NATIONAL RADIO ASTRONOMY OBSERVATORY

June 24, 1978

ENGINEERING MEMO #124

Stepping Bar Results for the 140-foot Telescope

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1. Introduction

This note is intended to give the results of the measurements made on June 7 and June 8 and to draw conclusions from them. The way the measures were made is covered in J. Ralston's Memo. #123. The details of the lengthy data reduction will not be given; the methods were straightforward.

2. Edge and center ring measures

On May 3 and again on June 1 the elevations of the outer ring of targets were measured using the Wild level on top of the Cassegrain house. The results are given in Table 1. To remove the unknown tilt of the telescope, a best-fit plane surface was passed through the measured points; the numbers in Table 1 are the elevations with respect to this plane. The agreement between the two sets of measurements is good. We propose to use such measurements, taken again when the dish is finally measured, to fix the end-point values for each of the stepping runs. In presenting the results of the June 7 & 8 runs, we have adjusted the unknown "zero-point angle" of the bar and inclinometer to give the end-point values for the four radii the same as those found from Table 1.

Table 2 gives a similar set of measures (see Memo #123) for the center ring of targets. We have not troubled to adjust the present results to include these elevations; this must, of course be done in the final measurements.

3. The raw data and its reduction to angles and lengths.

Table 3 shows the raw data in volts from the tilt and length sensors. Each tilt value is the mean of 10, and each length the mean of 5 readings. The RMS of the tilt voltage was also read and stored.

The following relations were used to get the tilt angle A and the step length L from the corresponding sensor voltages:-

$$\sin A = (.0071 - V) \times 5.01036 \times 10^{-2}$$
 (1)

$$L = 0.508 (V - 3.3127)$$
(2)

Table 4 gives all the angle and length data which result from these conversions.

4. The computed profiles for the four radii.

The profiles were computed from the data of Table 4 in the following way. A single value (X= 1575.77 mms, Y = 33.94 mms) was used for the start points for each radius. The first runs on all radii on June 8 (called June 8.1 throughout) were inadvertently taken with the DVM set on the 100-volt scale instead of the 10-volt scale. The error due to digitising is 1 millivolt (10.8 arc seconds) and this is not serious. However, inspection of the results shows that the meter calibration differs by about 0.16 % on the two ranges. This was allowed for in reducing the data. Each run over a radius was forced to give the end value found from the optical level measures.

The 9825A print-out gives the X and Y values for each of the 33 points along a radius. To show the departures from the parabolic shape, the quantity D was computed for each point.

$$D = X^{2}/_{73152} - Y$$
 (3)

where X and Y are the measured co-ordinates of the point in mms. Table 6 gives the values for D for each of the three runs along the four radii. The mean D is also given, and the final column is the RMS value of the departures of D from this mean. The D values are also plotted in Figures 1.1 through 1.4.

5. Discussion of the results

In studying the data, it became apparent that the step-length measures were not as consistent as they should be. This can be seen by looking at the numbers in Table 5, where, for example, Step # 19 shows a range of L

of half a millimeter. We believe this can easily be improved, and so to minimise the effects of the L differences from run to run we have used the mean L values in deriving the D values.

Figures 2.1 through 2.4 are interesting. They show the measured RMS values for the angles. We have plotted all three runs on a given radius on the same graph. (The value of zero at maximum X is a plotting error). High values of the RMS seem to cluster at 8-10 meters and at about 20 meters. There was a fair amount of machinery running during the measurements, and this amy be the source of the vibration. Nevertheless, the noisy values of angle on Radius # 1 at 8 - 10 meters do not seem to cause errors in the profile - in fact the agreement in D is best for Radius # 1.

Finally, in the following Table 7, we summarize the results.

Table 7 The Results for the 4 radii.

Radius #	Date measured	Zero-point angle	RMS of D	Edge value of Y
1	June 7 June 8.1 June 8.2	16.9782° 16.9727° 16.9770°	0.973 mm 0.912 mm 0.885 mm	53 mm
2	June 7 June 8.1 June 8.2	16.9722 ⁰ 16.9646 ⁰ 16.9727 ⁰	1.476 mm 1.528 mm 1.297 mm	+1.71 mm
3	June 7 June 8.1 June 8.2	16.9813 [°] 16.9757 [°] 16.9806 [°]	1.709 mm 1.608 mm 1.804 mm	71 mm
4	June 7 June 8.1 June 8.2	16.9905 ⁰ 16.9843 ⁰ 16.9893 ⁰	1.036 mm 1.099 mm 1.118 mm	+.92 mm

The values of the zero-point angle do not tell much, since they include the unknown tilt of the telescope. The values for June 8.1 are all lower; this may well be due to the DVM having a slightly different zero on its 10 and 100 volt scales, as well as the calibration slope difference already noted.

If we accept as a rough measure of the accuracy of the stepping method the average of all the RMS values of D in Table 6, we arrive at:-

Mean RMS = 112 microns

However, this does not include errors due to our reliance on the optical level edge measures, but it does seem safe to go ahead with the whole dish measurement, with a good chance of getting a measuring accuracy of about 200 microns. This would be quite good enough.

6. Some practical points

- (a) Why are the L measures not more consistent ?
- (b) We should now calibrate the inclinometer. I favor doing this by mounting it on the 140-foot and tilting it with the elevation drive. A calibration to a few arc seconds is fine, and the inductosyns will do this.
- (c) If we do (b), we should check for long-term calibration changes.
- (d) We might train two two-person crews to do the bar setting. I would prefer to have JR and SS supervising - and I hope one could do the optical edge measures while the stepping is being done.
 - (e) I would try to do 24 radii a night (6 hours, 24x33 = 792 points) and then interleaf the other 24 radii the following night. The excellent June 7 to June 8 agreement makes this look good.
 - (f) Can the targets be fixed ahead of time? Ask Rick Fisher' opinion. If not, it can be done just before the measurements.

Table 1

The elevations of the outer ring of telescope targets measured on May 3rd. and June 1st 1978 by Wild level.

The elevations are in millimeters above or below the plane which best fits the results. Positive values mean that the point lies below the best-fit plane.

