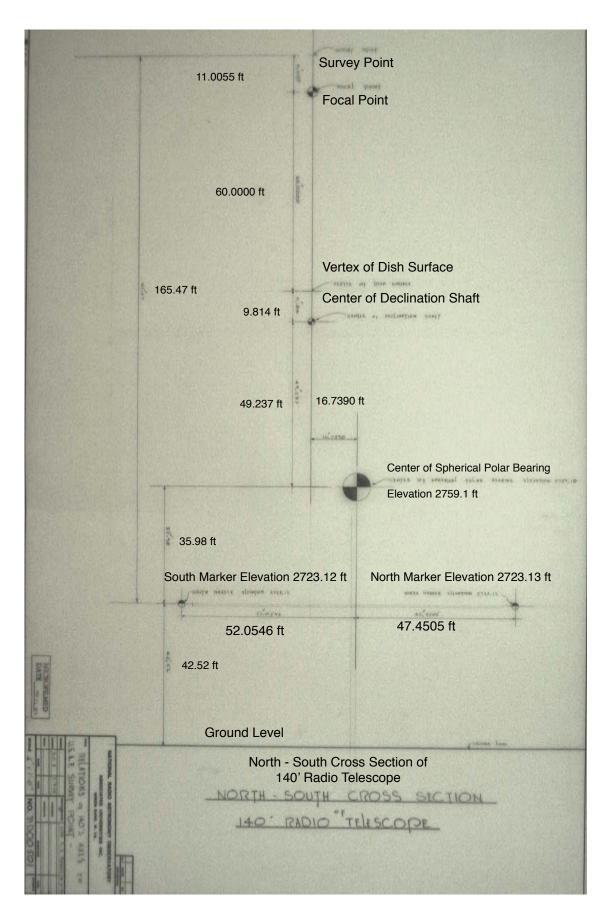


Fig. 1.— Schematic drawing of the relationship between the Geodetic markers and the Telescope hour-angle, declination axies.

#### 4. Horizon Limits

The 43m telescope sits in Deer Creek valley with the Allegheny mountains to the east and west. North and South, the visible horizon is lower.

Wes Sizemore kindly determined the horizon Elevations angles at the location of the 43m telescope based on a computer-based topographical map.

Tables 2 A,B list a representative selection of Azimuths and the Elevations at these Azimuths. The highest Elevation limits are due west of the telescope.

#### 5. Summary

The 43m telescope Azimuth and Elevation tracking limits are presented. At a sizable fraction of the telescope Azimuths, the Hour Angle, Declination limits are above the horizon.

Thanks to Wes Sizemore for his careful determination of the 43m horizon. Frank Ghigo, Mike Holstine, Jon Romney, Butch Wirt and Tim Weadon provided survey and limit measurements.

#### REFERENCES

This and all other EDIR memos are available on the web at:

http://www.gb.nrao.edu/electronics/edir

#### A. Historical measurements and Telescope Geodetic Survey Log

In the interest of completeness, we include to measures of the 43m position based on survey and VLBI measurements. Frank Ghigo provided these two measurements.

NAD 83 value from NGS data base (1993):

Designation N. Latitude W. Longitude

GREEN BANK VLBI 7204

NRAO 140 38 26 16.13751 79 50 8.79231

Height above MSL (geoid) 844.7 meters (NGVD 29)

And the following is the VLBI position converted to geodetic coordinates: VLBI position from Navy 1994-15 reference frame converted to GRS80 ellipsoid:

