

National Radio Astronomy Observatory
Socorro, NM

VLA TEST MEMO. 167

NOISE PERFORMANCE OF THE UPGRADED L-BAND SYSTEM

D.S.Bagri
1993Mar05

INTRODUCTION

For VLA L-band sky survey some tests were made during last D-array using new default center frequencies of 1464.9 and 1385.1 MHz with bandwidths of 50 MHz. It has been reported that the resulting images at 1385 MHz had 30% higher noise than those at 1465 MHz. Also there have been reports of increased incidence of external rfi by many VLA L-band users during recent past. Further three quarters of the antennas have now been outfitted with new VLBA design receivers to improve its noise performance. To see (1) whether there is any obvious cause of the higher noise in 1385±25 MHz band compared to 1465±25 MHz band, and (2) noise performance of the upgraded system and compare it with the old one, we decided to measure the system sensitivity over 1360 to 1560 MHz. This memo describes the results of the test measurements.

SYSTEM SENSITIVITY

We measured increase in the system temperature on Virgo-A (3C274) with respect to directions 5° on east and west of it, as a function of frequency for all the antennas in the array. Table 1 gives the average increase in system temperature values on Virgo-A for all the 27 antennas for each of the four IFs (IFs: A, B, C, and D) at various frequencies. Measurements were made with 12.5 MHz backend bandwidth on 1992Dec28, and used backend synchronous detector values. The data show: (1) pre-dawn measurements (starred), made at elevation of about 68° give about 10% higher G/T than those made between 8:18 and 8:42 MST (unstarred) at elevation of about 55° on the monday morning after X-mas weekend, (2) system G/T variation looks smooth with frequency, and peaks at about 1400 MHz, (3) from 1400 MHz to 1553 MHz Virgo-A flux density decreases by about 9 % but the G/T drops by about 20 %, i.e. $(G/T)_{1400\text{MHz}}/(G/T)_{1550\text{MHz}} \approx 1.11$, and (4) average System Equivalent Flux Density (SEFD) = $214/(0.594 * 1.02) = 353$ Jy at 1400 MHz for all 27 antennas (antennas #2 to 28) in the direction of Virgo-A. Lower G/T values for post-dawn measurements may be due to (1) lower elevation (55° instead of 68°) and increased atmospheric contribution due to increase in atmospheric water vapor—observation log comments possible rain in area, (2) Sun in far sidelobes of the antennas, (3) increased rfi — but that has to be present all over the observation frequency range of 1360 to 1560 MHz.

Observations were repeated at night time on 1993Feb01 on Crab and also tipping curves were performed at the same time. Table 2 gives system temperature measurements on Crab for the four IFs averaged over all the 27 antennas. Table 3 gives the average of tipping measurements (azimuth= 0°) at system default frequency settings (center frequencies 1385 and 1465 MHz

and bandwidth=50 MHz) for all the 27 antennas, and average of all four IFs are plotted against secant zenith angle (sec z) in Fig. 1. These measurements lead to basically the same results as those from measurements on 1992Dec28 on Virgo-A. The average SEFD =368 Jy at 1400 MHz is about 15 Jy higher than that for Virgo-A direction, which is consistent with the increased galactic background for the direction of Crab compared to that of the Virgo-A. From table 3 we see that system temperature increases by about 6% at 55° elevation compared with that at 70° elevation. About 10 % increase in the system temperature at 55° elevation compared with that at 68° elevation on 1992Dec28 may have been due to (some) variations in weather between the two sets of measurements (pre-dawn and post-dawn) on a day when there was bad weather (the two sets of measurements were separated in time by more than 2 hours).

Data of table 2 are separated for antennas with upgraded receivers and those with old receivers in tables 4 and 5 respectively. Results of table 4 show that increase in system temperature on Crab with frequency for upgraded antennas is present but it is much more prominent for un-upgraded antennas. For upgraded antennas SEFD at 1400 MHz is about 330 Jy in the direction of Crab compared with 590 Jy for the un-upgraded antennas.

Table 6 gives tipping measurements for 21 upgraded antennas at the system default settings for azimuth= 0°. Average results for all the four IFs are plotted against sec z in Fig. 2. From the tipping results we see that the average T_{sys} value increase by about 44% at elevation of 30° compared to zenith, and more than doubles at elevation of 10° elevation. For good antennas (probably those with low receiver temperatures) the increase is as much as 55% at 30° elevation. From opacity/transparency curves by Schwab and Hogg (MMA Memo. #58, 1989) we see that for the VLA one would expect zenith atmospheric contribution of about 2° K during good weather, and $\leq 3^\circ$ K during fairly poor weather (1.5 cm water). It means the antenna spillover is causing the increase in the T_{sys} values with increasing zenith angle. A quick look at the measured feed patterns suggest that a part of this may very well be accountable by the feed far sidelobes. A rough estimate of the contribution from scattering by the quadrupole legs (based on Landecker et al., 1990-Preprint) gives an increase of only about 4-8° K. Remainder of the increase in the T_{sys} for zenith angles of 20° to 70° is probably due to feed sidelobes.