May 3	June 1	May	3 - June 1
2.1.29579141840253509966122495735099661222843586327868377734409693966122284358632786837773445052683228843588461225683777344507338588478268278683777344506612228843588478266278683777344507358684782684782568327868377734466122786837773446612278683777746686122868435884782662786883777746686122868435886278688377774668612286843588627868837777466861228684358862786883777746686122868435886278688377774668612286843588627868837777466861228684358862786883777746686122868435886278688377774668612286843588627868837777466861228684358862786883777746686122868435886278688377774668612286843588687886878868788687886878868788687886	1.48148 1.0976974752626474 1.0976967477256264744 1.05276944225626474 1.05276944245 1.05276944744 1.05276944744 1.05276944744 1.0976969417 1.0976969417 1.0976969417 1.0976969417 1.0976969417 1.0976969417 1.0976969417 1.09769694918 1.0976969486225 1.1896486225 1.1896486225 1.199696918 1.19969696918 1.199696918 1.199696918 1.199696918 1.199696918 1.199696918 1.199696918 1.199696918 1.199696918 1.199696918 1.199696918 1.199696918 1.199696918 1.199696918 1.199696918 1.199696918 1.199696918 1.199696918 1.19969696918 1.199696969698 1.19969696969696969696969696969696969696		4.685499877919848198563441986138636944198613869444198618869444198618869444537286189563869445372861895638694453728638694453728638694453728638694453728638694453728638694453728638694453728638694453728638694453728638694453728638694453728638694453728638694453335724658944537286386944538694459445386944594694459469469469469469469469469469469469469469

The elevations in millimeters of the starting circle of targets. The plane of reference is the best-fit to the points

Points 1 to 24	Points 25 to 48
-0.076	-0.088
-0.087	-0.090
-0.019	-0.026
-0 . 010	0.001
-0.083	-0.066
-0.053	0.026
-0.055	0.104
0.007	0.035
-0.021	0.017
0.048	0.105
0.050	0.127
0.118	0.041
-0.072	-0.133
0.092	-0.119
0.163	-0.057
-0.048	-0.035
-0.080	-0.069
-0.036	-0:044
-0.037	0.002
0.001	0.120
-0.020	0.067
a.a15	0.109
0.044	0.092
0.020	0.016

Table 2

RADIUS #1
THE RAW DATA AS TILT VOLTS AND LENGTH VOLTS ARE GIVEN BELOW

Table 3

Note: The rightmost column was reproduced for the scanning process. The original data were obscured by a piece of scotch tape and unscanable.

RADIUS #2

MAE RAW DATA AS TILT VOLTS AND LENGTH VOLTS ARE GIVEN BELOW

-3.42561 2.8628 -3.41900 3.0910 -3.42731 4.4582 -3.14646 3.5749 -3.14050 3.3720 -3.14867 4.4392 -2.79027 3.3455 -2.78370 3.3840 -2.79039 4.4560 2.34356 3.5013 -2.33660 2.9790 -2.38821 4.4560 -2.10680 3.3960 -2.10060 3.3426 -2.10619 4.7601 -1.76375 3.1870 -1.75640 3.4310 -1.76277 4.6930 -1.48993 3.3932 -1.40810 3.3390 -1.49111 3.4959 -0.79362 3.5016 -0.79100 3.4924 -0.79817 3.5266 -0.50441 3.8605 -0.50310 3.1788 -0.50690 3.4865 -0.15873 3.3691 -0.15540 3.2992 -0.14949 3.5599 0.4219 3.2407 0.17070 3.2946 0.16870 3.5920 0.4219 3.2407 0.17070 3.2500 0.41972 3.5673 0.71486 3.0844 0.71370 3.1252 0.71049 3.574 <t< th=""><th>JUNE 7</th><th>JUNE 8.1</th><th>JUNE 8.2</th></t<>	JUNE 7	JUNE 8.1	JUNE 8.2
	-4.48717 3.2277 -4.12979 3.3843 -3.78967 3.2314 -3.42561 2.8628 -3.14646 3.5749 -2.79027 3.3455 -2.34356 3.5013 -2.10680 3.3960 -1.76375 3.1870 -1.42741 2.8755 -1.08993 3.3691 -1.79362 3.3691 -0.15873 3.2407 0.42129 3.2416 0.71486 3.9844 1.30246 3.3929 2.22237 3.1798 2.71053 3.3943 3.9993 3.9998 3.51569 3.0007 3.93214 3.6448 4.21953 1.6475	-4.47650 -4.12090 -3.78110 -3.4472 -3.41900 -3.14050 -2.78370 -2.78370 -2.33660 -2.10060 -1.75640 -1.42060 -1.64560 -1.64560 -1.64560 -2.15540 -2.15540 -2.15540 -2.15540 -2.15540 -2.15540 -3.1252 -4.2010 -3.1252 -4.2010 -3.1252 -4.2010 -3.1252 -4.2010 -3.1252 -4.2010 -3.1252 -4.2010 -3.20690 -4.2010 -3.2500 -4.2010 -3.2500 -4.2010 -3.2500 -4.2010 -3.2500 -4.2010 -3.2500 -4.2010 -3.2500 -4.2010 -3.2500 -4.2010 -3.2500 -4.2010 -3.2500 -4.2010 -3.2500 -4.2010 -3.2500 -4.2010 -3.2500 -4.2010 -3.2500 -	-4.48540 4.5938 -4.12915 4.6416 -3.78845 4.4592 -3.42731 4.4592 -2.79039 4.4500 -2.33821 4.4560 -2.10619 4.7001 -1.76277 4.6930 -1.09111 3.4959 -0.14949 3.5599 0.16870 3.5599 0.16870 3.5599 0.16870 3.5599 0.16870 3.5599 1.16365 3.5599 0.41972 3.56757 2.46864 3.7340 2.72251 3.6757 2.46864 3.7340 3.7363 3.6425 2.22251 3.6757 2.46864 3.7340 3.7363 3.6425 3.73883 3.7264 3.93282 3.2224