Designation N. Latitude W. Longitude 140-ft (VLBI): 38 26 16.161 79 50 8.799

Hour Angle	Declination	Azimuth	Elevation
(deg)	(deg)	(deg)	(deg)
-1.00	-41.01	-179.232	10.548
-10.00	-41.01	-172.353	10.030
-20.00	-41.01	-164.874	8.482
-30.00	-41.01	-157.706	5.967
-43.65	-41.01	-148.603	1.132
-43.65	-31.20	-143.245	9.367
-67.99	-31.20	-127.342	-4.068
-67.99	-11.10	-112.638	9.694
-102.55	-11.10	-91.091	-16.661
-102.55	0.00	-82.121	-9.800
-102.55	10.00	-74.364	-3.421
-102.55	20.00	-66.710	3.020
-102.55	30.00	-58.965	9.406
-102.55	40.00	-50.932	15.617
-102.55	50.00	-42.411	21.519
-102.55	60.00	-33.198	26.953
-102.55	70.00	-23.112	31.732
-102.55	82.00	-9.703	36.293
0.00	82.00	-0.000	46.437
102.30	82.00	9.717	36.326
102.30	70.00	23.156	31.809
102.30	60.00	33.270	27.061
102.30	50.00	42.509	21.651
102.30	40.00	51.053	15.769
102.30	30.00	59.104	9.574
102.30	20.00	66.861	3.200
102.30	10.00	74.522	-3.232
102.30	0.00	82.281	-9.606
102.30	-11.86	91.880	-16.922
69.20	-11.86	112.397	8.306
69.20	-20.00	118.418	2.795
69.20	-31.20	126.634	-4.825
44.70	-31.20	142.487	8.871
44.70	-41.01	147.939	0.700
30.00	-41.01	157.706	5.967
20.00	-41.01	164.874	8.482
10.00	-41.01	172.353	10.030
1.00	-41.01	179.232	10.548

Table 1: Table of Hour Angle, Declinations limits, with corresponding Azimuth and Elevations for the  $43\mathrm{m}$  Telescope.

Azimuth	Elevation
(deg)	(deg)
-177.8	1.429
-171.6	1.499
-165.7	1.273
-165.7	1.273
-163.5	1.008
-160.6	0.159
-156.5	-0.300
-156.0	-0.330
-150.4	0.071
-146.2	0.327
-140.7	-0.380
-129.8	1.808
-124.3	2.566
-112.5	4.240
-98.2	4.020
-82.8	5.040
-68.4	4.036
-56.3	2.697
-46.9	4.134
-31.8	4.360
-26.0	3.536
-19.6	1.689
-12.7	2.017
-5.30	2.351

Table 2: Table of Elevations of the Horizon as a function of the 43m Telescope Azimuth (part A).