At least about half of the antennas with upgraded receivers have more than 6 Volts synchronous detector output signal value, which is high. This is due to high injected noise calibration signal which contributes to the system temperature. We should reduce the T_{cal} values to give about 4-5 Volts in the backend Synchronous detectors and about 3 volts in the frontend synchronous detectors. This may reduce the average T_{sys} by a few percent.

NOISE IN IMAGES

To further pursue the problem of increased map noise seen by J. Condon in his snapshots made during the last D-array configuration, I made observations of a field at declination of 88° to have roughly same fringe rates as typical of the D-array. The observations were made in spectral line using all four IFs (VLA observing mode 4) with backend filters of 12.5 MHz over 1360 to 1560 MHz. The data (antenna gains and bandpasses) were calibrated using observations on 3C286. Channel 0 images for both Stokes parameters I and V of size 256X256 were made using HORUS. The peak maximum and minimum in these maps given by HORUS, and number of visibilities used for making the images are listed in table 7 for both I and V maps at various frequencies. The total intensity (I) maps were cleaned using APCLN with number of iterations

(NITER) =1000. The rms noise in the cleaned I and V maps are measured using IMSTAT as listed in table 7. The expected rms image noise is calculated using $S_{rms} = 1.234T_{sys}(Jy)/\sqrt{NtB}$ is also given in the table. The factor 1.234 is due to two bit three level correlator efficiency, $T_{sys}(Jy)$ is system temperature expressed in Jy (assumed =1.25*353 Jy, here 1.25 is due to the increase in the system temperature at 35° elevation compared with that at 70 ° elevation measured for Virgo-A to be 353 Jy —average value for all antennas), N is product of visibilities and polarizations (i.e. rcp and lcp), t is the integration period (=10s), and B is the bandwidth (=9.3 MHz). In these data there is no clear difference between noise over 1385 ±25 MHz band compared to 1465 ±25 MHz band at more than a few % level.

Peak noise in individual 1.5 MHz channel maps (using HORUS) is shown in Fig. 3. There are rfi spikes at 1364.5, 1400, and 1486.4 MHz. Channels in frequency range of 1529.5 to 1544.8 MHz are seriously affected due to external rfi but there is no indication of substantially increased noise in 1385±25 MHz band compared with those in 1465±25 MHz band. From these results (Table 7 and Fig. 3) it seems that at about 0.3 mJy rms noise level in images (for signal bandwidth of 9 MHz) we donot see much difference ($\leq 10 - 15\%$) in sensitivity obtained over any 50 MHz bandwidth in the frequency range of 1360 to 1520 MHz.

For one of the frequency settings (AC: 1396.3±6.25 MHz, BD: 1446.3±6.25 MHz) we split out the channel 0 data for durations of 30 sec, and 2 min from a total of 8 min data. We made images of 30 sec data, 2 min data, and 8 min data using HORUS for both Stokes I and V. The peaks in the images given by HORUS, along with number of visibilities used in making the images, are given in table 8. We cleaned the images using APCLN with NITER=1000. The resulting residuals given by APCLN for the images are given in table 8. Also rms noise the cleaned I and v images measured using IMSTAT are given in the table. Note that 1396.3 MHz channel 0 image contains 1400 MHz frequency where interference is observed. The peak and rms noise for 30 sec, 2 min, and 8 min images go down more rapidly than square root of integration for 1396.3 MHz images but slower than square root of integration period for the 1446.3 MHz images. This is probably due to the fact that narrow band interference for short integrations is likely to reduce more like linearly with the integration, and the 1396.3 MHz images have 1400 MHz birdie. This is probably also the explanation for the higher noise in 1385±25 MHz (which contains 1365 and 1400 MHz birdies) snapshots compared with 1465±25 MHz snapshots made by Condon.

CONCLUSIONS

Upgraded VLA antennas have average SEFD of about 310 Jy at zenith for cold galactic background, and when the system is finally (well) tuned up it may go down somewhat below 300 Jy. Unlike the old system the upgraded system has essentially flat G/T and noise performance (except when the map noise is dominated by rfi) over 1360 to 1560 MHz frequency range. The system temperature increases rapidly with increasing zenith angle (probably due to the feed sidelobes). For finally upgraded (and tuned up) system the increase in the system temperature is likely to be 50% at elevation of 30°, and double at 15° elevation. For short snapshot maps over a frequency band containing rfi the map noise is (probably) dominated by the interference especially for field with low fringe rates (very high declinations) even for A-array.

