

THERMAL BEHAVIOR of 12M REFLECTOR STRUCTURE in Green Bank

----- ANALYTICAL RESULTS -----

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There were two questions on July 14, 1982:

- (1) The astigmatism of the rim deflections due to temp. change.
- (2) The "wrong" direction of the rim movement due to temp. increase.

By July 30, 1982, we all agree that the reflector is a well behaved structure (thermally). Some thermal conditions are simulated in the computer and results are given in this memo. for further reference.

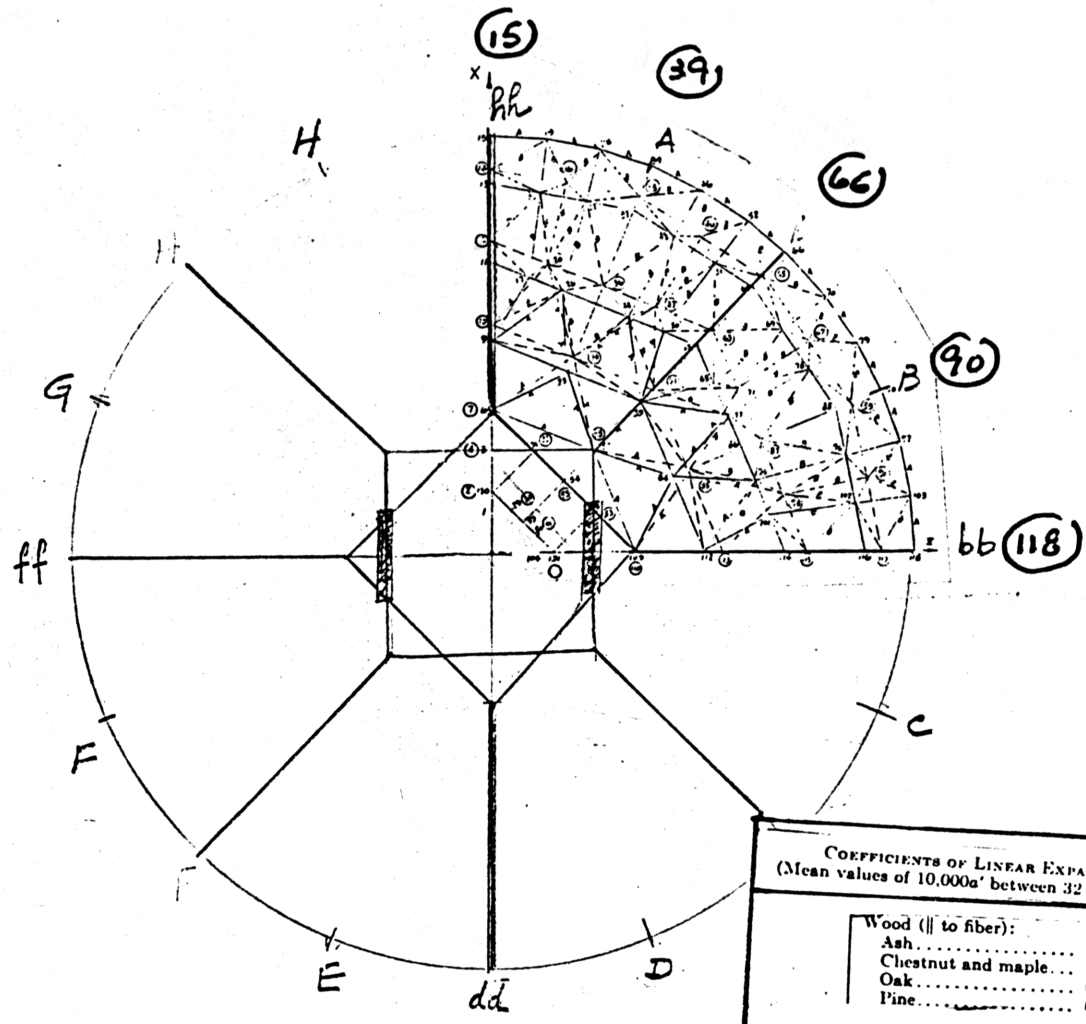
ASTIGMATISM (REF P.3) The supports are constrained at the interfaces with the concrete floor. A 2°C linear temp. distribution ^{in Hub} plus a 5°C uniform temp. increase for the entire structure. The result shows a $\pm 100 \mu\text{m}$ deflections on top of $-48 \mu\text{m}$ average. The tests in July resulted $-186 \pm 50 \mu\text{m}$. The discrepancy may be caused by some slipping at supports during the tests.