RADIUS #3

-4.82337 3.0813 -4.81180 3.0560 -4.82005 3.5462 -4.49006 3.0868 -4.48000 3.1468 -4.48757 3.5685 -4.14783 1.3336 -4.13960 1.1570 -4.14720 3.5489 -3.80214 3.2541 -3.79440 2.9500 -3.80175 3.5079 -3.46735 3.2266 -3.46040 3.0830 -3.46730 3.5004 -3.12001 3.5947 -3.11410 3.2510 -3.12081 3.5353 -2.79339 3.3381 -2.78740 3.3034 -2.79265 3.5585 -2.41962 3.3773 -2.41250 3.5872 -2.41671 3.6145 -2.10902 3.1874 -2.10320 3.3710 -2.10905 3.5848 -1.81045 3.1141 -1.80600 3.2230 -1.81050 3.5323 -1.43407 3.1981 -1.42770 3.3816 -1.43283 4.1966 -0.78374 2.5991 -0.77940 2.6372 -0.78578 4.2274 -0.45636 2.7804 -0.45220 2.7410 -0.45559 4.2857 -0.16588 2.9569 -0.18140 3.2560 -0.18335 3.9307 0.16951 3.1540 0.16970 3.2100 0.16878 3.9074 0.47016 3.0237 0.46970 3.1770 0.46960 3.9993 0.74165 3.1578 0.74010 3.1650 0.73990 3.9976 1.11645 3.2052 1.11780 2.3728 1.1916 3.9993 0.74165 3.1584 0.16970 3.2100 0.16878 3.9076 1.11645 3.2052 1.11780 2.3728 1.1916 3.9993 0.74165 3.1578 0.74010 3.1650 0.73990 3.9976 1.11645 3.2052 1.11780 2.3728 1.1916 3.9993 0.74165 3.1584 0.16970 3.2100 0.16878 3.9076 1.11645 3.2052 1.11780 2.3728 1.11916 3.9993 0.74165 3.1584 1.64460 3.1860 1.64592 4.0761 1.89658 2.5819 1.89580 2.6572 1.89689 4.1010 2.22350 4.9685 2.22140 3.3830 1.64592 4.0761 1.89658 2.5819 1.89580 2.6572 1.89689 4.1010 2.27280 4.9685 2.22140 3.3830 2.22290 4.0839 2.46299 3.1300 2.45960 3.2478 2.46243 4.2412 2.71815 3.0610 2.71490 3.2190 2.71705 4.2210 3.02094 2.5713 3.01680 2.4780 3.24950 2.71705 4.2210 3.02094 2.5713 3.01680 2.4780 3.24950 2.71705 4.2210 3.02094 2.5713 3.01680 2.4780 3.24950 2.71705 4.2210 3.92994 2.5713 3.01680 2.4780 3.0490 4.18724 3.1187 4.19198 2.9814 4.18260 3.0490 4.18724 3.1187	JUNE 7	JUNE 8.	. 1	JUNE 8.2	
4.44564 3.3838 4.43720 3.1838 4.44037 3.3853	-4.82337 3.6 -4.49006 3.6 -4.14783 1.3 -3.80214 3.2 -3.12001 3.5 -2.79339 3.3 -2.41962 3.1 -1.81045 3.1 -1.81045 3.1 -1.83407 3.1 -1.08804 2.5 -0.16951 3.1 -0.74165 3.1 -0.74165 3.1 -1.11645 3.1 -1.33419 3.6 -0.74165 3.1 -1.33419 3.6 -0.74165 3.1 -1.33419 3.6 -0.74165 3.1 -1.33419 3.6 -0.74165 3.1 -1.33419 3.6 -0.74165 3.1 -1.33419 3.6 -0.74165 3.1 -1.33419 3.6 -0.74165 3.1 -1.33419 3.6 -0.74165 3.1 -1.33419 3.6 -0.74165 3.1 -1.33419 3.6 -1.33	813 -4.81180 868 -4.48000 336 -4.13960 541 -3.79440 266 -3.46040 947 -3.11410 381 -2.78740 773 -2.41250 874 -2.10320 141 -1.80600 981 -1.4270 804 -0.77940 804 -0.45220 559 -0.18140 804 -0.74910 805 -0.18140 805 -1.11780 805 -2.22140 807 -2.45960 808 -2.23140 809 -2.71490 809 -2.71490 809 -2.71490 809 -2.71490 809 -2.73510 809 -2.73510 809 -2.23140 809 -3.97830 809 -3.97830 809 -3.97830 809 -3.97830 809 -3.97830 809 -3.97830	3.0560 -4.82 3.1468 -4.48 1.1570 -4.14 2.9500 -3.80 3.0830 -3.46 3.2510 -3.12 3.3834 -2.79 3.3710 -2.10 3.3816 -1.81 3.2230 -1.81 3.3898 -1.08 2.6372 -0.78 2.7410 -0.45 3.2760 -0.18 3.1650 0.46 3.1770 0.46 3.1860 1.64 2.6572 1.89 3.3830 2.22 3.2478 2.46 3.2290 2.71 3.2660 3.27 2.728 1.11 3.0990 1.33 3.1860 1.64 2.4780 2.27 3.2478 2.46 3.2190 3.25 2.4780 3.25 2.4260 3.49 2.5460 3.73 2.54780 3.98 3.983 3.98	305 3.5462 757 3.5685 720 3.5489 175 3.5004 730 3.5353 730 3.5353 730 3.5353 730 3.5353 730 3.5353 731 3.5348 735 3.5348 735 4.2274 735 4.2274 735 4.2274 735 4.2274 737 4.2078 743 4.2210 743 4.2210 743 4.2210 742 4.2078 742 4.2078 742 4.2078 742 4.2078 743 3.1926 744 3.1926 745 3.1926 747 3.1926 748 3.1926 749 3.1926 740 3.1926 741 3.1926 742 3.1926	

RADIUS #4

JUNE 7	JUNE 8.1	JUNE 8.2
-4.85614	-4.84590	-4.85262 3.47110 -4.47525 3.56900 -4.18593 3.85430 -3.77164 3.89310 -3.45529 3.94250 -3.13878 0.59200 -2.77707 3.41090 -2.36682 2.47990 -1.78004 3.47570 -1.44940 3.49500 -1.44940 3.49500 -1.14243 3.49500 -1.14243 3.49500 -0.76205 3.57680 -0.15042 3.72090 0.46941 3.72090 0.46941 3.72090 0.15042 3.72090 0.15040 3.72090 0.150600 0.72838 4.00930 0.7283845 3.63800 0.572415 3.41490
3.96202 3.12210 4.20160 3.05530 4.43830 2.92560	3.95760 3.28800 4.19610 3.22400 4.43320 3.04840	3.96019 3.43550 4.19932 3.42170 4.43192 3.40490

CONVERSION OF RADIUS #1

JUNE 7	JUNE 8.1	JUNE	8.2
14.08113	14.07385 650 12.97999 650 12.04844 650 12.90568 649 9.97857 650 9.97857 650 9.07857 650 9.07857 650 4.16115 650 4.16115 650 4.16115 650 4.16115 650 4.16115 650 4.16371 650 4.16371 650 4.16371 650 4.16371 650 -1.24571 650 -2.22581 649 -3.87291 649 -3.87291 649 -3.87291 649 -3.87291 649 -7.85559 649 -7.85559 649 -7.85559 649 -7.85559 649 -7.85559 649 -7.85559 649 -7.85559 649 -7.85559 649 -7.85559 649 -7.85559 649 -7.85559 649 -7.85559 649 -7.85559 649	.0503	8. 2 491999244885 491999244885 49199999999999999999999999999999999999
-12.87135 650.1003	-12.88235 649	.9560 -12.87977	650.0479

Table 4

The data of Table 3 converted to angles in degrees and lengths in millimeters.