Azimuth (deg)         Elevation (deg)           2.2         1.600           9.6         1.154           16.3         0.507           16.8         0.335           24.3         0.000           27.4         0.016           34.9         0.430           35.3         0.343           38.1         0.565           43.8         0.018           50.2         0.420           58.8         0.779           64.6         1.494           66.8         2.243           68.6         3.164           73.0         3.275           79.7         3.508           86.7         4.228           93.7         4.115           100.7         3.976           107.4         3.748           113.6         2.407           119.2         2.291           128.9         3.479           132.9         2.923           136.5         2.919           139.6         2.490           142.4         1.977           147.1         2.510           148.5         2.498           150.8		
2.2       1.600         9.6       1.154         16.3       0.507         16.8       0.335         24.3       0.000         27.4       0.016         34.9       0.430         35.3       0.343         38.1       0.565         43.8       0.018         50.2       0.420         58.8       0.779         64.6       1.494         66.8       2.243         68.6       3.164         73.0       3.275         79.7       3.508         86.7       4.228         93.7       4.115         100.7       3.976         107.4       3.748         113.6       2.407         119.2       2.291         128.9       3.479         132.9       2.923         136.5       2.919         139.6       2.490         142.4       1.977         147.1       2.510         148.5       2.498         150.8       2.530         153.3       1.970         158.4       1.630         169.9       1.	Azimuth	Elevation
9.6	,	
16.3       0.507         16.8       0.335         24.3       0.000         27.4       0.016         34.9       0.430         35.3       0.343         38.1       0.565         43.8       0.018         50.2       0.420         58.8       0.779         64.6       1.494         66.8       2.243         68.6       3.164         73.0       3.275         79.7       3.508         86.7       4.228         93.7       4.115         100.7       3.976         107.4       3.748         113.6       2.407         119.2       2.291         128.9       3.479         132.9       2.923         136.5       2.919         139.6       2.490         142.4       1.977         147.1       2.510         148.5       2.498         150.8       2.530         153.3       1.970         158.4       1.630         164.0       1.996         169.9       1.850	2.2	1.600
16.8       0.335         24.3       0.000         27.4       0.016         34.9       0.430         35.3       0.343         38.1       0.565         43.8       0.018         50.2       0.420         58.8       0.779         64.6       1.494         66.8       2.243         68.6       3.164         73.0       3.275         79.7       3.508         86.7       4.228         93.7       4.115         100.7       3.976         107.4       3.748         113.6       2.407         119.2       2.291         128.9       3.479         132.9       2.923         136.5       2.919         139.6       2.490         142.4       1.977         147.1       2.510         148.5       2.498         150.8       2.530         153.3       1.970         158.4       1.630         164.0       1.996         169.9       1.850	9.6	1.154
24.3       0.000         27.4       0.016         34.9       0.430         35.3       0.343         38.1       0.565         43.8       0.018         50.2       0.420         58.8       0.779         64.6       1.494         66.8       2.243         68.6       3.164         73.0       3.275         79.7       3.508         86.7       4.228         93.7       4.115         100.7       3.976         107.4       3.748         113.6       2.407         119.2       2.291         128.9       3.479         132.9       2.923         136.5       2.919         139.6       2.490         142.4       1.977         147.1       2.510         148.5       2.498         150.8       2.530         153.3       1.970         158.4       1.630         169.9       1.850	16.3	0.507
27.4       0.016         34.9       0.430         35.3       0.343         38.1       0.565         43.8       0.018         50.2       0.420         58.8       0.779         64.6       1.494         66.8       2.243         68.6       3.164         73.0       3.275         79.7       3.508         86.7       4.228         93.7       4.115         100.7       3.976         107.4       3.748         113.6       2.407         119.2       2.291         128.9       3.479         132.9       2.923         136.5       2.919         139.6       2.490         142.4       1.977         147.1       2.510         148.5       2.498         150.8       2.530         153.3       1.970         158.4       1.630         169.9       1.850	16.8	0.335
