# GAIN CURVES FOR 1.3CM VLBI WITH A SINGLE VLA ANTENNA 

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Most single-antenna VLBI projects at the VLA use just the preferred VLBI antenna identified in the VLA operator's log for that project. For 1.3 cm VLBI projects we try to provide two additional calibrator antennas, and we use the VIA correlator data from the resulting three-antenna subarray to give the ratio of antenna temperature to system temperature, Tant/Tsys, as a function of time for the VLA's preferred VLBI antenna. This ratio, which is all that is needed for amplitude calibration of VLBI baselines involving the VLA, tracks the effects of the position dependent gain (the "gain curve") and the pointing errors of the preferred VLBI antenna, plus the atmospheric opacity above that antenna. For operational reasons, however, some 1.3 cm VLBI projects involve just the preferred VLBI antenna. In such cases post-observing adjustments should be made for that antenna's gain curve and for the atmospheric opacity above that antenna. This memorandum provides information regarding gain curve adjustments. Suggestions regarding opacity adjustments will be dealt with in a separate test memorandum.

Crane (1991, VLA Test Memorandum No. 159) obtained VLA antenna gain data for IFs A, B, C and D on 1989 December 29-30 at an effective frequency of 22460.1 MHz . All antennas except for 21 and 22 were available. Over-the-top antenna motions were not allowed, as recommended for all 1.3 cm observing including VLBI. Crane first adjusted his observations for atmospheric opacity and then fitted the gain corrections with Legendre polynomials assuming a minimum correction at a zenith angle of 40 degrees. Each antenna showed good agreement among the four IFs, so Crane tabulated for each antenna the Legendre polynomial coefficients averaged over the four IFs. He also provided Legendre polynomial coefficients for the gain corrections for an average VLA antenna, which he called antenna "29"; these gain corrections might usefully be applied to antennas 21 or 22, as well as to 1.3 cm phased VLA observations. Consult Crane (1991) for a discussion of the significance of the 1989 gain correction differences from antenna to antenna, plus gain correction differences when compared with 1985 data (Crane, 1987, VIA Test Memorandum No. 149).

ANCAL in AIPS or CAL in the Caltech VLBI Analysis Programs require standard polynomial fits to the gain curve, which is the inverse of Crane's gain corrections. For each antenna, including " 29 . I have approximated the gain curve with the inverse of Crane's Legendre polynomial fit to the gain corrections, normalized the gain curve to its maximum, and fitted the normalized gain curve with a fifth-order polynomial using $C$. Walker's Fortran program "fit". Figure 1 compares the inverse of Crane's Legendre polynomial fits to the gain corrections with my standard polynomial fits to the normalized gain curves. Gain curve values from my fits are given in Table 1 every 4 degrees in zenith angle, which is sufficiently dense to permit application of interpolation schemes if desired.

Below I give complete antenna gain information, including my fitted polynomial coefficients, in the form expected by ANCAL and CAL for VLA antennas 1 through 20,23 through 28 , and " 29 ". Two points should be kept in mind when using this gain information. First, I have assumed that each antenna has the nominal 1.3 cm degrees per flux unit (DPFU) quoted by Crane \& Napier (1986, Synthesis Imaging in Radio Astronomy, ASP conference series volume 6, eds. Perley, Schwab \& Bridle [San Francisco: ASP], 139). Variations in DPFU from antenna to antenna are expected but no systematic measurements of these variations are presently available. Second, the VLBI correlator may use an antenna name for your project other than that assumed below. Consult the antennas file for your VLBI data and make the appropriate name substitution if necessary.

VLA antenna 1: GAIN VLA ALTAZ DPFU=0.082
POLY $=+0.99830 \mathrm{E}+00,+0.69335 \mathrm{E}-03,-0.61046 \mathrm{E}-04$, $-0.20542 \mathrm{E}-05,+0.38125 \mathrm{E}-07,-0.16986 \mathrm{E}-09 /$

VLA antenna 2: GAIN VLA ALTAZ DPFU=0.082
POLY $=+0.99929 \mathrm{E}+00,+0.29071 \mathrm{E}-03,-0.26353 \mathrm{E}-04$, $-0.12533 \mathrm{E}-05,+0.18808 \mathrm{E}-07,-0.71527 \mathrm{E}-10 /$