CONVERSION OF RADIUS #2

14.04150 650.0814 14.02821 650.0677 14.03988 650.1362 13.01341 649.9568 13.00301 650.0540 13.01275 650.6568 11.96260 650.0364 11.95585 650.1134 11.96490 650.6751 10.96631 649.9587 10.95898 650.0683 10.96658 650.6751 9.90361 649.7715 9.90036 649.8874 9.91203 650.5819 9.09110 650.1332 9.08847 650.0362 8.06017 650.5723 8.05701 650.0167 8.05098 650.0362 8.06017 650.5782 6.07983 650.0958 6.75460 649.8385 6.75069 650.5888 6.07983 650.09423 6.07175 650.0161 5.08927 650.7042 4.12164 649.7779 4.10868 649.8081 4.11689 650.0662 3.15086 650.0409 3.15069 650.0134 3.15536 650.0931 4.29926 650.0409 3.15069 650.0134 3.15536 650.0931 2.29926 650.0409 3.15069 650.04466
-10.79299 649.8415 -10.79502 649.8239 -10.77996 649.9249 -11.34163 650.1687 -11.36487 649.8717 -11.34759 649.9541

Table 4

The data of Table 3 converted to angles in degrees and lengths in millimeters.

TOMVERSION OF RADIUS #3

JUNE 7	JUNE 8.1	JUNE 8.2
14.00603 649.8824 13.02193 649.8852 12.01554 648.9946 11.00278 649.9563 10.02527 649.9563 8.06605 650.0129 6.98373 649.8991 4.14081 649.9363 5.22492 649.8991 4.14081 649.9418 3.14543 649.8991 4.14081 649.9418 3.14543 649.8375 1.33059 649.83991 4.14081 649.9418 3.14543 649.8375 1.33059 649.83991 4.14081 649.9363 649.8375 649.8388 649.8588 649.8532 649.8532 649.8532 649.8532 649.8588 649.8532 649.8588 649.8588 649.8588 649.8588	13.99443 649.8696 13.01333 649.9157 12.01081 648.9049 10.99793 649.8333 9.01161 649.9953 6.96172 649.9953 6.97441 650.0350 3.13486 649.5368 4.12915 650.0350 3.13486 649.5368 4.12915 650.9568 4.12915 650.9568 4.12915 649.9554 4.12915 649.9550 3.13486 649.9554 4.12915 649.9550 -3.2078 649.9550 -3.13486 649.9550 -3.13486 649.9556 -1.33027 649.9356 -2.10812 649.9356 -3.82737 649.9356 -3.82737 649.9556 -3.82737 649.9556 -3.82737 649.9556 -3.82737 649.9556 -3.82737 649.9556 -3.82737 649.9556 -3.82737 649.9556 -4.71373 649.9556 -5.43886 649.9524 -6.38008 650.0357 -7.81003 649.9526 -1.36998 649.5560 -9.37715 649.8560 -10.78273 649.85660	JUNE 8.2 14.00110 650.1186 13.01914 650.1299 12.01789 650.1200 11.00549 650.0992 10.02863 650.0954 9.01969 650.1131 8.06673 650.1249 6.97775 650.1382 5.22690 650.4490 4.13869 650.4490 2.27754 650.4990 2.27754 650.3339 -0.46431 650.3990 -2.10488 650.3990 -2.10488 650.3990 -3.19519 650.3990 -3.19519 650.3990 -3.19519 650.3990 -3.19519 650.3990 -3.19519 650.3990 -3.19519 650.3990 -3.19519 650.3990 -3.19519 650.3990 -3.19519 650.3990 -3.19519 650.3990 -3.19519 650.3990 -3.19519 650.3990 -3.19519 650.3990 -3.19519 650.3990 -3.19519 650.3990 -3.19519 650.3990
-12.84926 650.0361	-12.84519 649.9345	-12.83824 650.0369

Table 4

the data of Table 3 converted to angles in degrees and lengths in millimeters.

JUNE 7	JUNE 8.1	JUNE	8.2
14.10300 649.3872 12.99052 649.8678 12.13126 649.8016 10.91874 649.9046 9.96819 649.9992 6.83367 649.8308 6.05708 649.9575 4.18631 649.9575 4.18631 649.9101 2.20923 649.9301 2.20923 649.9316 -0.41769 649.8682 0.47922 649.9316 -1.32886 650.1888 -2.07369 650.4618 -3.16857 649.9674 -4.63029 650.3321 -5.51667 649.9674 -4.63029 650.3321 -5.51667 649.9674 -4.63029 650.3321 -5.51667 649.9674 -4.63029 650.3321 -5.51667 649.9674 -4.63029 650.3321 -5.51667 649.9674 -4.63029 650.3321 -5.51667 649.9674 -4.63029 650.3321 -5.51667 649.9674 -4.63029 650.3321 -5.51667 649.9674 -4.63029 650.3321 -5.51667 649.9674 -4.63029 650.3321 -5.51667 649.9674 -4.63029 650.3321 -5.51667 649.9674 -4.63029 650.3321 -5.51667 649.9674 -4.63029 650.3321 -5.51667 649.9032	14.09549 649.4072 12.98117 649.9392 12.12430 649.9113 10.91388 649.6214 9.98297 649.9676 6.05151 649.9676 6.83221 649.9590 4.18421 649.3746 3.28749 649.9150 2.20567 649.9590 4.18421 649.9590 4.18421 649.9590 4.18421 649.9613 6.48019 649.9613 6.48019 649.9613 6.48019 649.7228 6.32266 649.7228 6.32266 649.7228 6.32266 649.7228 6.32266 649.7228 6.32266 649.7286 6.25106 649.7286 6.25106 649.8659 6.25106 649.86938 6.25106 649.86938 6.25106 649.86938 6.25106 649.86938 6.25106 649.86938 6.25106 649.86938 6.25106 649.86938 6.25106 649.86938 6.25106 649.86938 6.25106 649.86938 6.25106 649.86938 6.25106 649.86938 6.25106 649.86938 6.25106 649.86938 6.25106 649.8659	JUNE 14.09752 12.98283 12.13163 12.91742 12.99361 9.07154 9.02154 6.83550 6.83550 6.83550 6.83550 7.49011 0.42777 -3.16800 -1.32777 -3.16800 -7.0755 -7.0755 -7.0755 -7.0777 -7.12.2925 -12.81335	2

Table 4

The data of Table 3 converted to angles in degrees and lengths in millimeters.