93 JAN 05 T_{sys} increase on VIRGO-A at L-band (92 DEC 28 data)

Average over Antennas # 2 to 28

| VIRGO S_p (Gp) | FREQ (G) MHz | IF A | IF B | IF C | IF D |
|------------------|--------------|---------|---------|---------|---------|
| 218.3 | 1366 | 1.589 * | 1.554 | 1.597 * | 1.567 |
| | 1378 | 1.597 * | 1.548 | 1.598 * | 1.561 |
| | 1391 | 1.622 * | 1.569 | 1.621 * | 1.578 |
| | 1404 | 1.614 * | 1.564 | 1.615 * | 1.574 |
| | 1416 | 1.559 | 1.562 * | 1.558 | 1.600 * |
| | 1428 | 1.534 | 1.584 * | 1.538 | 1.610 * |
| | 1440 | 1.556 | 1.525 * | 1.552 | 1.608 * |
| | 1453 | 1.546 | 1.580 * | 1.549 | 1.595 * |
| | 1466 | 1.561 * | 1.515 | 1.572 * | 1.534 |
| | 1478 | 1.567 * | 1.523 | 1.590 * | 1.546 |
| | 1491 | 1.560 * | 1.523 | 1.572 * | 1.533 |
| | 1503 | 1.548 * | 1.493 | 1.557 * | 1.515 |
| | 1516 | 1.491 | 1.526 * | 1.516 | 1.548 * |
| | 1528 | 1.493 | 1.532 * | 1.486 | 1.550 * |
| | 1541 | 1.487 | 1.527 * | 1.499 | 1.53 * |
| | 195.6 | 1553 | 1.469 | 1.509 * | 1.464 |

$T_{sys}(G) = \frac{214 \times 10^{-21}}{.595 \times 10^{-2}} = 353.5$

$\Rightarrow T_{sys}(Jy) \sim$

unstarred measurements between 8:18 to 8:40 MST el ~ 55°

* MEASUREMENTS BETWEEN 5:48 to 6:15 " el ~ 68°

Table 1

93 FEB 01

INCREASE IN T_{sys} ON CRAB (EL ~ 70°) for VLA antennas at 20 cm - ALL 27 antennas

| Freq V (MHz) | A | B | C | D | $\frac{A+B+C+D}{4} = R$ |
|-----------------|-------|-------|-------|-------|-------------------------|
| 1366 | 3.494 | 3.480 | 3.460 | 3.571 | 3.501 |
| 1378 | 3.494 | 3.424 | 3.516 | 3.475 | 3.477 |
| 1391 | 3.558 | 3.507 | 3.565 | 3.587 | 3.554 |
| 1404 | 3.605 | 3.507 | 3.601 | 3.578 | 3.573 |
| 1416 | 3.488 | 3.413 | 3.505 | 3.476 | 3.471 |
| 1428 | 3.441 | 3.414 | 3.460 | 3.463 | 3.444 |
| 1440 | 3.531 | 3.484 | 3.554 | 3.578 | 3.536 |
| 1453 | 3.528 | 3.488 | 3.510 | 3.572 | 3.525 |
| 1466 | 3.436 | 3.392 | 3.443 | 3.46 | 3.432 |
| 1478 | 3.512 | 3.446 | 3.561 | 3.561 | 3.520 |
| 1491 | 3.501 | 3.409 | 3.504 | 3.492 | 3.477 |
| 1503 | 3.401 | 3.351 | 3.431 | 3.471 | 3.414 |
| 1516 | 3.388 | 3.344 | 3.44 | 3.443 | 3.404 |
| 1528 | 3.409 | 3.366 | 3.439 | 3.439 | 3.413 |
| 1541 | 3.244 | 3.321 | 3.297 | 3.331 | 3.298 |
| 1553 | 3.346 | 3.286 | 3.349 | 3.301 | 3.321 |

