THE REFERENCE JIG

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## 1. The Design

The design of the reference jig (RJ), shown in Drawing No. 87D00005, is due to J. Ralston, T. Hame and D. Stone. The drawing shown with this memo is not quite correct. The pin coordinates have been slightly changed; they are correct in Table 3. The jig will have a steel-framed stand to allow it to stand upright and level on the floor.

## 2. The Use of the RJ

The RJ is to be used to check the validity of the measuring template whenever it seems necessary to do this. The template is lifted from its task of setting the surface panels and rested on the RJ (see paragraph 5 of my May 14,1981 memo, No. 36). The template on the RJ will rest on a steel ball close to dowel pin No. 0 and on a surface--yet to be designed--to the right of dowel pin No. 12. The dowel pins 1 through 12 will contact the 12 depth sensors on the template and these sensors will be read (multiplexed) into an Apple computer. The sensor readings will be nominally* identical to those expected when the template rests on a perfect reflector radius.

## 3. The Template/RJ Contact Problem

The template is being designed to carry 12 Schaevitz GCD-121-500 sensors. These give an output over $a \pm 12.7 \mathrm{~mm}$ range of 1 millivolt per $1.27 \mu \mathrm{~m}$ displacement. This range is far greater than we need, but we have used 9 of these sensors in the plate-measuring machine and know how good they are.

We shall mount these sensors so that each is normal to the telescope surface (assumed perfect) at the points given in Table 1 below. (All dimensions are in inches and millimeters--we plan to make the RJ on a machine calibrated in inches.)

* By "nominally" I mean that various small but known differences will in fact exist.

Table 1. The radial distances ( $R$ ) and the vertical distances ( $Z$ ) of the contact points of the 12 template sensors on the telescope (assumed perfect with $f=200.000$ inches).

| Sensor No. | R |  | Z |  | $\begin{gathered} \mathrm{RE} \\ \text { inches } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | inches | mm | Inches | mm |  |
| 1 | 24.2703 | 616.466 | 0.7363 | 18.702 | 24.27 |
| 2 | 46.0861 | 1170.587 | 2.6549 | 67.434 | -- |
| 3 | 67.7677 | 1721.300 | 5.7406 | 145.811 | 70.63 |
| 4 | 89.2576 | 2267.143 | 9.9587 | 252.951 | -- |
| 5 | 110.5052 | 2806.832 | 15.2643 | 387.713 | 111.86 |
| 6 | 131.4674 | 3339.272 | 21.6046 | 548.757 | -- |
| 7 | 152.1089 | 3863.566 | 28.9214 | 734.604 | 151.28 |
| 8 | 154.8478 | 3933.134 | 29.9723 | 761.296 | 154.78 |
| 9 | 175.1852 | 4449.704 | 38.3623 | 974.403 | -- |
| 10 | 195.1498 | 4956.805 | 47.6043 | 1209.149 | 203.38 |
| 11 | 214.7295 | 5454.129 | 57.6360 | 1463.953 | -- |
| 12 | 233.9181 | 5941.520 | 68.3971 | 1737.286 | 234.60 |

The last column of this table gives (RE), the position on the surface directly above the ESSCO adjustment screw attachment nearest to our proposed measurement point.

The panels edges fall at the following radial distances:
Inner panels - Inner edge $=23.98$ inches or 609.1 mm Outer edge $=153.10$ inches or 3888.7 mm

Outer panels - Inner edge $=154.24$ inches or 3892.3 mm Outer edge $=236.2$ inches or 5999.5 mm

I have good reason for choosing this array of sensors (see paragraph 5(c)), so note that sensors Nos. 3, 5, and 10 miss the tops of the nearest adjustment screws by more than 1 inch.

With the template in position on the jig, each sensor will contact its dowel pin as sketched below. Each sensor will contact the surface at normal incidence. We may put a small flat on the end of each sensor probe to make more definite the contact between sensor probe and dowel pin.

4. The RJ Geometry

Finally, I develop Tables 2 and 3 from Table 1, where Table 2 gives the coordinates of the dowel pin centers in the telescope coordinates and also the values of $\theta$ in degrees. Of course, the dowel pin centers do not lie on the exact parabola--we have arranged that the contact points $P$ are on this parabola.