VLA antenna 3: GAIN VLA ALTAZ DPFU=0.082
POLY $=+0.84344 \mathrm{E}+00,+0.42562 \mathrm{E}-02,+0.37521 \mathrm{E}-04$, $-0.14501 \mathrm{E}-05,+0.29040 \mathrm{E}-08,+0.41362 \mathrm{E}-10 /$

VLA antenna 4: GAIN VLA ALTAZ DPFU $=0.082$
POLY $=+0.88697 \mathrm{E}+00,+0.37490 \mathrm{E}-02,+0.31550 \mathrm{E}-04$,
$-0.18109 \mathrm{E}-05,+0.10831 \mathrm{E}-07,+0.11181 \mathrm{E}-11 /$
VLA antenna 5: GAIN VLA ALTAZ DRFU=0.082
POLY $=+0.81221 \mathrm{E}+00,+0.39333 \mathrm{E}-02,+0.27406 \mathrm{E}-04$, $-0.60410 \mathrm{E}-06,-0.45888 \mathrm{E}-08,+0.55069 \mathrm{E}-10 /$

VLA antenna 6: GAIN VLAA ALTAZ DPFU $=0.082$
POLY $=+0.91072 \mathrm{E}+00,+0.28710 \mathrm{E}-02,+0.14770 \mathrm{E}-04$, $-0.10050 \mathrm{E}-05,+0.49226 \mathrm{E}-08,+0.81116 \mathrm{E}-11 /$

VLA antenna 7: GAIN VLA ALTAZ DPFU $=0.082$
POLY $=+0.80521 \mathrm{E}+00,+0.46668 \mathrm{E}-02,+0.41575 \mathrm{E}-04$, $-0.11537 \mathrm{E}-05,-0.36684 \mathrm{E}-08,+0.75107 \mathrm{E}-10 /$

VLA antenna 8: GAIN VLA ALTAZ DPFU $=0.082$
POLY $=+0.84548 \mathrm{E}+00,+0.40646 \mathrm{E}-02,+0.32370 \mathrm{E}-04$,

$$
-0.12109 \mathrm{E}-05,+0.13968 \mathrm{E}-08,+0.41096 \mathrm{E}-10 /
$$

VLA antenna 9: GAIN VLA ALTAZ DPFU=0.082
POLY $=+0.88285 \mathrm{E}+00,+0.32262 \mathrm{E}-02,+0.19441 \mathrm{E}-04$, $-0.91732 \mathrm{E}-06,+0.24575 \mathrm{E}-08,+0.20539 \mathrm{E}-10 /$

VLA antenna 10: GAIN VLA ALTAZ DPFU $=0.082$
POLY $=+0.88215 \mathrm{E}+00,+0.33278 \mathrm{E}-02,+0.21567 \mathrm{E}-04$, $-0.10309 \mathrm{E}-05,+0.32000 \mathrm{E}-08,+0.20464 \mathrm{E}-10 /$

VLA antenna 11: GAIN VLA ALTAZ DPFU=0.082
POLY $=+0.94535 \mathrm{E}+00,+0.26381 \mathrm{E}-02,+0.12000 \mathrm{E}-04^{\prime}$, $-0.17636 \mathrm{E}-05,+0.16119 \mathrm{E}-07,-0.36350 \mathrm{E}-10 /$

VLA antenna 12: GAIN VLA ALTAZ DPFU $=0.082$
POLY $=+0.81440 \mathrm{E}+00,+0.47925 \mathrm{E}-02,+0.48861 \mathrm{E}-04$, $-0.16022 \mathrm{E}-05,+0.57254 \mathrm{E}-09, \quad+0.65362 \mathrm{E}-10$ /

VLA antenna 13: GAIN VLA ALTAZ DPFU=0.082
POLY $=+0.97331 \mathrm{E}+00,+0.15866 \mathrm{E}-02,-0.66131 \mathrm{E}-06$, $-0.10459 \mathrm{E}-05,+0.99851 \mathrm{E}-08,-0.23228 \mathrm{E}-10 /$

VLA antenna 14: GAIN VLA ALTAZ DPFU $=0.082$
POLY $=+0.88346 \mathrm{E}+00,+0.33854 \mathrm{E}-02,+0.21897 \mathrm{E}-04$, $-0.11021 \mathrm{E}-05,+0.38728 \mathrm{E}-08,+0.19024 \mathrm{E}-10 /$