34.9       0.430         35.3       0.343         38.1       0.565         43.8       0.018         50.2       0.420         58.8       0.779         64.6       1.494         66.8       2.243         68.6       3.164         73.0       3.275         79.7       3.508         86.7       4.228         93.7       4.115         100.7       3.976         107.4       3.748         113.6       2.407         119.2       2.291         128.9       3.479         132.9       2.923         136.5       2.919         139.6       2.490         142.4       1.977         147.1       2.510         148.5       2.498         150.8       2.530         153.3       1.970         158.4       1.630         164.0       1.996         169.9       1.850	24.3	0.000
35.3       0.343         38.1       0.565         43.8       0.018         50.2       0.420         58.8       0.779         64.6       1.494         66.8       2.243         68.6       3.164         73.0       3.275         79.7       3.508         86.7       4.228         93.7       4.115         100.7       3.976         107.4       3.748         113.6       2.407         119.2       2.291         128.9       3.479         132.9       2.923         136.5       2.919         139.6       2.490         142.4       1.977         147.1       2.510         148.5       2.498         150.8       2.530         153.3       1.970         158.4       1.630         164.0       1.996         169.9       1.850	27.4	0.016
38.1       0.565         43.8       0.018         50.2       0.420         58.8       0.779         64.6       1.494         66.8       2.243         68.6       3.164         73.0       3.275         79.7       3.508         86.7       4.228         93.7       4.115         100.7       3.976         107.4       3.748         113.6       2.407         119.2       2.291         128.9       3.479         132.9       2.923         136.5       2.919         139.6       2.490         142.4       1.977         147.1       2.510         148.5       2.498         150.8       2.530         153.3       1.970         158.4       1.630         164.0       1.996         169.9       1.850	34.9	0.430
43.8       0.018         50.2       0.420         58.8       0.779         64.6       1.494         66.8       2.243         68.6       3.164         73.0       3.275         79.7       3.508         86.7       4.228         93.7       4.115         100.7       3.976         107.4       3.748         113.6       2.407         119.2       2.291         128.9       3.479         132.9       2.923         136.5       2.919         139.6       2.490         142.4       1.977         147.1       2.510         148.5       2.498         150.8       2.530         153.3       1.970         158.4       1.630         164.0       1.996         169.9       1.850	35.3	0.343
50.2       0.420         58.8       0.779         64.6       1.494         66.8       2.243         68.6       3.164         73.0       3.275         79.7       3.508         86.7       4.228         93.7       4.115         100.7       3.976         107.4       3.748         113.6       2.407         119.2       2.291         128.9       3.479         132.9       2.923         136.5       2.919         139.6       2.490         142.4       1.977         147.1       2.510         148.5       2.498         150.8       2.530         153.3       1.970         158.4       1.630         164.0       1.996         169.9       1.850	38.1	0.565
58.8       0.779         64.6       1.494         66.8       2.243         68.6       3.164         73.0       3.275         79.7       3.508         86.7       4.228         93.7       4.115         100.7       3.976         107.4       3.748         113.6       2.407         119.2       2.291         128.9       3.479         132.9       2.923         136.5       2.919         139.6       2.490         142.4       1.977         147.1       2.510         148.5       2.498         150.8       2.530         153.3       1.970         158.4       1.630         164.0       1.996         169.9       1.850	43.8	0.018
64.6       1.494         66.8       2.243         68.6       3.164         73.0       3.275         79.7       3.508         86.7       4.228         93.7       4.115         100.7       3.976         107.4       3.748         113.6       2.407         119.2       2.291         128.9       3.479         132.9       2.923         136.5       2.919         139.6       2.490         142.4       1.977         147.1       2.510         148.5       2.498         150.8       2.530         153.3       1.970         158.4       1.630         164.0       1.996         169.9       1.850	50.2	0.420
66.8       2.243         68.6       3.164         73.0       3.275         79.7       3.508         86.7       4.228         93.7       4.115         100.7       3.976         107.4       3.748         113.6       2.407         119.2       2.291         128.9       3.479         132.9       2.923         136.5       2.919         139.6       2.490         142.4       1.977         147.1       2.510         148.5       2.498         150.8       2.530         153.3       1.970         158.4       1.630         164.0       1.996         169.9       1.850	58.8	0.779