The measured step lengths in millimeters. Radius # 1

Step #	June_7	June 8.1	June 8.2	RMS
123466786612346678662866786686868686868686868686868686	6500.299986214978655490.0938655499.0938655499.09386554509.09386554509.09386555555555555555555555555555555555555	956 956 967 97 97 97 97 97 97 97 97 97 9	99.00.00.00.00.00.00.00.00.00.00.00.00.0	0.1000 0.1000 0.1000 0.0000 0.

Table 5

The measured step lengths in millimeters. Radius # 2

Step #	June 7	June 8.1	June 8.2	RMS
12045670000111111111111100000000000000000000	650.033 649.956 649.959 649.773 650.099 650.099 650.099 650.099 650.099 649.964 650.099 649.99 649.99 649.99 649.99 649.99 649.99 649.879 649.879 649.879 649.879	650.054 650.054 650.067 650.067 650.066 650.066 650.0666 650.0666 650.0666 650.0666 650.0666 650.0666 650.0666 650.0666 650.0666 650.0666 650.0666 650.0666 650.0666 650.0666 650.0666 650.0666 650.0666 6649.0666 6649.0666 6649.06649 6649.06649 6649.06649	650.136 650.675 650.675 650.572 650.572 650.706 650.706 650.706 650.144 650.144 650.144 650.144 650.184 650.184 650.184 650.184 650.184 650.184 650.184 650.184 650.184 650.184 650.184 650.184 650.184 650.184 650.184 650.184 650.184 650.184 650.184	0.00755019593726076976948430945726020000000000000000000000000000000000

Table 5

The measured lengths in millimeters.

Radius # 3

Step #	June 7	June 8.1	June 8.2	RMS
1234567898112345678981233456789812	649.8855 649.8950 649.97563 649.97563 650.03394767 6550.03394767 6550.03394767 6550.03394767 6550.03394767 654499.8824 664499.8824 664499.88336 664499.88336 664499.88336 664499.88336 664499.88336 664499.88336 664499.88336	649.878 649.916 649.883 649.883 649.969 649.995 649.995 649.995 649.995 649.931 649.931 649.935 649.935 649.935 649.935 649.935 649.935	0.1309535382995355802953556550.12995355865544288458022155865500.12995355865500.12995355865500.12995355865500.12995355865500.12995355865500.12995355865500.1299535565500.1299535565500.1299535500.1299535565500.1299535565500.1299535565500.1299535565500.129955500.129955500.1299555500.1299555500.1299555500.1299555500.1299555500.129955500.1299555500.1299555500.1299555500.1299555500.1299555500.129955500.129955500.129955500.129955500.129955500.129955500.129955500.129955500.129955500.129955500.129955500.129955500.1299555500.1299555500.1299555500.1299555500.1299555500.1299555500.1299555500.1299555500.1299555500.1299555500.1299555500.1299555500.1299555500.1299555500.1299555500.1299555500.1299555500.1299555500.12995500.1299555500.1299555500.1299555500.1299555500.12995555500.1299555500.1299555500.1299555500.1299555500.1299555500.1299555500.1299555500.1299555500.1299555500.1299555500.1299555500.129955500.129955500.129955500.129955500.129955500.129955500.129955500.12995500.129955500.129955500.129955500.12995500.12995500.12995500.129955500.12995500.12995500.12995500.12995500.12995500.12995500.12995500.12995500.12995500.12995500.12995500.12995500.12995500.1299500.12995500.12995500.12995500.12995500.12995500.12995500.12995500.1299500	493686742001557440565500324000138 1151875589255574405655003240000138 00000000000000000000000000000000

Table 5

The measured step lengths in millimeters

Radius # 4

Step #	June 7	June 8.1	June 8.2	RMS
+2045678994-2045678999+2	7882752910880448239918925139364499.8091088044720918955139364499.80918925139364499.80918925139364499.80918925139364499.8091899.809654499.809654499.80965499.80965499.80965499.80965499.80965499.80965499.80965499.80965499.80965499.80965499.80965499.80965499.80965499.8096566666666666666666666666666666666666	649.931 649.921 649.621 649.621 649.49.391 649.391 649.391 6449.391 6449.391 6449.391 6449.391 6449.391 6449.391 6449.391 6449.391 6449.391 6449.391 6449.391 6449.391 6449.391 6449.391 6449.391 6449.391 6449.391	650.135 650.235 650.2310 650.3310 650.3310 650.057 650.057 650.057 650.037 650.037 650.037 650.374	2112979452965342896949198128867678 21129794529653428567948128867678 20.129548787428567948128987678 20.228567948128987678 20.2285679481288 20.228567948128 20.228567949198128 20.228567949198128 20.228567949198128 20.228567949198128 20.22867949198128 20.22867949198128 20.22867949198128 20.22867949198128 20.22867949198128 20.22867949198128 20.22867949198128 20.22867949198128 20.22867948128 20.22867949198128 20.22867949198128 20.22867949198128 20.22867949198128 20.22867949198128 20.22867949198128 20.22867949198128 20.22867949198128 20.22867949198128 20.22867949818 20.2286798 20.228

Table 5

THE MEAN VALUE OF D AND ITS RMS ALONG RADIUS # 1

June	June 8.	1 June 8.2	Mean	RMS
1 0.8	- 30 0.000	0.000	0.000	0.000
2 0.8;	31 0.861	0.800	0.847	0.035
3 0.8;		0.727	0.781	0.040
4 1.6		1.531	1.582	0.036
5 0.8;		0.777	0.819	0.032
6 0.7		0.809	0.807	0.006
7 1.8		1.986	1.934	0.040
8 1.5		1.634	1.560	0.053
	58 -0.164	-0.074	-0.136	0.044
10 0.6		0.714	0.656	0.043
	39 -0.353	-0.225	-0.272	0.057
12 -0.0		-0.025	-0.077	0.047
13 9.0		-0.173	-0.060	0.101
14 -9.4		-0.770	-0.647	0.115
15 9.8		0.479	0.648	0.162
16 0.3		-0.092	0.068	0.188
17 0.0		-0.277	-0.133	0.162
18 0.8		9.522	9.633	0.121
19 1.3 ¹		1.176	1.276	0.089
		0.975	1.080	0.086
21 1.1: 22 1.4:		0.906	1.029	0.108
23 1.8		1.076	1.226	0.135
24 1.2		1.530 1.049	1.649	0.114
25 1.1		0.995	1.146 1.075	0.103
26 1.0:		9.858 9.858	1.075 0.948	0.086 0.071
27 0.5		9.360	0.740 0.423	
28 1.3		1.329	1.337	0.065 0.025
	38 - 0.031	0.059	0.066	0.032
30 -0.2.		-0.211	-0.229	0.015
31 -0.5		-0.429	-0.474	0.037
32 -0. 0		0.076	0.037	0.040
33 -0.5:		-0.530	-0.530	0.000