$$T_{sys}(Jy) = \frac{940}{2.56} \sim 368 Jy$$

at 1460 MHz

Table 2

93 FEB 01 INCREASE IN T_{sys} of 21 upgraded L-band Antennas
AT 20 cm ON CRAB ($el \sim 70^\circ$)

| $S_{\nu}(Jy)$ | Freq ν (MHz) | A | B | C | D | $\frac{A+B+C+D}{4}$ |
|---------------|------------------|-------|-------|-------|-------|---------------------|
| 950 | 1366 | 3.779 | 3.749 | 3.724 | 3.852 | 3.776 |
| | 1378 | 3.776 | 3.681 | 3.795 | 3.750 | 3.75 |
| | 1391 | 3.847 | 3.78 | 3.845 | 3.867 | 3.835 |
| | 1404 | 3.883 | 3.751 | 3.89 | 3.868 | 3.848 |
| | 1416 | 3.742 | 3.649 | 3.783 | 3.750 | 3.732 |
| | 1428 | 3.70 | 3.659 | 3.746 | 3.745 | 3.713 |
| | 1440 | 3.797 | 3.729 | 3.850 | 3.881 | 3.814 |
| | 1453 | 3.791 | 3.730 | 3.795 | 3.862 | 3.795 |
| | 1466 | 3.688 | 3.625 | 3.72 | 3.736 | 3.692 |
| | 1478 | 3.787 | 3.701 | 3.861 | 3.862 | 3.803 |
| | 1491 | 3.781 | 3.665 | 3.808 | 3.791 | 3.761 |
| | 1503 | 3.691 | 3.616 | 3.723 | 3.764 | 3.699 |
| | 1516 | 3.669 | 3.604 | 3.747 | 3.752 | 3.701 |
| | 1528 | 3.698 | 3.631 | 3.739 | 3.734 | 3.701 |
| | 1541 | 3.500 | 3.581 | 3.573 | 3.605 | 3.565 |
| 914 | 1553 | 3.62 | 3.572 | 3.638 | 3.597 | 3.609 |

Ave SEFD $\sim 330 Jy$

Table 3

93 FEB 01 INCREASE IN T_{sys} ON 6 NOT upgraded L-Band
Antennas AT 20 cm ON CRAB — (Ant # 2, 6, 9, 12, 16, 17) ($el \sim 70^\circ$)

| Freq ν (MHz) | A | B | C | D | $\frac{R=A+B+C+D}{4}$ |
|------------------|-------|-------|-------|-------|-----------------------|
| 1366 | 2.498 | 2.538 | 2.535 | 2.585 | 2.539 |
| 1378 | 2.507 | 2.525 | 2.543 | 2.513 | 2.522 |
| 1391 | 2.546 | 2.553 | 2.589 | 2.607 | 2.574 |
| 1404 | 2.633 | 2.653 | 2.589 | 2.564 | 2.61 |
| 1416 | 2.596 | 2.586 | 2.529 | 2.514 | 2.556 |
| 1428 | 2.536 | 2.556 | 2.461 | 2.473 | 2.51 |
| 1440 | 2.603 | 2.625 | 2.518 | 2.518 | 2.566 |
| 1453 | 2.606 | 2.642 | 2.512 | 2.555 | 2.579 |
| 1466 | 2.555 | 2.579 | 2.474 | 2.494 | 2.526 |
| 1478 | 2.550 | 2.552 | 2.513 | 2.505 | 2.53 |
| 1491 | 2.521 | 2.512 | 2.439 | 2.444 | 2.479 |
| 1503 | 2.388 | 2.423 | 2.409 | 2.444 | 2.416 |
| 1516 | 2.406 | 2.433 | 2.364 | 2.362 | 2.391 |
| 1528 | 2.395 | 2.439 | 2.391 | 2.402 | 2.407 |
| 1541 | 2.349 | 2.411 | 2.332 | 2.370 | 2.366 |

Table 4
 $T_{sys}(Jy)_{at 1400} = \frac{940}{1.58} \sim 590 Jy$

$\frac{R_{1400}}{R_{1550}} \sim \frac{2.61-1}{2.32-1}$
 $\frac{(G/T)_{1400}}{(G/T)_{1550}} \sim \frac{1.22}{1.03}$

| EL | A | B | C | D | $\frac{A+B+C+D}{4}$ | SEC Z |
|----|-------|-------|-------|-------|---------------------|-------|
| 90 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| 70 | 1.019 | 1.014 | 1.022 | 1.013 | 1.017 | 1.064 |
| 65 | 1.028 | 1.020 | 1.031 | 1.021 | 1.025 | 1.103 |
| 60 | 1.045 | 1.039 | 1.05 | 1.039 | 1.043 | 1.155 |
| 55 | 1.073 | 1.067 | 1.078 | 1.064 | 1.071 | 1.221 |
| 50 | 1.109 | 1.102 | 1.115 | 1.10 | 1.107 | 1.305 |
| 40 | 1.22 | 1.218 | 1.225 | 1.214 | 1.219 | 1.556 |
| 30 | 1.391 | 1.395 | 1.403 | 1.395 | 1.396 | 2.0 |
| 20 | 1.603 | 1.624 | 1.62 | 1.628 | 1.619 | 2.924 |
| 15 | 1.754 | 1.783 | 1.771 | 1.792 | 1.775 | 3.964 |
| 12 | 1.868 | 1.903 | 1.885 | 1.905 | 1.890 | 4.81 |
| 10 | 1.963 | 1.998 | 1.984 | 2.003 | 1.987 | 5.759 |
| 8 | 2.061 | 2.094 | 2.085 | 2.104 | 2.086 | 7.185 |