VLA antenna 15: GAIN VLA ALTAZ DPFU $=0.082$
POLY $=+0.88144 \mathrm{E}+00,+0.31877 \mathrm{E}-02,+0.19286 \mathrm{E}-04$, $-0.87167 \mathrm{E}-06,+0.20873 \mathrm{E}-08,+0.20935 \mathrm{E}-10 /$

VLA antenna 16: GAIN VLA ALTAZ DPFU=0.082
POLY $=+0.91245 \mathrm{E}+00,+0.34879 \mathrm{E}-02,+0.27739 \mathrm{E}-04$, $-0.21829 \mathrm{E}-05,+0.17535 \mathrm{E}-07,-0.29238 \mathrm{E}-10 /$

VLA antenna 17: GAIN VLA ALTAZ DPFU=0.082
POLY $=+0.86866 \mathrm{E}+00,+0.44241 \mathrm{E}-02,+0.49918 \mathrm{E}-04$, $-0.26577 \mathrm{E}-05,+0.17672 \mathrm{E}-07,-0.10220 \mathrm{E}-10 /$

VLA antenna 18: GAIN VLA ALTAZ DPFU $=0.082$
POLY $=+0.96139 \mathrm{E}+00,+0.24623 \mathrm{E}-02,+0.77170 \mathrm{E}-05$, $-0.23839 \mathrm{E}-05,+0.26618 \mathrm{E}-07,-0.82899 \mathrm{E}-10 /$

VLA antenna 19: GAIN VLA ALTAZ DPFU $=0.082$
POLY $=+0.77687 \mathrm{E}+00,+0.50309 \mathrm{E}-02,+0.48759 \mathrm{E}-04$,

$$
-0.10865 \mathrm{E}-05,-0.78073 \mathrm{E}-08,+0.10186 \mathrm{E}-09 /
$$

VLA antenna 20: GAIN VLA ALTAZ DPFU $=0.082$
POLY $=+0.83151 \mathrm{E}+00,+0.51104 \mathrm{E}-02,+0.73924 \mathrm{E}-04$, $-0.31539 \mathrm{E}-05,+0.17687 \mathrm{E}-07,+0.11594 \mathrm{E}-10 /$

VLA antenna 23: GAIN VLA ALTAZ DPFU=0.082
POLY $=+0.85965 \mathrm{E}+00,+0.41235 \mathrm{E}-02,+0.36397 \mathrm{E}-04$, $-0.16447 \mathrm{E}-05,+0.62953 \mathrm{E}-08,+0.26065 \mathrm{E}-10 /$

VLA antenna 24: GAIN VLA ALTAZ DPFU=0.082
POLY $=+0.91544 \mathrm{E}+00,+0.27415 \mathrm{E}-02,+0.14512 \mathrm{E}-04$,

$$
-0.99902 \mathrm{E}-06,+0.53543 \mathrm{E}-08,+0.43692 \mathrm{E}-11 /
$$

VLA antenna 25: GAIN VLA ALTAZ DPFU=0.082
POLY $=+0.82342 \mathrm{E}+00,+0.40254 \mathrm{E}-02,+0.30486 \mathrm{E}-04$,
$-0.83839 \mathrm{E}-06,-0.26339 \mathrm{E}-08,+0.51901 \mathrm{E}-10$ /
VLA antenna 26: GAIN VLA ALTAZ DPFU $=0.082$
POLY $=+0.90705 \mathrm{E}+00,+0.34446 \mathrm{E}-02,+0.25907 \mathrm{E}-04$, $-0.18651 \mathrm{E}-05,+0.13346 \mathrm{E}-07,-0.13653 \mathrm{E}-10 /$

VLA antenna 27: GAIN VLA ALTAZ DPFU=0.082
POLY $=+0.66159 \mathrm{E}+00,+0.57885 \mathrm{E}-02,+0.47140 \mathrm{E}-04$, $+0.44222 \mathrm{E}-06,-0.35081 \mathrm{E}-07,+0.23071 \mathrm{E}-09 /$

VLA antenna 28: GAIN VLA ALTAZ DPFU $=0.082$
POLY $=+0.90389 \mathrm{E}+00,+0.31510 \mathrm{E}-02,+0.18512 \mathrm{E}-04$, $-0.12138 \mathrm{E}-05,+0.63095 \mathrm{E}-08,+0.75857 \mathrm{E}-11 /$