68.6       3.164         73.0       3.275         79.7       3.508         86.7       4.228         93.7       4.115         100.7       3.976         107.4       3.748         113.6       2.407         119.2       2.291         128.9       3.479         132.9       2.923         136.5       2.919         139.6       2.490         142.4       1.977         147.1       2.510         148.5       2.498         150.8       2.530         153.3       1.970         158.4       1.630         164.0       1.996         169.9       1.850	64.6	1.494
73.0 3.275 79.7 3.508 86.7 4.228 93.7 4.115 100.7 3.976 107.4 3.748 113.6 2.407 119.2 2.291 128.9 3.479 132.9 2.923 136.5 2.919 139.6 2.490 142.4 1.977 147.1 2.510 148.5 2.498 150.8 2.530 153.3 1.970 158.4 1.630 164.0 1.996 169.9 1.850	66.8	2.243
79.7       3.508         86.7       4.228         93.7       4.115         100.7       3.976         107.4       3.748         113.6       2.407         119.2       2.291         128.9       3.479         132.9       2.923         136.5       2.919         139.6       2.490         142.4       1.977         147.1       2.510         148.5       2.498         150.8       2.530         153.3       1.970         158.4       1.630         164.0       1.996         169.9       1.850	68.6	3.164
86.7       4.228         93.7       4.115         100.7       3.976         107.4       3.748         113.6       2.407         119.2       2.291         128.9       3.479         132.9       2.923         136.5       2.919         139.6       2.490         142.4       1.977         147.1       2.510         148.5       2.498         150.8       2.530         153.3       1.970         158.4       1.630         164.0       1.996         169.9       1.850	73.0	3.275
93.7       4.115         100.7       3.976         107.4       3.748         113.6       2.407         119.2       2.291         128.9       3.479         132.9       2.923         136.5       2.919         139.6       2.490         142.4       1.977         147.1       2.510         148.5       2.498         150.8       2.530         153.3       1.970         158.4       1.630         164.0       1.996         169.9       1.850	79.7	3.508
$\begin{array}{ccccc} 100.7 & 3.976 \\ 107.4 & 3.748 \\ 113.6 & 2.407 \\ 119.2 & 2.291 \\ 128.9 & 3.479 \\ 132.9 & 2.923 \\ 136.5 & 2.919 \\ 139.6 & 2.490 \\ 142.4 & 1.977 \\ 147.1 & 2.510 \\ 148.5 & 2.498 \\ 150.8 & 2.530 \\ 153.3 & 1.970 \\ 158.4 & 1.630 \\ 164.0 & 1.996 \\ 169.9 & 1.850 \\ \end{array}$	86.7	4.228
$\begin{array}{cccc} 107.4 & 3.748 \\ 113.6 & 2.407 \\ 119.2 & 2.291 \\ 128.9 & 3.479 \\ 132.9 & 2.923 \\ 136.5 & 2.919 \\ 139.6 & 2.490 \\ 142.4 & 1.977 \\ 147.1 & 2.510 \\ 148.5 & 2.498 \\ 150.8 & 2.530 \\ 153.3 & 1.970 \\ 158.4 & 1.630 \\ 164.0 & 1.996 \\ 169.9 & 1.850 \\ \end{array}$	93.7	4.115
113.6       2.407         119.2       2.291         128.9       3.479         132.9       2.923         136.5       2.919         139.6       2.490         142.4       1.977         147.1       2.510         148.5       2.498         150.8       2.530         153.3       1.970         158.4       1.630         164.0       1.996         169.9       1.850	100.7	3.976
119.2       2.291         128.9       3.479         132.9       2.923         136.5       2.919         139.6       2.490         142.4       1.977         147.1       2.510         148.5       2.498         150.8       2.530         153.3       1.970         158.4       1.630         164.0       1.996         169.9       1.850	107.4	3.748
128.9       3.479         132.9       2.923         136.5       2.919         139.6       2.490         142.4       1.977         147.1       2.510         148.5       2.498         150.8       2.530         153.3       1.970         158.4       1.630         164.0       1.996         169.9       1.850	113.6	2.407
132.9       2.923         136.5       2.919         139.6       2.490         142.4       1.977         147.1       2.510         148.5       2.498         150.8       2.530         153.3       1.970         158.4       1.630         164.0       1.996         169.9       1.850	119.2	2.291
136.5       2.919         139.6       2.490         142.4       1.977         147.1       2.510         148.5       2.498         150.8       2.530         153.3       1.970         158.4       1.630         164.0       1.996         169.9       1.850	128.9	3.479
139.6       2.490         142.4       1.977         147.1       2.510         148.5       2.498         150.8       2.530         153.3       1.970         158.4       1.630         164.0       1.996         169.9       1.850	132.9	2.923
$\begin{array}{cccc} 142.4 & 1.977 \\ 147.1 & 2.510 \\ 148.5 & 2.498 \\ 150.8 & 2.530 \\ 153.3 & 1.970 \\ 158.4 & 1.630 \\ 164.0 & 1.996 \\ 169.9 & 1.850 \\ \end{array}$	136.5	2.919
147.12.510148.52.498150.82.530153.31.970158.41.630164.01.996169.91.850	139.6	2.490
148.5       2.498         150.8       2.530         153.3       1.970         158.4       1.630         164.0       1.996         169.9       1.850	142.4	1.977
150.8       2.530         153.3       1.970         158.4       1.630         164.0       1.996         169.9       1.850	147.1	2.510
153.31.970158.41.630164.01.996169.91.850	148.5	2.498
158.4 1.630 164.0 1.996 169.9 1.850	150.8	2.530
164.0 1.996 169.9 1.850	153.3	1.970
169.9 1.850	158.4	1.630
	164.0	1.996
176.0 1.615	169.9	1.850
	176.0	1.615