* HE MEAN VALUE OF D AND ITS RMS ALONG RADIUS # 2

	June 7	June 8.1	June 8.2	<u>Mean</u>	RMS
1	0.000	0.000	0.000	0.000	0.000
	0.499	0.434	0.475	0.469	0.027
3	0.821	0.724	0.784	0.776	0.040
:	0.670	0.581	0.653	0.635	0.038
5	0.612	0.526	0.592	0.577	0.037
6	-0.176	-0.213	-0.105	-0.165	0.044
7	1.098	1.117	1.273	1.163	0.078
8	1.818	1.855	2.024	1.899	0.090
9	-1.192	-1.083	-1.053	-1.079	0.020
10	-0.743	-0.731	-0.696	-0.723	0.020
11	-0.732	-0.782	-0.703	-0.739	0.033
12	-0.949	-1.062	-0.981	-0.997	0.048
13	-1.548	-1.574	-1.533	-1.552	0.017
14	-1.261	-1.243	-1.089	-1.198	0.077
15	0.033	0.123	0.289	0.148	0.106
16	0.283	0.358	0.221	0.287	0.056
17	-0.140	0.040	-0.118	-0.073	0.081
18	1.357	1.647	1.422	1.475	0.124
19	3.134	3.517	3.335	3.328	0.156
20	-0.314	0.033	-0.195	-0.159	0.144
21	1.476	1.786	1.332	1.531	0.189
22	1.583	1.600	1.034	1.405	0.263
23	2.509	2.515	1.866	2.297	0.304
24	1.620	1.626	0.934	1.393	0.325
25	1.565	1.582	0.871	1.339	0.331
26	2.397	2.438	1.716	2.184	0.331
27	1.862	1.889	1.266	1.672	0.288
28	1.570	1.617	1.046	1.411	0.259
29	0.888	0.971	0.436	0.765	0.235
30	0.766	0.920	0.472	0.720	0.186
31	2.585	2.537	2.206	2.443	0.169
92	2.372	2.334	2.182	2.296	0.082
33	1.710	1.710	1.711	1.710	0.000

Table 6

THE MEAN VALUE OF D AND ITS RMS ALONG RADIUS # 3

	June 7	June 8.1	June 8,2	Mean	RMS
1	0.000	0.000	0.000	0.000	0.000
2	-0.010	-0.077	-0.058	-0.048	0.028
**************************************	0.300	0.199	0.228	0.242	0.043
4	0.632	0.541	0.594	0.589	0.037
5	0.860	0.778	0.862	0.834	0.039
	1.331	1.268	1.380	1.326	0.046
7	1.590	1.561	1.709	1.620	0.064
8	2.275	2.262	2.411	2.316	0.067
9	1.753	1.697	1.828	1.759	0.054
10	2.050	1.979	2.158	2.062	0.074
11	3.484	3.427	3.624	3.512	0.083
12	3.355	3.228	3.479	3.354	0.102
13	2.559	2.374	2.650	2.528	0.115
14	2.373	2.151	2.551	2.358	0.164
1,5	1.893	1.621	2.060	1.858	0.181
16	2.915	2.567	3.006	2.829	0.189
17	2.407	2.109	2.530	2.349	0.176
18	2.074	1.833	2.219	2.042	0.159
19	2.766	2.605	2.971	2.780	0.150
20	0.735	0.533	0.842	0.704	0.128
21	1.261	0.946	1.276	1.161	0.152
22	0.947	0.605	0.902	0.818	0.152
23	1.664	1.309	1.592	1.522	0.153
24	0.569	0.230	0.499	0,433	0.146
25	0.589	0.299	0.516	0.468	0.123
25	0.982	0.722	0.923	0.876	0.111
27	-0.184	-0.399	-0.265	-0.283	0.089
28	-0.295	-0.901	-0.776	-0.657	0.261
29	-0.504	-0.987	-0.936	-0.809	0.217
30	-0.686	-1.080	-0.978	-0.915	0.167
31	-1.052	-1.356	-1.338	-1.249	0.140
32	-0.399	-0.528	-0.553	-0.493	0.067
33	-0.709	-0.710	-0.710	-0.710	0.000

Table 6

THE MEAN VALUE OF D AND ITS RMS ALONG RADIUS # 4

	June 7	June 8.1	June 8.2	Mean	RMS
1	0.000	0,000	0.000	0.000	0.000
2	0.985	0.970	0.936	0.964	0.021
3	0.829	0.777	0.705	0.770	0.051
4	2.375	2.314	2.269	2.7320	0.044
5	1.547	1.500	1.439	1.496	0.044
Ë	1.512	1.457	1.460	1.476	0.025
7	2.279	2.177	2.277	2.242	0.046
3	2.293	2.201	2.336	2.276	0.'056
9	-0.093	-0.132	-0.039	-0.038	0.038
1.0	-0.278	-0.310	-0.229	-0.272	0.033
11	0.043	-0.002	0.074	0.038	0.031
12	0.288	0.289	0.333	0.304	0.021
13	1.102	1.069	1.235	1.135	0.072
14	0.040	9.037	0.189	0.089	0.071
15	1.179	1.297	1.451	1.309	0.111
16	1.164	1.367	1.473	1.335	0.128
17	1.978	1,344	1.476	1.299	0.165
18	0.597	0.890	1.023	0.837	0.178
19	1.563	1.898	2.028	1.830	0.196
20	-0.402	-0,012	0.086	-0.109	9.211
21	-0.130	0.351	0.414	0.212	0.243
ala mm	0.336 -0.128	0.865	0.869	0.690	0.250
<u> </u>	-9.120 9.199	0.438	0.430	0.247	0.265
25	0.177	0.815 0.884	0.803	0.606	0.288
a.u o.c	-0.298	0.298	0.842 0.203	0.689	0.246
2 U 2 Z	0.022	9.665	0.545	0.068 0.411	0.261 0.279
5	-0.018	0.718	0.556	0.419	0.316
29	0.240	0.192	-0.002	0.143	0.105
āá	0.563	0.518	9.289	0.457	0.120
31	0.934	0.895	0.689	0.839	0.107
32	1.084	1.080	0.884	1.016	0.093
33	0.921	0. 920	0.921	0.921	0.000
	10 1000 100		ees or so loves sin	no H or han de	Year D. Sout Sout Sout