VLA antenna "29" = average VLA antenna, if applied to a single VLA antenna: GAIN VLA ALTAZ DPFU=0.082
POLY $=+0.88484 \mathrm{E}+00,+0.37375 \mathrm{E}-02,+0.29616 \mathrm{E}-04$,
$-0.16660 \mathrm{E}-05,+0.89798 \mathrm{E}-08,+0.83668 \mathrm{E}-11 /$
VLA antenna "29" = average VLA antenna, if applied to phased VLA data using ANCAL in AIPS: GAIN VLA27 ALTAZ DPFU=1.0
$\begin{aligned} \text { POLY }= & +0.88484 \mathrm{E}+00,+0.37375 \mathrm{E}-02,+0.29616 \mathrm{E}-04, \\ & -0.16660 \mathrm{E}-05,+0.89798 \mathrm{E}-08,+0.83668 \mathrm{E}-11 /\end{aligned}$

Table 1. Gain Curve Values

| Zenith | Antenna |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| (degrees) | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 82 | 0.6060 | 0.7401 | 0.9298 | 0.9019 | 0.9826 | 0.9440 | 0.9439 | 0.9443 | 0.9596 |
| 78 | 0.6269 | 0.7566 | 0.9425 | 0.9161 | 0.9882 | 0.9532 | 0.9557 | 0.9552 | 0.9677 |
| 74 | 0.6492 | 0.7739 | 0.9551 | 0.9306 | 0.9931 | 0.9624 | 0.9674 | 0.9659 | 0.9756 |
| 70 | 0.6730 | 0.7920 | 0.9671 | 0.9448 | 0.9970 | 0.9712 | 0.9780 | 0.9759 | 0.9828 |
| 66 | 0.6983 | 0.8107 | 0.9778 | 0.9581 | 0.9994 | 0.9792 | 0.9871 | 0.9846 | 0.9891 |
| 62 | 0.7248 | 0.8297 | 0.9868 | 0.9702 | 1.0001 | 0.9861 | 0.9940 | 0.9916 | 0.9941 |
| 58 | 0.7523 | 0.8489 | 0.9936 | 0.9805 | 0.9989 | 0.9919 | 0.9984 | 0.9966 | 0.9977 |
| 54 | 0.7805 | 0.8679 | 0.9980 | 0.9889 | 0.9957 | 0.9962 | 1.0001 | 0.9994 | 0.9996 |
| 50 | 0.8088 | 0.8865 | 0.9999 | 0.9950 | 0.9904 | 0.9989 | 0.9988 | 0.9998 | 0.9999 |
| 46 | 0.8368 | 0.9044 | 0.9990 | 0.9986 | 0.9831 | 0.9999 | 0.9946 | 0.9978 | 0.9983 |
| 42 | 0.8640 | 0.9213 | 0.9954 | 0.9998 | 0.9739 | 0.9993 | 0.9875 | 0.9933 | 0.9950 |
| 38 | 0.8898 | 0.9371 | 0.9891 | 0.9983 | 0.9629 | 0.9969 | 0.9776 | 0.9864 | 0.9899 |
| 34 | 0.9138 | 0.9513 | 0.9803 | 0.9943 | 0.9502 | 0.9929 | 0.9651 | 0.9772 | 0.9832 |
| 30 | 0.9355 | 0.9640 | 0.9691 | 0.9877 | 0.9362 | 0.9872 | 0.9503 | 0.9660 | 0.9749 |
| 26 | 0.9544 | 0.9748 | 0.9558 | 0.9789 | 0.9209 | 0.9800 | 0.9336 | 0.9529 | 0.9651 |
| 22 | 0.9702 | 0.9836 | 0.9407 | 0.9680 | 0.9048 | 0.9715 | 0.9152 | 0.9382 | 0.9541 |
| 18 | 0.9827 | 0.9905 | 0.9241 | 0.9553 | 0.8880 | 0.9619 | 0.8957 | 0.9223 | 0.9422 |
| 14 | 0.9918 | 0.9954 | 0.9065 | 0.9411 | 0.8708 | 0.9512 | 0.8754 | 0.9055 | 0.9294 |
| 10 | 0.9974 | 0.9985 | 0.8883 | 0.9259 | 0.8536 | 0.9399 | 0.8548 | 0.8882 | 0.9162 |
| 6 | 0.9999 | 0.9998 | 0.8700 | 0.9102 | 0.8367 | 0.9283 | 0.8344 | 0.8708 | 0.9027 |
| 2 | 0.9994 | 0.9998 | 0.8521 | 0.8946 | 0.8202 | 0.9165 | 0.8147 | 0.8537 | 0.8894 |
| 0 | 0.9983 | 0.9993 | 0.8434 | 0.8870 | 0.8122 | 0.9107 | 0.8052 | 0.8455 | 0.8828 |

