NATIONAL RADIO ASTRONOMY OBSERVATORY GREEN BANK, WEST VIRGINIA

ELECTRONICS DIVISION INTERNAL REPORT No. 230

256-CHANNEL, 2 MHz PER CHANNEL, FILTER RECEIVER

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Introduction

This report covers the new 256-channel, 2 MHz per channel, filter system, an updated version of the systems described in EDIR No. 146. The general design and construction is the same though most of the printed circuit boards have been changed to accommodate the wider bandwidth and higher frequencies. Figures 1 and 2 show the spectrum processing for the series and parallel modes and the block diagram.

IF Processor Unit

The IF Processor, Figure 3, is used for changing the series spectrum into the parallel mode. Switching between series and parallel is done by a TO-5 relay assembly under control of a TTL signal fed in the back panel. This signal also changes the digital card to accommodate the inverted channel counting in the series mode. The processor schematic shows a small capacitor on the second mixer output line. Other components not shown were added around some of the mixers to suppress the feedthru level to more than 30 dB below the desired output. Extensive shielding was also added.

Oscillator-Multiplier Unit

The two processor associated LO's are generated from a crystal oscillator operating just above 100 MHz followed by three active doublers, a filter and power amplifier. One of these circuits is also shown in Figure 3. Tuned matching circuits are used between multiplier stages, and the final multiplier output is bandpass filtered to provide suppression of the unwanted harmonics. The output amplifier provides +10 dBm to the mixers. During system testing it was discovered that "birdies" were showing up in some channels. Most of these

could be traced to subharmonics of the processor LO's. The filter in the LO's was not doing an adequate job because of its close proximity to the multiplier chain. External filters were added to provide the very high rejection required.

Amplifier-Splitter Unit

The Amplifier-Splitter Unit, Figure 4, contains a 520 MHz low pass filter, amplifier and power splitter for each section. A trap was added to the A section to prevent the 128 MHz difference frequency from generating in-band harmonics in the following amplifier. The 128 MHz is the result of incomplete LO rejection in the first mixer of the processor unit.

Splitter Unit

The Splitter Units are a new design to give adequate gain, match and isolation to 470 MHz. These circuits use a grounded base stage with matching transformer on the output. See Figure 5. Reflection from an out-of-band bandpass filter back into an in-band circuit is down 40 dB or more at other outputs. The very low output VSWR prevents deterioration of the shape of the following bandpass filters.

Oscillator-Mixer Unit

The Oscillator-Mixer Units use circuits similar to the oscillator-multipliers except that only two doublers are required. A representative circuit is shown in Figure 5. A power amplifier and divider furnish +7 dBm to the four mixers. Shunt capacitors and series resistors were added on the mixer inputs to improve the match. Small attenuators on the mixer outputs are chosen to compensate for loss variations in the mixers and all previous units. With levels normalized at this point the filter cards need not be gain trimmed for a particular slot.

Filter Card

The filter cards were redesigned to provide sockets for the op amp and detector diode, provide a new input amplifier and to eliminate ground and power jumpers. The filter and detector circuits are the same except for space for loading the DC side of the detector. See Figures 6 and 7. This loading allows use of some diodes that would otherwise be rejected for poor square law accuracy. The op amps may be either Fairchild μ A 714C or Harris HA-5135-5. The Fairchild unit is equivalent to an OP-07C and the most economical but is available only in a TO-99 can at this time. These units provide an offset temperature coefficient of less than 1.8 μ V/°C compared to 15 μ V/°C for the 741 KN previously used at about the same cost. Some improvement in stability may have been gained by using metal film resistors. Corning type C4 resistors are better than \pm 100 ppm/°C, physically interchangeable with 1/4 W carbon compositions and have better long-term stability at a cost 20% above the molded carbons.

The filter cards operate over the input frequency range of 16 to 48 MHz. At the higher frequencies the signal distribution line down the middle of the board produced a significant standing wave. This problem was eliminated by terminating the line in 43 ohms. This lower impedance increased the signal loss but was offset by a higher gain, wider band input amplifier. See Figure 6. Temperature tests were made on a channel circuit to determine gain instability. The coils measured worse than predicted from data on the core material Unfortunately, the amplifier also drifted in the negative direction. These errors exceed the positive coefficient of the detector by about two times. The first inclination was to compensate one of the stages with a temperature sensitive resistor but a satisfactory type was not found. Also, the compensation required at 48 MHz is considerably higher than at the low end. This would

imply separate and different compensation for each channel, a significant complication. The solution was to provide circuit space for a temperature/frequency compensation network at the output of the input amplifier using a thermistor-capacitor-resistor combination. The necessity for compensation will be determined later.