RIM MOVEMENTS The results of 4 cases of thermal loadings are given in the following table:

(REF P.4 & P.5)

CASE	UNIT TEMP AT	LINEAR TEMP IN HUB (TOP TO BOTTOM)	AVERAGE REFL. RIM DEFL (STA. ON CONC FLOOR)	
			SUPPORTS CONSTRAINED	SUPPORTS FREE
1	5°C	$5^{\circ}\text{C} - 5^{\circ}\text{C}$	+76 μm	+101 μm
2	5°C	$5^{\circ}\text{C} - 4^{\circ}\text{C}$	+15	+35
3	5°C	$5^{\circ}\text{C} - 3^{\circ}\text{C}$	-48	-33
4	5°C	$5^{\circ}\text{C} - 2^{\circ}\text{C}$	-111	-100

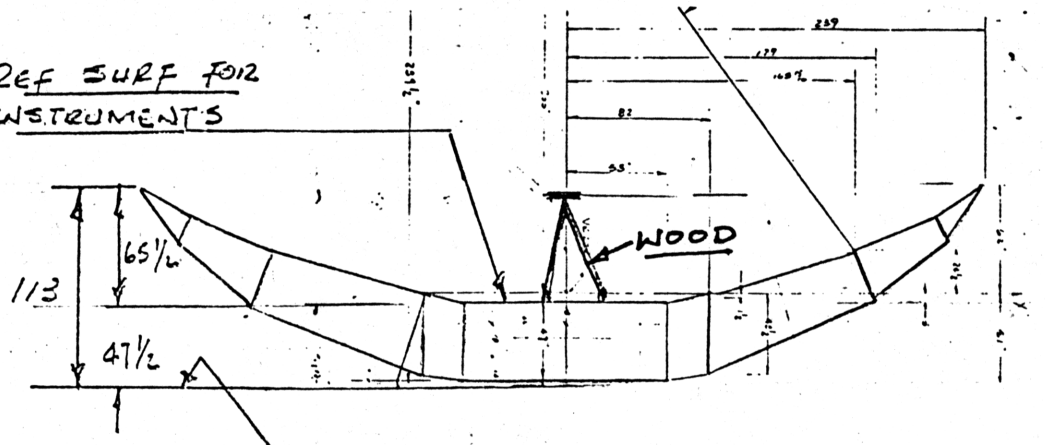
The July 8/9, 1982 tests showed a much higher average rim deflection of $-186 \mu\text{m}$. This may be due to the temperature dependency of the wooden (instrument) tripod.



COEFFICIENTS OF LINEAR EXPANSION
(Mean values of 10,000a' between 32 and 212 F)

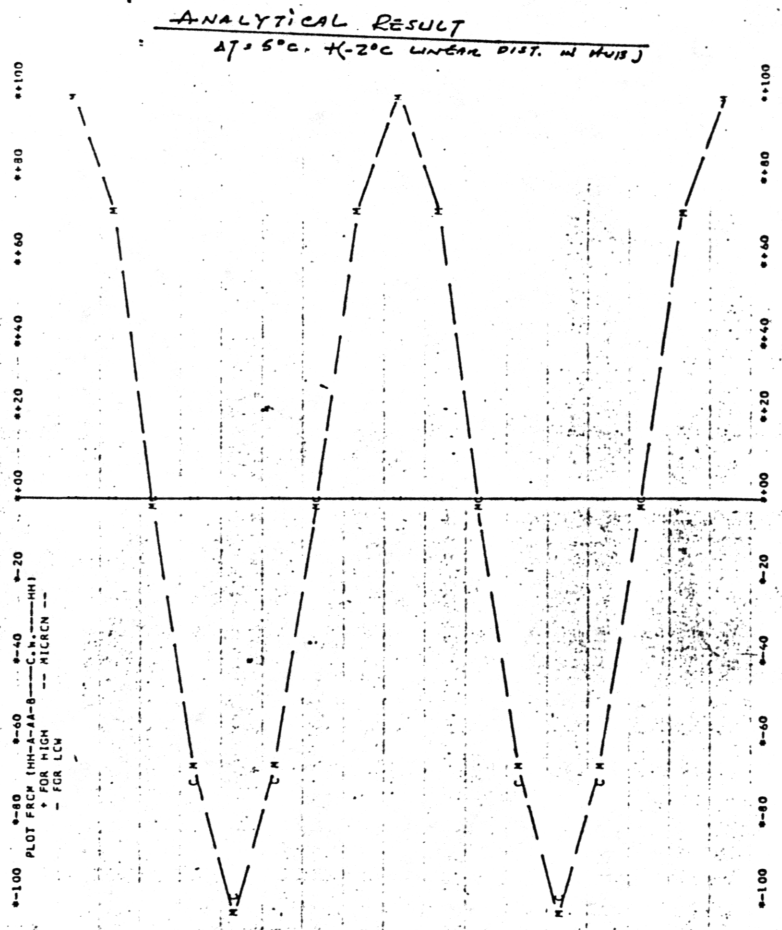
Wood (to fiber):	
Ash.....	0.053
Chestnut and maple.....	0.036
Oak.....	0.027
Pine.....	0.030
Steel:	
Bessemer, rolled hard....	0.056
Bessemer, rolled soft....	0.063
Nickel (10% Ni).....	0.073