Table 1. (continued)

| Zenith | Antenna |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| (degrees) | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 |
| 82 | 0.9522 | 0.8640 | 0.9207 | 0.8876 | 0.9462 | 0.9639 | 0.8658 | 0.8628 | 0.7969 |
| 78 | 0.9612 | 0.8789 | 0.9350 | 0.8992 | 0.9560 | 0.9715 | 0.8820 | 0.8808 | 0.8150 |
| 74 | 0.9701 | 0.8943 | 0.9496 | 0.9111 | 0.9656 | 0.9788 | 0.8988 | 0.8997 | 0.8341 |
| 70 | 0.9784 | 0.9098 | 0.9633 | 0.9231 | 0.9746 | 0.9854 | 0.9157 | 0.9185 | 0.8537 |
| 66 | 0.9857 | 0.9250 | 0.9756 | 0.9348 | 0.9827 | 0.9911 | 0.9320 | 0.9365 | 0.8734 |
| 62 | 0.9917 | 0.9396 | 0.9858 | 0.9461 | 0.9895 | 0.9955 | 0.9474 | 0.9532 | 0.8929 |
| 58 | 0.9962 | 0.9532 | 0.9935 | 0.9568 | 0.9947 | 0.9985 | 0.9614 | 0.9679 | 0.9119 |
| 54 | 0.9990 | 0.9655 | 0.9983 | 0.9666 | 0.9982 | 0.9999 | 0.9736 | 0.9802 | 0.9298 |
| 50 | 1.0000 | 0.9762 | 0.9999 | 0.9754 | 0.9998 | 0.9997 | 0.9838 | 0.9897 | 0.9463 |
| 46 | 0.9991 | 0.9851 | 0.9983 | 0.9830 | 0.9995 | 0.9977 | 0.9916 | 0.9961 | 0.9611 |
| 42 | 0.9962 | 0.9921 | 0.9935 | 0.9893 | 0.9971 | 0.9940 | 0.9969 | 0.9993 | 0.9738 |
| 38 | 0.9915 | 0.9969 | 0.9855 | 0.9942 | 0.9928 | 0.9886 | 0.9995 | 0.9991 | 0.9842 |
| 34 | 0.9849 | 0.9995 | 0.9746 | 0.9977 | 0.9866 | 0.9816 | 0.9994 | 0.9955 | 0.9921 |
| 30 | 0.9766 | 0.9998 | 0.9609 | 0.9996 | 0.9786 | 0.9731 | 0.9966 | 0.9886 | 0.9974 |
| 26 | 0.9668 | 0.9980 | 0.9449 | 1.0000 | 0.9689 | 0.9632 | 0.9912 | 0.9787 | 0.9999 |
| 22 | 0.9557 | 0.9940 | 0.9269 | 0.9990 | 0.9578 | 0.9522 | 0.9833 | 0.9659 | 0.9997 |
| 18 | 0.9434 | 0.9881 | 0.9073 | 0.9966 | 0.9455 | 0.9402 | 0.9733 | 0.9508 | 0.9969 |
| 14 | 0.9303 | 0.9804 | 0.8867 | 0.9929 | 0.9323 | 0.9275 | 0.9614 | 0.9338 | 0.9918 |
| 10 | 0.9166 | 0.9713 | 0.8656 | 0.9882 | 0.9184 | 0.9144 | 0.9481 | 0.9154 | 0.9847 |
| 6 | 0.9027 | 0.9613 | 0.8446 | 0.9826 | 0.9043 | 0.9011 | 0.9339 | 0.8965 | 0.9760 |
| 2 | 0.8889 | 0.9507 | 0.8242 | 0.9765 | 0.8903 | 0.8879 | 0.9195 | 0.8777 | 0.9663 |
| 0 | 0.8821 | 0.9454 | 0.8144 | 0.9733 | 0.8835 | 0.8814 | 0.9124 | 0.8687 | 0.9614 |