Monitor Controller Card

The Channel Monitor Digital Controller is unchanged. A schematic and description are given in the previous report. Figure 9 relates channel number to input frequency and card channel number.

Buffer and Monitor Card

The Power Monitor card of the previous system has become the Buffer and Monitor card of this system. In addition to providing single channel or A and B section total power monitoring to the front panel meter and coax jack, it provides simultaneously buffered total power outputs from each card (16 channels summed) to OSM connectors on the back panel. The schematic is given in Figure 8.

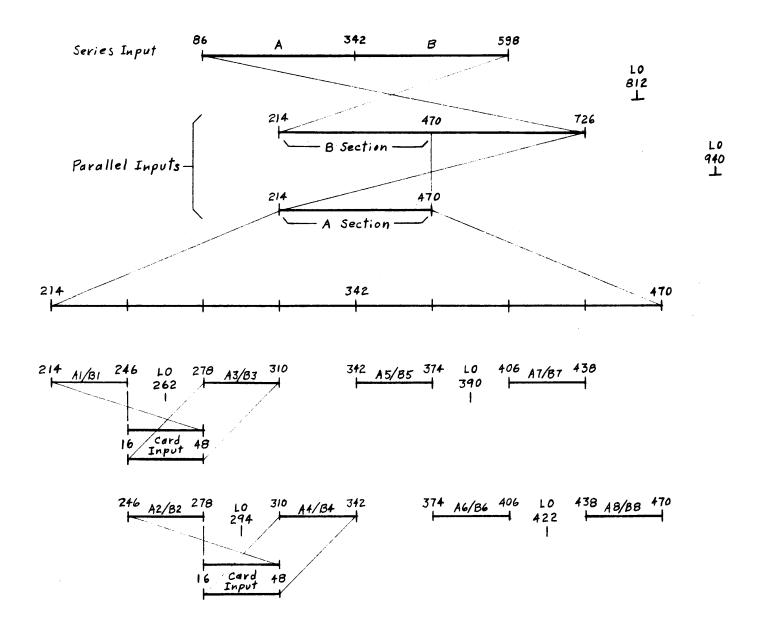
Cost

Since 1973 the cost of components for this system has increased about 1.5X to around \$13,000. The BD4 back diodes were one of the major factors, increasing from \$3.30 to \$8.66 each.

Acknowledgements

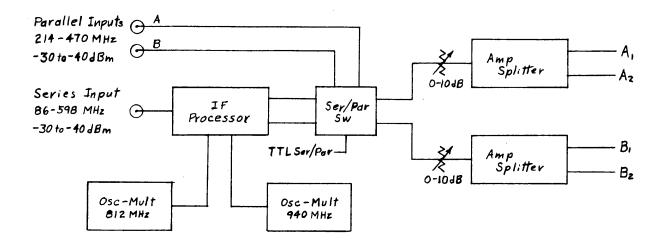
I wish to recognize L. Beale for his construction efforts again.

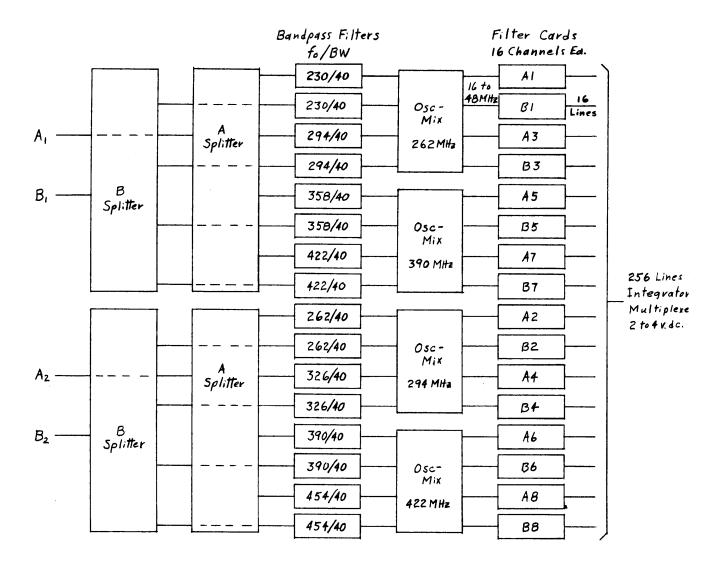
A. Weinreb and R. Lacasse provided an automated square law measuring system to speed up testing and D. Ross and D. Webb were very helpful in arranging for purchase of printed circuit boards and in contracting for the assembly of parts on the filter boards.