93 FEB 01 TIPPING Data

02:57 JAT

LOOKING NORTH

AMB TEMP 2.2 °C

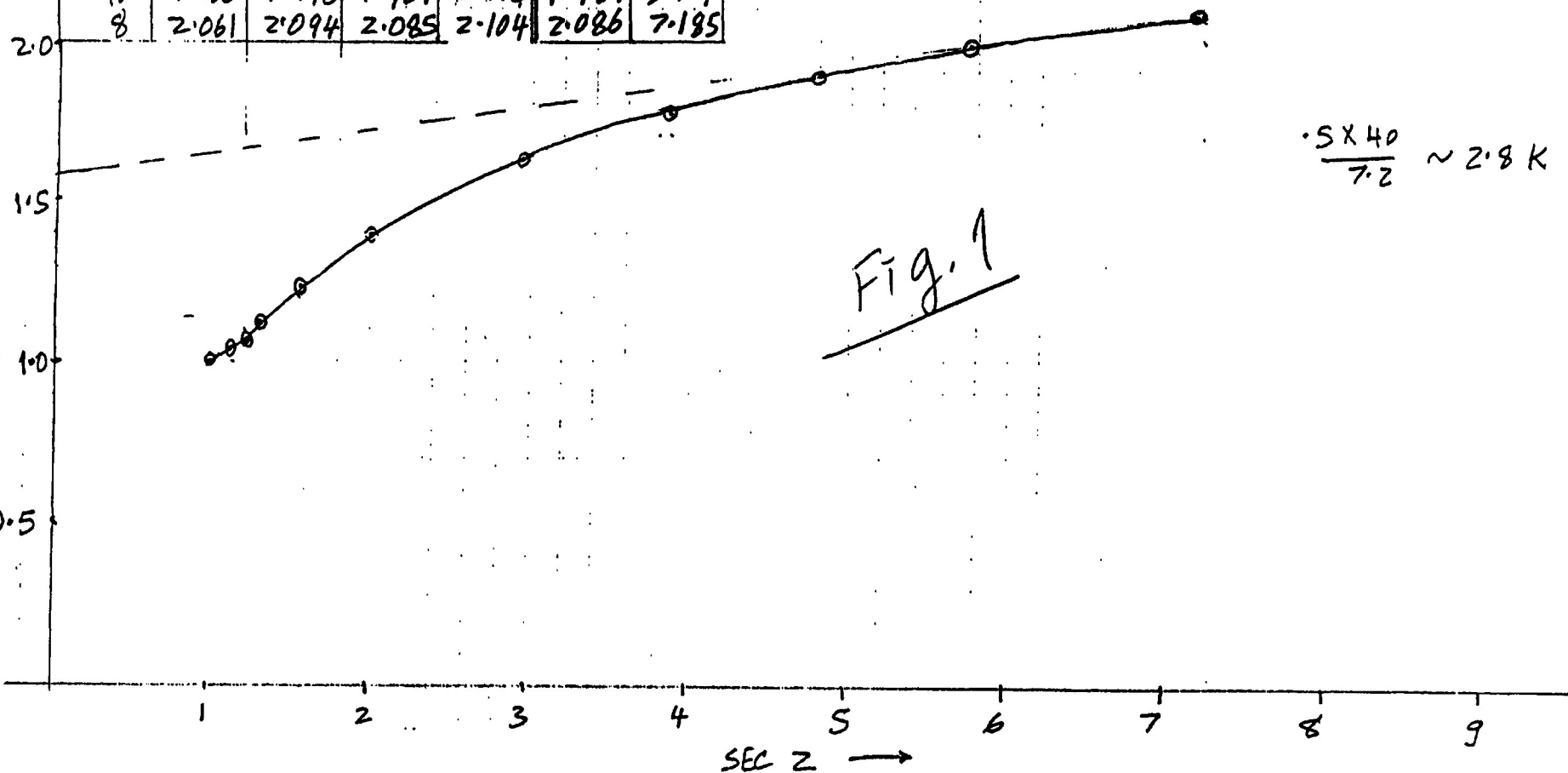
DEW PT 0.1 °C

AC: 1385 MHz / 50

BD: 1465 / 50

Table 5

↑ AVE. T_{SYS} (NORMALIZED TO ZENITH)



$$\frac{.5 \times 40}{7.2} \sim 2.8 \text{ K}$$

Fig. 1

9320209

TIPPING CURVES AT 20 CM ON 21 L-band upgraded antennas -

93 FEB 01 data 02:57 IAT

TIPPING AZ = 0 (NORTH)

AMB-TEMP. = 2.2°C

DEW PT = 0.1°C.