Table 3: Table of Elevations of the Horizon as a function of the 43m Telescope Azimuth (part B).

### 43M / 140FT LIMITS

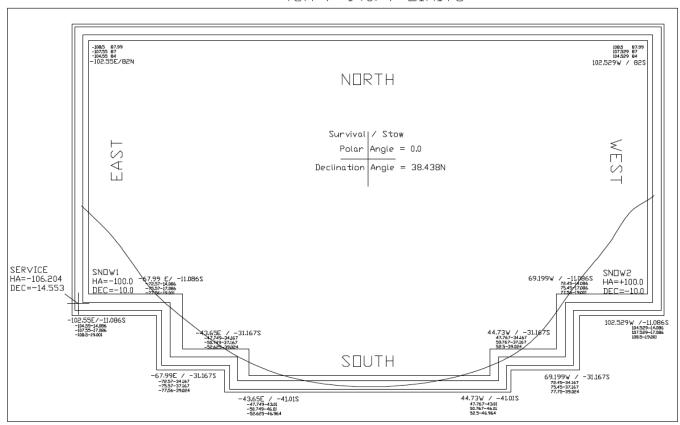


Fig. 2.— Hour Angle, Declination Limits.

## 43m Azimuth, Elevation Limits Ha,Dec Limits Horizon Limits 80 60 Elevation (deg) 40 20 0 -150 -100 -50 0 50 100 150 West Azimuth (deg) East

Fig. 3.— Azimuth-Elevation Limits due to Hour Angle, Declination Constraints (Red) and Horizon constraints (Green). For an astronomical object to be visible at a specified azimuth and elevation, the coordinate must be above both the red and green curves. North is at Azimuth = 0, and South is at Azimuth = 180.

Height: 812.62 meters.

Scot Ransom's presto database of telescopes has geodetic (not geocentric) coordinates:

Designation N. Latitude W. Longitude GB 140FT 38 26 15.409 79 50 9.613

Height: 880.87

1 National Geodetic Survey, Retrieval Date = JANUARY 5, 1998

HW3239 DESIGNATION - GREEN BANK VLBI 7204 NRAO 140

HW3239 PID - HW3239

HW3239 STATE/COUNTY- WV/POCAHONTAS

HW3239 USGS QUAD - GREEN BANK (1979)

HW3239

HW3239

HW3239 \*CURRENT SURVEY CONTROL

HW3239 \_\_\_\_\_

HW3239\* NAD 83(1995)- 38 26 16.13756(N) 079 50 08.79264(W) ADJUSTED

HW3239\* NAVD 88 - 844.7 (meters) 2771. (feet) VERTCON

HW3239 X - 882,880.434 (meters) COMP

HW3239 Y - -4,924,483.834 (meters) COMP

HW3239 Z - 3,944,130.882 (meters) COMP

HW3239 LAPLACE CORR- -0.95 (seconds) DEFLEC96

HW3239 ELLIP HEIGHT- 813.90 (meters) GPS OBS

HW3239 GEOID HEIGHT- -30.62 (meters) GEOID96

HW3239

HW3239 HORZ ORDER - A

HW3239 ELLP ORDER - FIRST CLASS I

HW3239

HW3239.The horizontal coordinates were established by VLBI observations

HW3239.and local terrestrial surveys and adjusted by the National Geodetic

HW3239.Survey in April 1992.