SPECTRUM PROCESSING

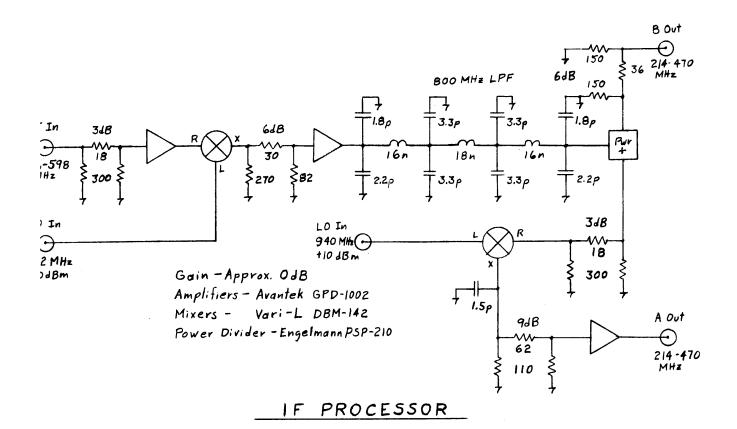
Figure 1

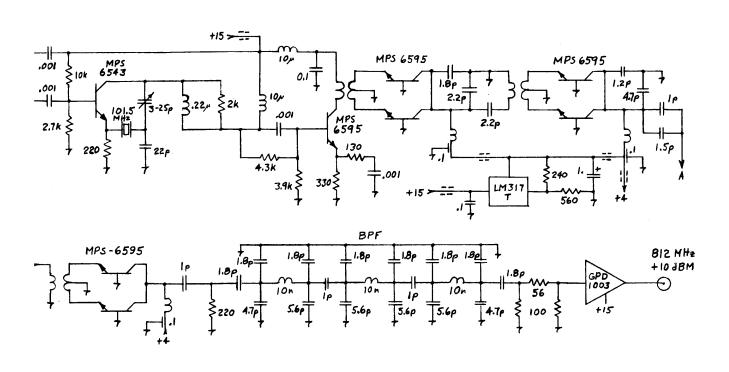




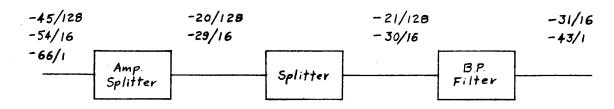
BLOCK DIAGRAM

Figure 2

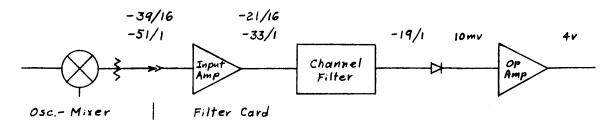




OSCILLATOR - MULTIPLIER



X/x - dBm equiv. per No. of channels



SYSTEM POWER LEVELS

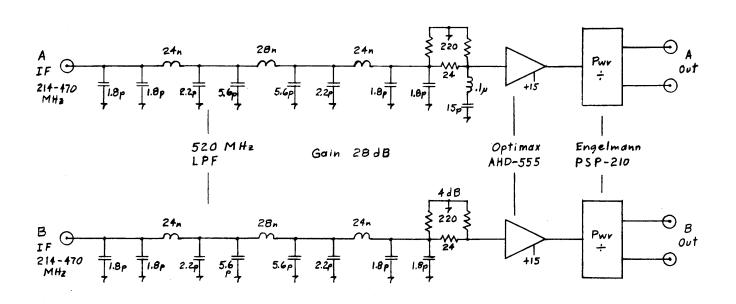
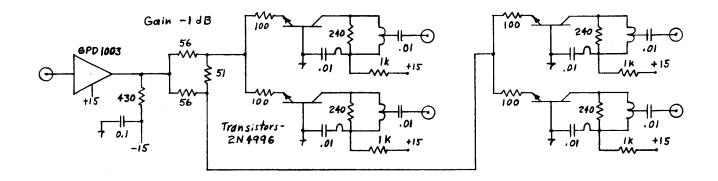
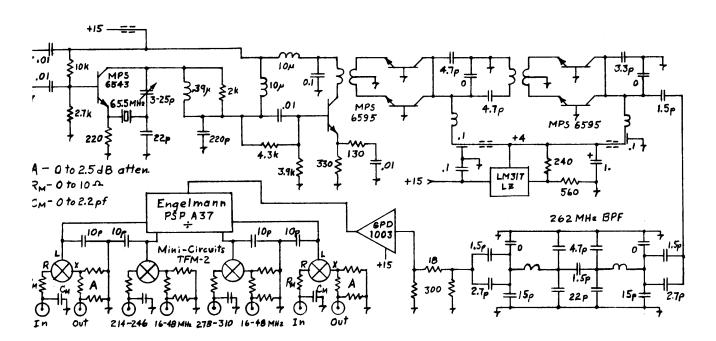