DEFAULT FRER/BW AC 1385/50 MHz
BD 1465/50

| EL | A | B | C | D | AVERAGE 4 | SEC Z |
|-----|-------|-------|-------|-------|--------------|-------|
| 90° | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| 70 | 1.021 | 1.016 | 1.020 | 1.016 | 1.018 | 1.064 |
| 65 | 1.031 | 1.023 | 1.031 | 1.024 | 1.027 | 1.103 |
| 60 | 1.051 | 1.044 | 1.053 | 1.044 | 1.048 | 1.155 |
| 55 | 1.083 | 1.075 | 1.085 | 1.073 | 1.079 | 1.221 |
| 50 | 1.123 | 1.116 | 1.126 | 1.112 | 1.119 | 1.305 |
| 40 | 1.247 | 1.246 | 1.253 | 1.239 | 1.246 | 1.556 |
| 30 | 1.439 | 1.444 | 1.453 | 1.442 | 1.444 | 2.0 |
| 20 | 1.675 | 1.701 | 1.696 | 1.702 | 1.694 | 2.924 |
| 15 | 1.842 | 1.88 | 1.867 | 1.896 | 1.869 | 3.864 |
| 12 | 1.97 | 2.014 | 1.994 | 2.012 | 1.997 | 4.81 |
| 10 | 2.076 | 2.121 | 2.105 | 2.122 | 2.106 | 5.759 |
| 8 | 2.185 | 2.229 | 2.218 | 2.236 | 2.217 | 7.185 |