HW3239. This is a SPECIAL STATUS position. See SPECIAL STATUS under the

HW3239.DATUM ITEM on the data sheet items page.

HW3239

HW3239.The NAVD 88 height was computed by applying the VERTCON shift value to

HW3239.the NGVD 29 height (displayed under SUPERSEDED SURVEY CONTROL.)

HW3239

HW3239.The X, Y, and Z were computed from the position and the ellipsoidal ht.

HW3239

HW3239.The Laplace correction was computed from DEFLEC96 derived deflections.

HW3239

HW3239. The ellipsoidal height was determined by GPS observations

HW3239.and is referenced to NAD 83.

HW3239

HW3239. The geoid height was determined by GEOID96.

HW3239

HW3239; North East Units Scale Converg.

HW3239;SPC WV S - 160,220.769 701,636.521 MT 0.99993542 +0 43 11.0

HW3239;UTM 17 - 4,255,035.224 601,606.705 MT 0.99972714 +0 43 25.7

HW3239

HW3239 SUPERSEDED SURVEY CONTROL

HW3239

HW3239 NAD 83(1986)- 38 26 16.13751(N) 079 50 08.79231(W) ADJUSTED

HW3239 NGVD 29 - 844.7 (meters) 2771. (feet) GPS OBS

HW3239

HW3239.Superseded values are not recommended for survey control.

HW3239.NGS no longer adjusts projects to the NAD 27 or NGVD 29 datums.

HW3239.See file format.dat to determine how the superseded data were derived.

HW3239

HW3239\_STABILITY: D = MARK OF QUESTIONABLE OR UNKNOWN STABILITY

HW3239\_SATELLITE: THE SITE LOCATION WAS REPORTED AS NOT SUITABLE FOR

HW3239+SATELLITE: SATELLITE OBSERVATIONS - 1986

HW3239

HW3239 HISTORY - Date Condition Recov. By

HW3239 HISTORY - 1976 MONUMENTED NASA

HW3239 HISTORY - 1986 GOOD

HW3239

HW3239 STATION DESCRIPTION

HW3239

HW3239'DESCRIBED BY NAT AERO SPACE ADMIN 1976

HW3239'PRIMARY SCIENTIFIC PURPOSE - MEASUREMENTS SUPPORTING THE DETERMINATION HW3239'OF PLATE MOTION, PLATE STABILITY, AND POLAR MOTION /EARTH ROTATION.

HW3239'SITE DESCRIPTION - THE STATION IS LOCATED IN EASTERN WEST VIRGINIA AT HW3239'THE NATIONAL RADIO ASTRONOMY OBSERVATORY (NRAO) OPERATED BY THE HW3239'NATIONAL SCIENCE FOUNDATION. THE 140-FOOT RADIO TELESCOPE AND THE HW3239'NUMBER 3 85-FOOT ANTENNA HAVE BEEN USED FOR VLBI MEASUREMENTS.

HW3239'THE MARK IS A REFERENCE POINT ON THE 43-METER (140-FOOT) RADIO

HW3239'SITE TOPO MAP - CASS, WV., USGS.

HW3239'GEOLOGICAL PROVINCE - THE VALLEY AND RIDGE PROVINCE

HW3239'LOCAL GEOLOGY - PALEOZOIC CONSOLIDATED SEDIMENTARY ROCKS

HW3239

HW3239 STATION RECOVERY (1986)

HW3239

HW3239'RECOVERED 1986

HW3239'TELESCOPE.

HW3239'RECOVERED IN GOOD CONDITION.