Figure 4

AMPLIFIER - SPLITTER

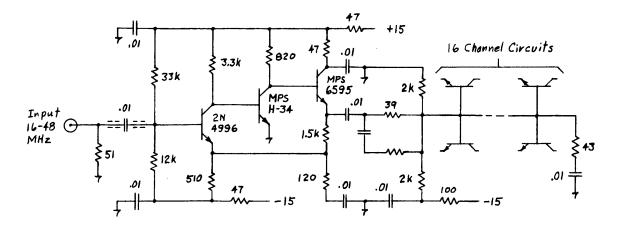


SPLITTER

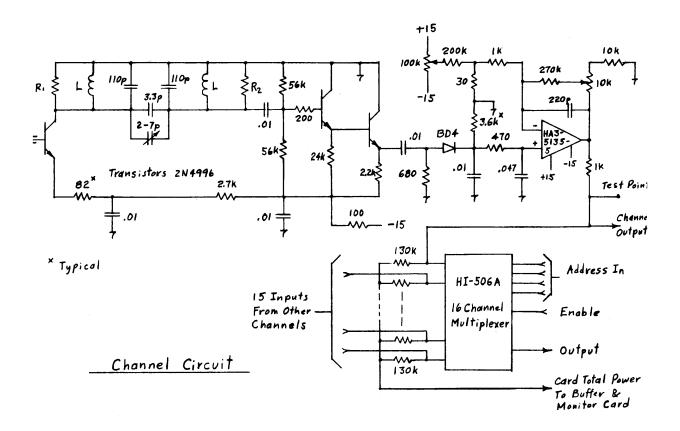


OSCILLATOR - MIXER

Figure 5



Input Amplifier



FILTER CARD

Figure 6

nannel No.	fo MHz	C pf	L pu h	L No. 558-7107-	R _p	R₁ k⊶	R ₂ k-∩-	Cc pf
1	17	110	.716	11	1070	1,3	1.3	9.4
2	19		.578	10			1.3	8.5
3	21		.476	9			1.5	7.6
4	23		.399	8				7.0
5	25		.339	7		1.3		6.4
6	27		.292	6		1.5		5.9
7	29		.254	6				5.5
8	31		.223	5				5.2
9	33		.197	4		1.5	1.5	4.9
10	3 5		.176	4		1.6	1.6	4.6
11	37		.158	3		1.5		4.3
12	39		.142	3		1.6		4.1
13	41		.129	2		1.6	1.6	3.9
14	43		.117	. 2		1.8	1.8	3.7
15	45		.107	1		1.8	1.8	3.6
16	47	011	.098	Į.	1070	1.8	1.8	3.4