REF SURF FOR INSTRUMENTS

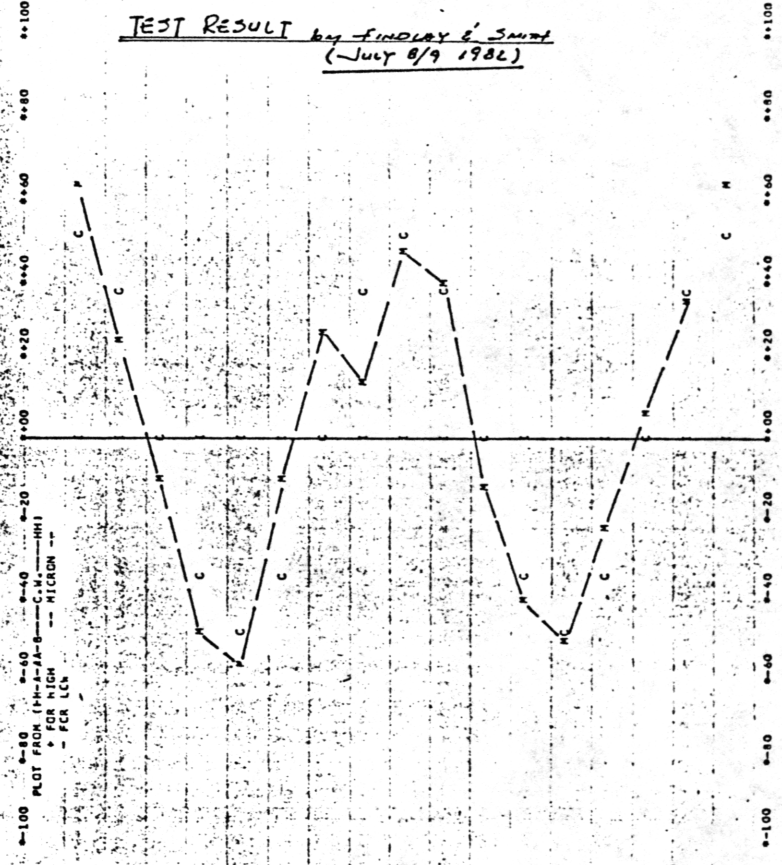


REF SURF FOR COMP. ANALYSIS

12M THERMAL ANALYSIS (1-5 C UNIF + 2 C LINEAR AT HUB)



12M GB JULY 8/9, 1982 (162 - 364) AVG DATA



DISPLACEMENTS
 REAL OUTPUT
 SUBCASE ID #

$\int (\text{Avg } \Delta \text{ ctr. Ring}) = -.00252''$

15	G	-1.441226E-02	-6.513696E-03	0.0
-CONT-		0.0	0.0	-6.721422E-08
39	G	-1.331395E-02	-6.514113E-03	-5.514804E-03
-CONT-		3.330451E-08	2.967318E-09	-7.764237E-08
66	G	-1.019060E-02	-6.513651E-03	-1.019076E-02
-CONT-		4.692894E-08	-1.729793E-09	-5.411200E-08
90	G	-5.514830E-03	-6.513350E-03	-1.231433E-02
-CONT-		6.881629E-08	-2.517274E-09	-3.260083E-08
118	G	0.0	-6.512962E-03	-1.441243E-02
-CONT-		6.443082E-08	0.0	0.0

DISPLACEMENTS
 REAL OUTPUT
 SUBCASE ID #

$\int = .00255''$

15	G	-1.533724E-02	-1.097132E-03	0.0
-CONT-		0.0	0.0	1.469956E-05
39	G	-1.415553E-02	-1.229357E-03	-5.850635E-03
-CONT-		-5.658945E-06	-1.035477E-08	1.420349E-05
66	G	-1.084755E-02	-1.139264E-03	-1.081323E-02
-CONT-		-9.623409E-06	-1.696297E-07	1.098764E-05
90	G	-5.862027E-03	-1.418810E-03	-1.409429E-02
-CONT-		-1.213508E-05	3.052315E-07	6.479270E-06
118	G	0.0	-1.357295E-03	-1.527425E-02
-CONT-		-1.287978E-05	0.0	0.0