Table 2. The coordinates of the dowel pin centers (in the telescope coordinate system) and the angle $\theta$ in that same system.

| Dowe1 No. | R inches | $\begin{gathered} \mathrm{Z} \\ \text { inches } \end{gathered}$ | $\begin{gathered} \theta \\ \text { degrees } \end{gathered}$ |
| :---: | :---: | :---: | :---: |
| 0 | 0 | 0 | 0 |
| 1 | 24.2930 | 0.7370 | 3.4722 |
| 2 | 46.1290 | 2.6574 | 6.5724 |
| 3 | 67.8303 | 5.7458 | 9.6157 |
| 4 | 89.3393 | 9.9677 | 12.5791 |
| 5 | 110.6051 | 15.2778 | 15.4435 |
| 6 | 131.5845 | 21.6233 | 18.1941 |
| 7 | 152.2422 | 28.9459 | 20.8204 |
| 8 | 154.9832 | 29.9976 | 21.1624 |
| 9 | 175.3356 | 38.3938 | 23.6516 |
| 10 | 195.3142 | 47.6423 | 26.0066 |
| 11 | 214.9069 | 57.6806 | 28.2280 |
| 12 | 234.1074 | 68.4484 | 30.3189 |

In the following Table 3, we list (in inches and in millimeters) the positions of the dowell pin centers in the RJ coordinate system. We have rotated the coordinates through an angle of 17.88595 degrees to put dowels Nos. 1 and 12 at the same $Y$ values*. We have also, in column 5, given the stepping bar lengths (see paragraph 5(c)) for the dowel pin distances we propose to measure by the stepping method.

* The proposal for an RJ is due to $W-Y$. Wong. Not only does it reduce the RJ in size, but it makes the measurement tasks easier.

Table 3. The coordinates of the dowel pin centers in the RJ reference system, and the stepping bar lengths.

Rotation angle $=17.88595$ degrees

| Dowel No. | X |  | Y |  | $\begin{gathered} \text { Step } \\ \text { No. } \\ \hline \end{gathered}$ | StepLengthmm |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | inches | mm | inches | mm |  |  |
| 0 | 0 | 0 | 0 | 0 |  |  |
| 1 | 23.3453 | 592.971 | -6.7596 | -171.694 |  |  |
| 2 | 44.7157 | 1135.779 | -11.6384 | -296.615 | 1-2 | 556.776 |
| 3 | 66.3167 | 1684.444 | -15.3641 | -390.248 | 2-3 | 556.766 |
| 4 | 88.0828 | 2237.303 | -17.9523 | -455.988 | 3-4 | 556.753 |
| 5 | 109.9517 | 2792.773 | -19.4300 | -493.522 | 4-5 | 556.737 |
| 6 | 131.8660 | 3349.396 | -19.8344 | -503.794 | 5-6 | 556.718 |
| 7 | 153.7743 | 3905.867 | -19.2101 | -487.939 | 6-7 | 556.697 |
| 8 | 156.7058 | 3980.327 | -19.0511 | -483.898 |  |  |
| 9 | 178.6532 | 4537.791 | -17.3114 | -439.710 | 8-9 | 559.214 |
| 10 | 200.5067 | 5092.870 | -14.6458 | -372.003 | 9-10 | 559.192 |
| 11 | 222.2354 | 5644.779 | -11.1100 | -282.194 | 10-11 | 559.170 |
| 12 | 243.8150 | 6192.901 | -6.7596 | -171.694 | 11.12 | 559.148 |

## 5. Measuring the RJ

We discuss here briefly the methods available to us to determine the positions of the dowel pins on the RJ.
(a) The machine - We have reason to believe that the machine which bores the dowel pin holes may be in the $\pm 25 \mu \mathrm{~m}$ accuracy range. If so, this gives us an excellent start.
(b) J. Ralston and the NIII optical level - The dowel pin centers are being marked (see "Dowel Pin Detail"). JR will apply his best efforts using our NIII optical level and good distance micrometers to measure the RJ.
(c) Stepping bar measurements - The dowel pins and their positions have been chosen so that JWF can, with a single bar, measure all steps except 0-1 and 7-8. He will treat these separately.

For the first time we have a profile where the bar inclination passes through $0^{\circ}$. We can thus use a stepping bar both ways round and thus remove the (hard to find) zero point angle.
(d) The H-P interferometer - In planning the RJ we have kept in mind the value of this device, and it could well be applied. However, we shall see first how well the other methods agree. the instrument is in the $\$ 50 \mathrm{k}$ cost range and so we would try to rent/borrow one. I believe BNL/Isabelle has one.
6. Accuracy, etc.

As soon as we have an RJ, we shall apply 5(a), 5(b), and 5(c) to it. This will tell us a great deal. We have issued a purchase order for the reference jig--the delivery is about December $1,1981$.


