# National Radio Astronomy Observatory 

Very Large Array

June 15, 1981
THE ESSCO CONTRACT
To: $\quad$ I. W. Findlay, H. Hvatum

From: W. Horne


Subject: Response to Memo \#48

1. Since JWF states in Memo 488 that he proposes to accept in essence ESSCO document D81-15 down to a point 7 lines from the send of rage 13 I feel sure John intends to take the same exception that I have in that I see no justification for computing any overall aggregate RMS. This kind of figure juggling is superflows and is only useful in trying to secure acceptance of a few panels which do not meet the agreed panel RMS which will be written for individual panels. I would prefer to leave to the discretion of the AUI inspector whether or not a few panels which marginally exceed the contract RMS would be accepted.
2. I take exception to the subtraction of the average deviation for a panel from the measured deviation in the computation of the RMS for that panel. If this is permitted it would require that a history of each panel be utilized in panel setting so that the average deviation curve for individual panels are made to coincide with the design curve for the antenna. THis of course could be done by prior calculation of offsets required at the control points during the setting program. My main objection to the subtraction of the average deviation in the compotation of the RMS however is that it brings up the danger of one row of panels having a curvature greater than the design curvature while the other row has a curvature less than the design curvature (due to mold fabrication) yet when the average deviation is subtracted out the panels would meet the specification. We would then have one row of panels with one focal length and the second row with a different focal length. It will be recalled that the 1401 telescope panels were accepted based on a subtraction of the average deviation in RMS compotation and we ended up with focal lengths of 713 inches for inner panels, 717 inches for intermediate panels and 720 inches for the outer panels.
3. On page 13 of the E'SSCO document the statement that $\operatorname{Cos} \theta$ accounts for the fact that the path length change is twice the axial component of the deviation measured perpendicular to the surface is pure baloney. Since the deviation is measured perpendicular to the panel slope angle $\theta$ the actual path length change is twice the measured deviation divided (not multiplied) by the cosine of the slope angle $\theta$.

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4. Note that ESSCO uses tooling holes in both mold and panel which are then used to locate the panel on the measuring machine. These tooling holes must be the prime control points, must have the same antenna coordinates for each type of panel and all other points on the panel are related in the measuring machine to these points.