THE 140 FOOT SURFACE

Black: June 7 Red: June 8.1 Green: June 8.2

Radius # 1

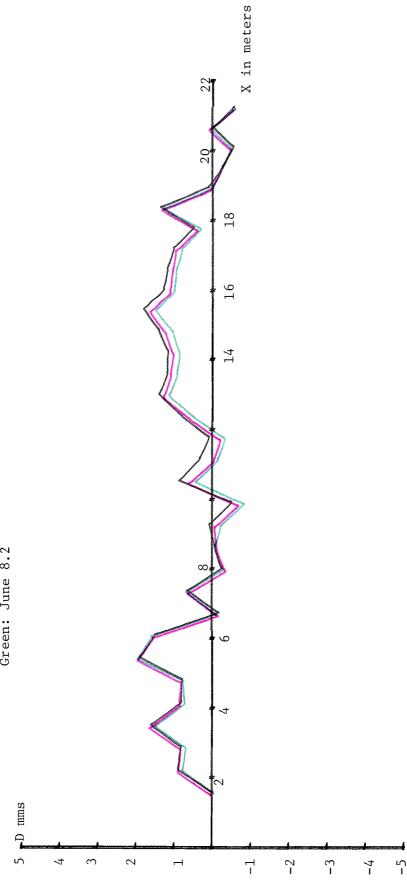
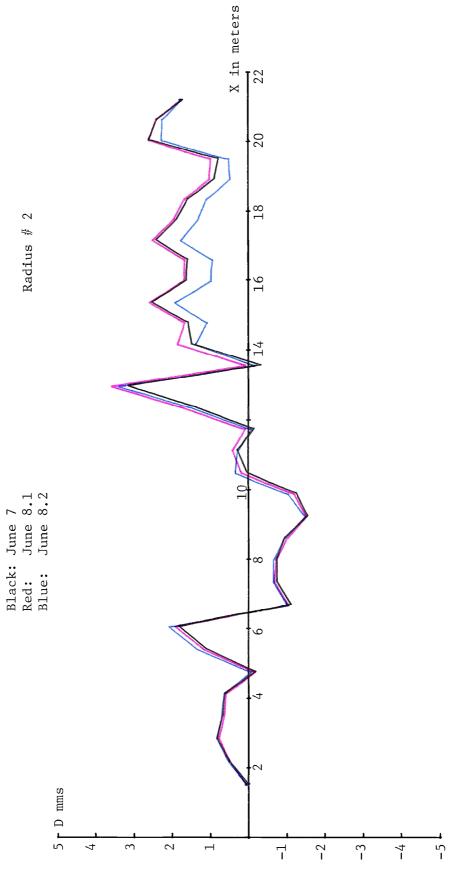


Figure 1.2

THE 140 FOOT TELESCOPE SURFACE



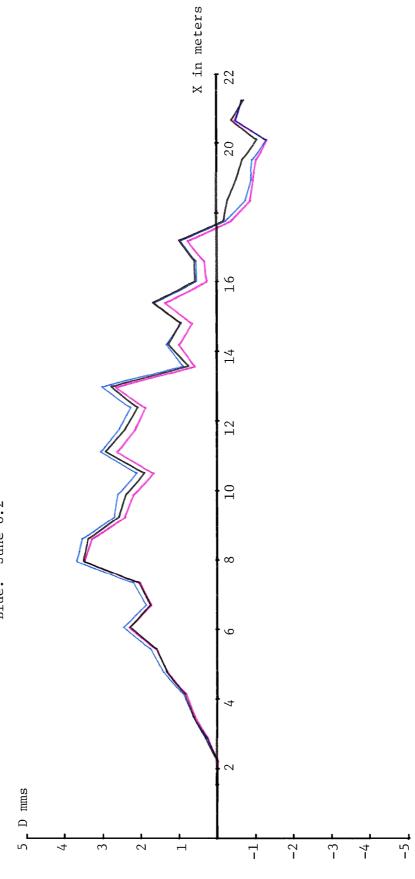
Radius # 2



THE 140 FOOT SURFACE

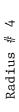
Black: June 7 Red: June 8.1 Blue: June 8.2