Table 6

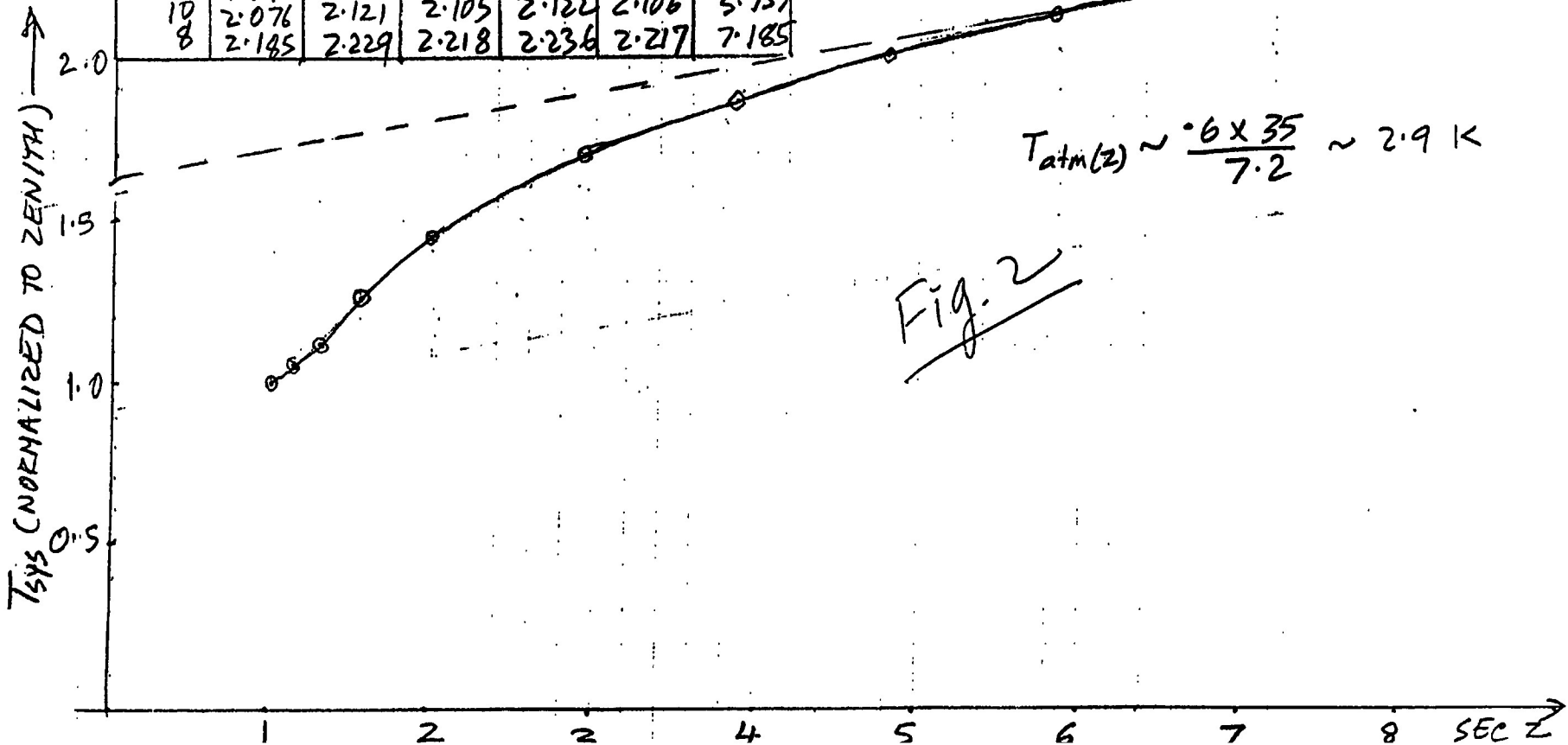


Fig. 2

| FREQUENCY (MHz) CHP: BW=9.3 | IFs | # OF VISIBILITY | I MAP | | V MAP | | EXPECTED RMS (mJy) |
|-----------------------------------|-----|--------------------|---------------------------|----------------------|----------------------------|----------------------|--------------------------|
| | | | HDRUS MIN MAX (mJy) | RMS (*1) (mJy) | HDRUS MIN. MAX (mJy) | RMS (*2) (mJy) | |
| 1366.3 | AC | 15444 | -1.6 2.6 | 338 | -1.4 1.4 | 310 | 312 |
| 1376.3 | AC | 17199 | -1.5 1.1 | 274 | -1.0 1.2 | 260 | 296 |
| 1386.3 | AC | 17199 | -1.6 1.6 | 345 | -1.2 1.2 | 310 | 296 |
| 1396.3 | AC | 17199 | -1.5 1.9 | 306 | -1.7 1.8 | 438 | 296 |
| 1406.3 | AC | 17199 | -1.4 1.4 | 268 | -1.2 1.0 | 268 | 296 |
| 1416.3 | BD | 15444 | -1.9 1.6 | 355 | -1.3 1.4 | 308 | 312 |
| 1426.3 | BD | 17199 | -1.5 1.7 | 286 | -1.1 1.2 | 272 | 296 |
| 1436.3 | BD | 17199 | -1.2 1.5 | 286 | -1.1 1.2 | 258 | 296 |
| 1446.3 | BD | 17199 | -1.3 1.5 | 258 | -1.1 1.2 | 261 | 296 |
| 1456.3 | BD | 17199 | -1.5 1.2 | 260 | -1.2 1.2 | 274 | 296 |
| 1466.3 | AC | 12636 | -1.8 1.6 | 319 | -1.3 1.4 | 299 | 345 |
| 1476.3 | AC | 17199 | -1.3 1.2 | 260 | -1.2 1.1 | 255 | 296 |
| 1486.3 | AC | 17199 | -1.7 1.3 | 338 | -1.4 1.3 | 336 | 296 |
| 1496.3 | AC | 16497 | -1.5 2.0 | 262 | -1.2 1.3 | 268 | 302 |
| 1506.3 | AC | 17199 | -1.9 1.4 | 254 | -1.8 1.4 | 282 | 296 |
| 1516.3 | BD | 12636 | -1.6 1.6 | 299 | -1.3 1.5 | 323 | 345 |
| 1526.3 | BD | 17199 | -6.8 6.8 | 1517 | -6.1 6.6 | 1710 | 296 |
| 1536.3 | BD | 17199 | -11.2 7.5 | 2382 | -11.2 8.6 | 2638 | 296 |
| 1546.3 | BD | 16497 | -4.8 5.1 | 1161 | -3.1 3.7 | 830 | 302 |
| 1556.3 | BD | 17199 | -1.4 1.2 | 256 | -1.5 1.2 | 282 | 296 |

*1 = RMS USING IMSTAT OVER CLEANED MAP USING APLN (NITER=1000)
 *2 = RMS USING IMSTAT OVER V-MAPS

TABLE 7 (Revised 930224PM)