DISPLACEMENTS
 REAL OUTPUT
 SUBCASE ID #

$\int = -.00255''$

15	G	-1.487474E-02	-3.805426E-03	0.0
-CONT-		0.0	0.0	7.316074E-06
39	G	-1.373474E-02	-3.871742E-03	-5.682722E-03
-CONT-		-2.832905E-06	-3.741597E-09	7.062831E-06
66	G	-1.051908E-02	-3.826451E-03	-1.050200E-02
-CONT-		-4.788329E-06	8.391635E-08	5.466711E-06
90	G	-5.688429E-03	-3.966063E-03	-1.370431E-02
-CONT-		-6.033214E-06	1.513422E-07	3.223314E-06
118	G	0.0	-3.935110E-03	-1.484335E-02
-CONT-		-6.407763E-06	0.0	0.0

DISPLACEMENTS
 REAL OUTPUT
 SUBCASE ID #

$\int = -.00256''$

15	G	-1.575973E-02	1.611139E-03	0.0
-CONT-		0.0	0.0	2.208292E-05
39	G	-1.457632E-02	1.413008E-03	-6.018549E-03
-CONT-		-8.565045E-06	-1.698559E-08	2.134404E-05
66	G	-1.117602E-02	1.547916E-03	-1.112445E-02
-CONT-		-1.445859E-05	2.553066E-07	1.650846E-05
90	G	-6.035626E-03	1.128452E-03	-1.448426E-02
-CONT-		-1.823707E-05	4.590984E-07	9.735161E-06
118	G	0.0	1.220534E-03	-1.570515E-02
-CONT-		-1.935191E-05	0.0	0.0

DISPLACEMENTS
REAL OUTPUT
SUBCASE ID #

$\delta = -.00286''$

	15	G	4	-1.409332E-02	-1.002704E-02	0.0
-CONT-				0.0	0.0	-2.615033E-05
	39	G		-1.282401E-02	-8.790024E-03	-5.757224E-03
-CONT-				-1.406680E-05	-2.455055E-06	-2.539835E-05
	66	G		-9.826768E-03	-5.988229E-03	-1.069894E-02
-CONT-				-2.384212E-05	-6.640125E-06	-2.305250E-05
	90	G		-5.232436E-02	-2.972153E-03	-1.404261E-02
-CONT-				-2.958422E-05	-3.506925E-06	-1.621737E-05
	118	G		0.0	-1.393963E-03	-1.504182E-02
-CONT-				-3.20E894E-05	0.0	0.0

DISPLACEMENTS
REAL OUTPUT
SUBCASE ID #

$\delta = -.00289''$

	15	G	6	-1.431450E-02	-7.453226E-03	0.0
-CONT-				0.0	0.0	-1.849257E-05
	39	G		-1.309181E-02	-6.285794E-03	-5.913343E-03
-CONT-				-1.692363E-05	-3.358512E-06	-1.801412E-05
	66	G		-1.010232E-02	-3.487530E-03	-1.103656E-02
-CONT-				-2.778375E-05	-6.872217E-06	-1.671551E-05
	90	G		-5.507238E-03	-7.180299E-04	-1.453508E-02
-CONT-				-3.451506E-05	-3.968799E-06	-1.231054E-05
	118	G		0.0	8.040241E-04	-1.564453E-02
-CONT-				-3.702124E-05	0.0	0.0

DISPLACEMENTS
REAL OUTPUT
SUBCASE ID #

$\delta = -.00292''$

	15	G	8	-1.453568E-02	-4.879411E-03	0.0
-CONT-				0.0	0.0	-1.083477E-05
	39	G		-1.335960E-02	-3.781572E-03	-6.069459E-03
-CONT-				-1.978037E-05	-4.341514E-06	-1.062985E-05
	66	G		-1.037787E-02	-9.868473E-04	-1.137418E-02
-CONT-				-3.172531E-05	-7.104286E-06	-1.037852E-05
	90	G		-5.682044E-03	1.536076E-03	-1.502754E-02
-CONT-				-3.944586E-05	-4.430678E-06	-8.403718E-06
	118	G		0.0	3.001995E-03	-1.624723E-02
-CONT-				-4.195349E-05	0.0	0.0

DISPLACEMENTS
REAL OUTPUT
SUBCASE ID #

$\delta = -.00295''$

	15	G	8	-1.475686E-02	-2.305600E-03	0.0
-CONT-				0.0	0.0	-3.176934E-06
	39	G		-1.362740E-02	-1.277353E-03	-6.225571E-03
-CONT-				-2.263710E-05	-5.285299E-06	-3.245543E-06
	66	G		-1.065342E-02	1.513830E-03	-1.171180E-02
-CONT-				-3.566686E-05	-7.336349E-06	-4.041510E-06
	90	G		-5.856846E-03	3.790176E-03	-1.552000E-02
-CONT-				-4.437666E-05	-4.892549E-06	-4.496854E-06
	118	G		0.0	5.199958E-03	-1.684993E-02
-CONT-				-4.688570E-05	0.0	0.0