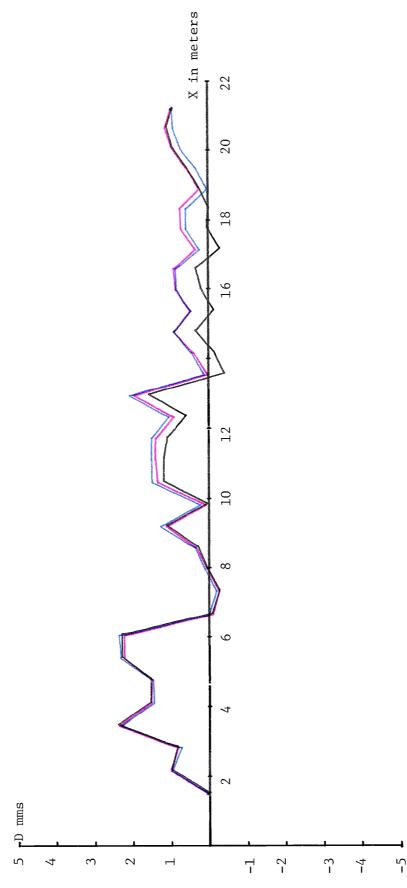
Radius # 3



THE 140 FOOT SURFACE

Black: June 7 Red: June 8.1 Blue: June 8.2





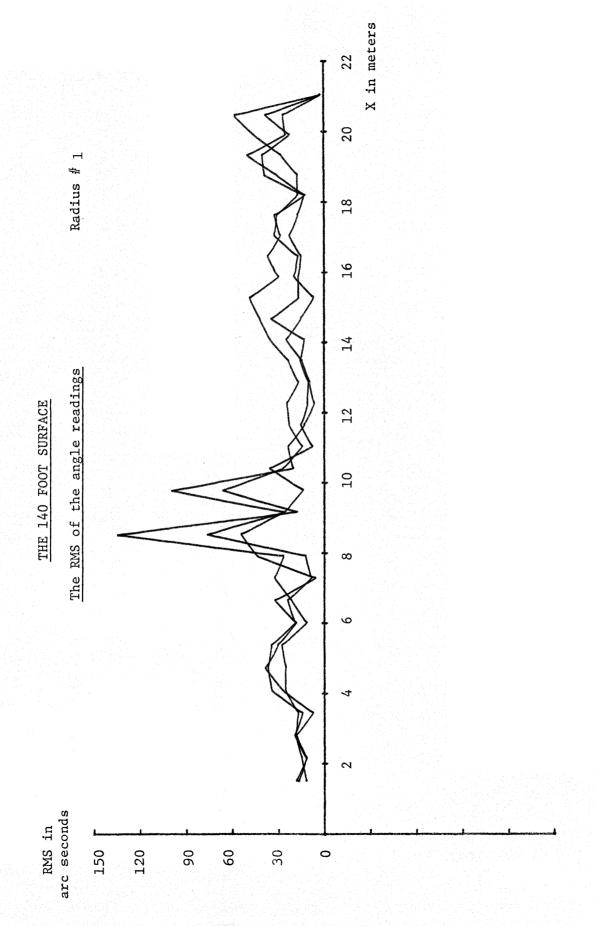
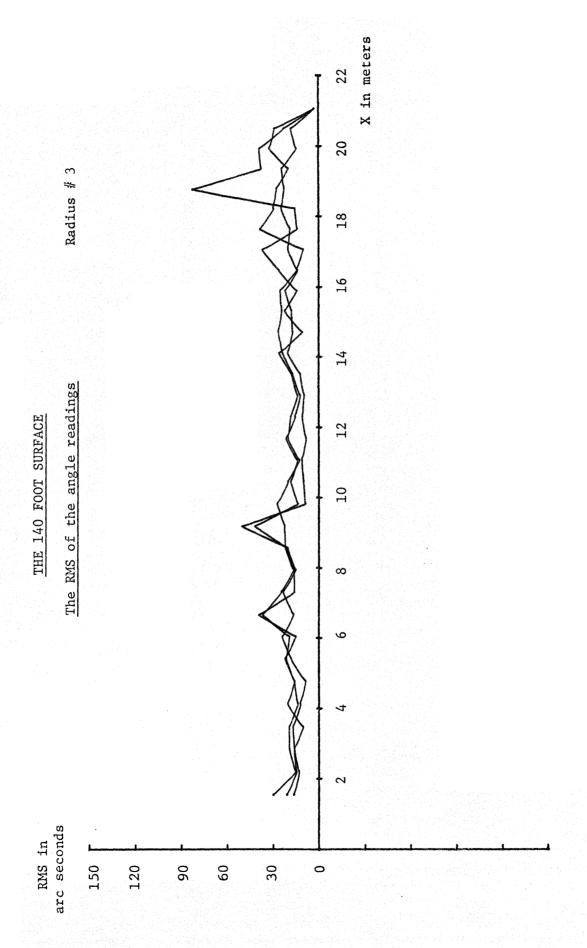
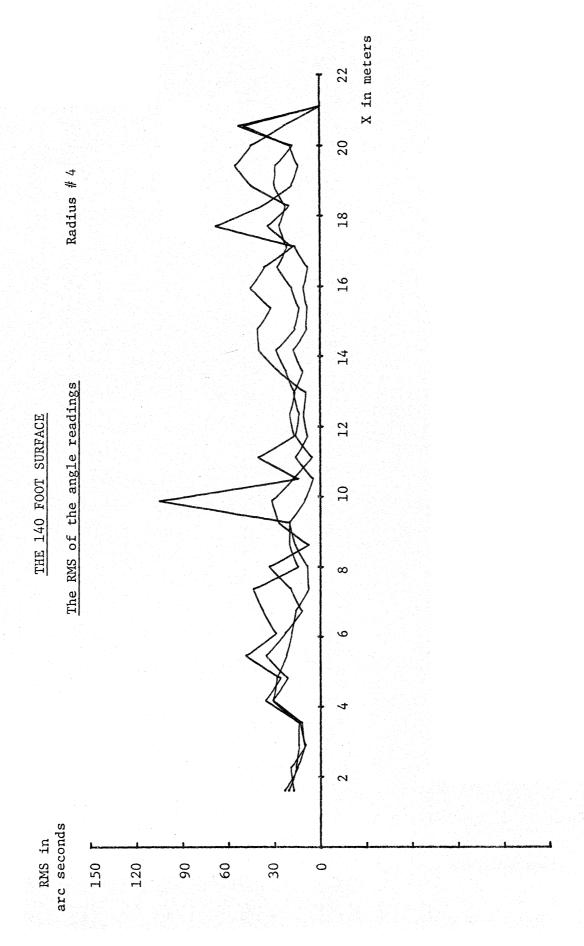


Figure 2.2





NATIONAL RADIO ASTRONOMY OBSERVATORY Charlottesville, Virginia

June 28, 1978

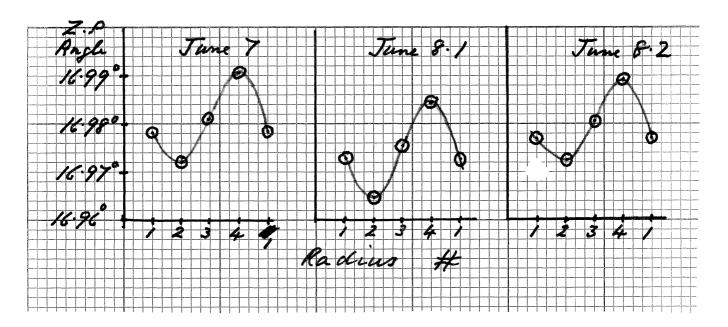
MEMORANDUM

To: Those Receiving Engineering Memo No. 124

From: John W. Findlay

Subj: Additional Analysis

1. I left the discussion of the results given in Table 7 of Memo No. 124 with a less-than-complete look at the zero-point angles (see the end of page 3). However, if one plots these angles against the radii for the three runs, one gets:



These results clearly support the suggestion that the dish was set each day at the same tilt. The way of stowing the dish now does this.

2. The best-fit curves to the points are:

June 7 A =
$$16.98053+9.285 \times 10^{-3}$$
 ($\sin \frac{n\pi}{2} + 100^{\circ}$)

June 8.1 A =
$$16.97432+9.975x10^{-3}$$
 ($\sin \frac{n\pi}{2} + 99^{\circ}$)

June 8.2 A =
$$16.97989 + 8.520 \times 10^{-3}$$
 ($\sin \frac{n\pi}{2} + 102^{\circ}$)

The agreement of amplitude and phase of the tilt is excellent, and says that the mean dish surface was 33 ± 2 arc seconds away from the local gravity horizontal.

If we leave out June 8.1 (DVM zero errors is possible), we find the mean A for the measuring bar was:

$$A_0 = 16.9802^{\circ} + 1 \text{ arc second.}$$

If all this is true, it seems as if our measuring system does have excellent day-to-day stability.

JWF/pj