| INTEGRATION DURATION | FREQ/BW (MHz) | # OF VISIBILITIES. | I MAP | | | V MAP | | | |
|----------------------|---------------|--------------------|---------------------------|----------------------|--------------------|--------------------------|----------------------|--------------------|--|
| | | | HORUS PEAK MIN. MAX (mJy) | APCLN PEAK RES (mJy) | RMS (IMSTAT) (uJy) | HORUS PEAK MIN MAX (mJy) | APCLN PEAK RES (mJy) | RMS (IMSTAT) (uJy) | |
| 30 SEC | 1396.3/9.3 | 1053 | -8.8 11.7 | 1947 | 1769 | -8.9 8.5 | 1895 | 2279 | |
| | 1446.3/9.3 | 1053 | -5.9 4.9 | 996 | 912 | -6.1 4.5 | 935 | 1107 | |
| 2 MIN | 1396.3/9.3 | 4212 | -4.9 4.4 | 857 | 819 | -4.2 3.8 | 848 | 989 | |
| | 1446.3/9.3 | 4212 | -2.8 2.8 | 574 | 479 | -2.0 1.9 | 471 | 508 | |
| 8 MIN | 1396.3/9.3 | 17199 | -1.6 1.9 | 388 | 306 | -1.7 1.8 | 429 | 438 | |
| | 1446.3/9.3 | 17199 | -1.4 1.5 | 308 | 262 | -1.1 1.2 | 284 | 268 | |

Table 8 -

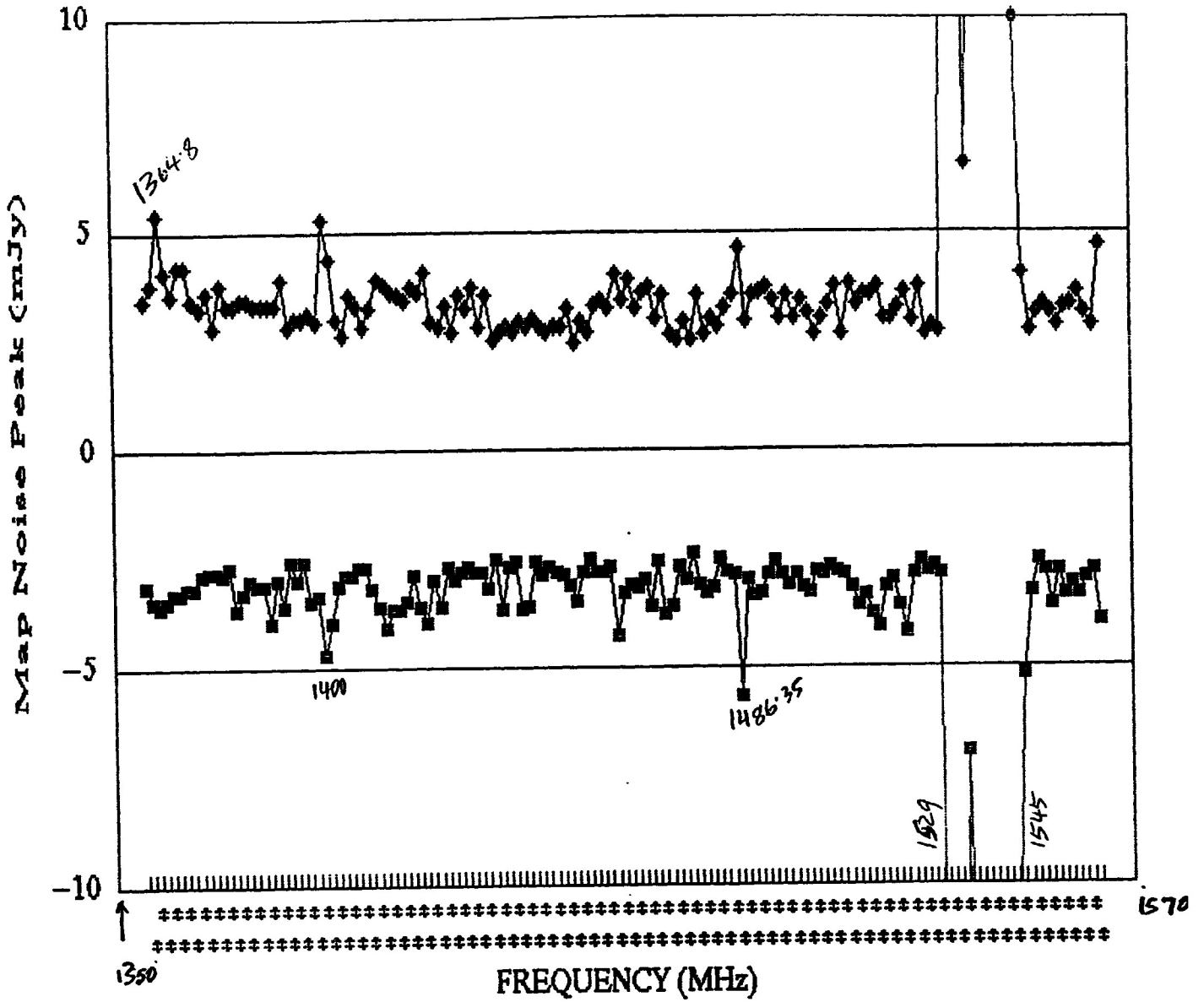


FIG. 3