Table 1. (continued)

| Zenith | Antenna |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| (degrees) | 19 | 20 | 23 | 24 | 25 | 26 | 27 | 28 | "29" |
| 82 | 0.9429 | 0.8513 | 0.9170 | 0.9453 | 0.9696 | 0.8882 | 0.9663 | 0.9309 | 0.9089 |
| 78 | 0.9554 | 0.8713 | 0.9305 | 0.9543 | 0.9774 | 0.9029 | 0.9773 | 0.9417 | 0.9225 |
| 74 | 0.9678 | 0.8925 | 0.9443 | 0.9632 | 0.9847 | 0.9180 | 0.9873 | 0.9526 | 0.9363 |
| 70 | 0.9790 | 0.9138 | 0.9575 | 0.9717 | 0.9910 | 0.9329 | 0.9949 | 0.9631 | 0.9498 |
| 66 | 0.9884 | 0.9342 | 0.9696 | 0.9794 | 0.9959 | 0.9472 | 0.9994 | 0.9728 | 0.9624 |
| 62 | 0.9952 | 0.9528 | 0.9802 | 0.9862 | 0.9990 | 0.9604 | 1.0001 | 0.9813 | 0.9737 |
| 58 | 0.9992 | 0.9690 | 0.9887 | 0.9918 | 1.0001 | 0.9722 | 0.9966 | 0.9885 | 0.9833 |
| 54 | 1.0000 | 0.9821 | 0.9950 | 0.9960 | 0.9991 | 0.9821 | 0.9889 | 0.9940 | 0.9909 |
| 50 | 0.9975 | 0.9918 | 0.9987 | 0.9987 | 0.9959 | 0.9901 | 0.9770 | 0.9978 | 0.9962 |
| 46 | 0.9917 | 0.9976 | 0.9998 | 0.9999 | 0.9904 | 0.9957 | 0.9611 | 0.9997 | 0.9992 |
| 42 | 0.9827 | 0.9994 | 0.9982 | 0.9994 | 0.9827 | 0.9990 | 0.9416 | 0.9996 | 0.9997 |
| 38 | 0.9706 | 0.9972 | 0.9938 | 0.9973 | 0.9730 | 0.9998 | 0.9190 | 0.9975 | 0.9976 |
| 34 | 0.9558 | 0.9909 | 0.9869 | 0.9935 | 0.9614 | 0.9980 | 0.8939 | 0.9935 | 0.9931 |
| 30 | 0.9385 | 0.9808 | 0.9774 | 0.9882 | 0.9481 | 0.9938 | 0.8668 | 0.9876 | 0.9861 |
| 26 | 0.9192 | 0.9671 | 0.9657 | 0.9815 | 0.9334 | 0.9873 | 0.8384 | 0.9800 | 0.9770 |
| 22 | 0.8983 | 0.9503 | 0.9521 | 0.9734 | 0.9175 | 0.9786 | 0.8094 | 0.9708 | 0.9658 |
| 18 | 0.8763 | 0.9309 | 0.9368 | 0.9642 | 0.9007 | 0.9679 | 0.7804 | 0.9602 | 0.9530 |
| 14 | 0.8536 | 0.9096 | 0.9203 | 0.9541 | 0.8834 | 0.9557 | 0.7519 | 0.9485 | 0.9388 |
| 10 | 0.8309 | 0.8870 | 0.9029 | 0.9434 | 0.8659 | 0.9424 | 0.7243 | 0.9361 | 0.9236 |
| 6 | 0.8086 | 0.8642 | 0.8854 | 0.9322 | 0.8485 | 0.9283 | 0.6981 | 0.9232 | 0.9080 |
| 2 | 0.7871 | 0.8420 | 0.8680 | 0.9210 | 0.8316 | 0.9140 | 0.6734 | 0.9103 | 0.8924 |
| 0 | 0.7769 | 0.8315 | 0.8596 | 0.9154 | 0.8234 | 0.9070 | 0.6616 | 0.9039 | 0.8848 |

crosses - fit from Crane (1991) line - fit from this work

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crosses - fit from Crane (1991) line - fit from this work


Zenith Angle (degrees)
FIG. I (CONT'D)