CHANNEL FILTER CIRCUIT VALUES

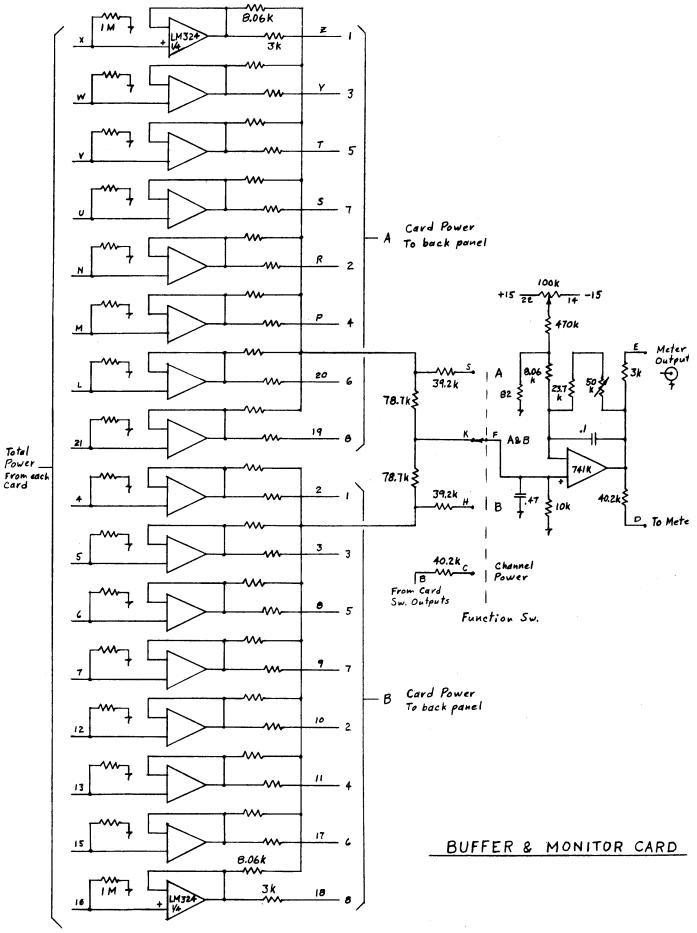


Figure 8

FREQUENCY CHART										
	CHANNEL REC.A	NO. REC.B	PARALLEL	SEF	RIES	PARALLEL	SERIES			
	0	128 129	215.000 217.000	87.000 89.000	343.000	A & B	/ [^] / ⁰ 16			
	2	130	219.000	91.000	345.000 347.000	15	15			
	4	131 132	221.000	93.000 95.000	349.000 351.000	13	13			
	5 6 7	133 134	225.000 227.000	97.000 99.000	353.000 355.000	11	11			
*		135 136	229.000 231.000	101.000	357.000 359.000	AI - 9 BI - 8	B8- 9			
	9 10	137 138	233.000 235.000	105.000	361.000	1 7	;			
	11 12	139 140	237.000	109.000	365.000 367.000	5	5			
	13 14	141 142	241-000	113.000	369.000	3	3			
	15	143	243.000 245.000	117.000	371.000 373.000	2	2			
	16 17	144 145	247.000 249.000	119.000	375.000 377.000	16	1 16			
	18 19	146 147	251.000 253.000	123.000 125.000	379.000 381.000	14	14			
	20 21	148 149	255.000 257.000	127.000	383.000 385.000	12	12			
	22 23	150 151	259.000	131.000	387.000	11	110			
•	24	152	261.000 263.000	133.000 135.000	389.000 391.000	A2- 9 82- 8	B7- 9			
	25 26	153 154	265-000 267-000	137.000 139.000	393.000 395.000	1 7	7			
	27 28	155 156	269.000 271.000	141.000	397.000 399.000		3			
	29 30	157 158	273.000 275.000	147.000	401-000	3	1 3			
	3 1 32	159 160	277.000 279.000	149.000	405.000		<u> </u>			
	33	161	281.000	151.000	407.000 409.000	1	1 2			
	34 35	162 163	283.000 285.000	155.000 157.000	411.000 413.000	3	3 4			
	. 36 37	164	287.000 289.000	159.000 161.000	415.000 417.000	3	5 6			
	38 39	166 167	291.000 293.000	163.000	419.000 421.000	1	7			
	40 41	168 169	295.000	167.000	423.000	B3- 9	B6- 8			
	42	170	297.000 299.000	171-000	425.000 427.000	10	10			
	43 44	171 172	301.000 303.000	173.000 175.000	429.000 431.000	12	12			
	45 46	173 174	305.000 307.000	177.000 179.000	433.000 435.000	14	14			
	47 48	175 176	309.000 311.000	181.000	437.000 439.000	i i	16			
	49 50	177 178	313.000 315.000	185.000	441.000	2	1 1			
	51	179	317-000	187.000	443.000 445.000	3 4	1 3			
	52 53	180 181	319.000 321.000	191.000 193.000	447.000 449.000	5	5			
	54 55	182 183	323.000 325.000	195.000	451.000 453.000	A4- 8	1 ?			
	56 57	184 185	327.000 329.000	199.000 201.000	455.000 457.000	84- 9 10	85- Ş			
	58 59	186 187	331.000 333.000	203.000 205.000	459-000 461-000	11	11			
	60 61	188	335.000	207-000	463.000	12	12			
	62	190	337.000 339.000	209.000 211.000	467.000	14	15			
	63 64	191 192	341.000 343.000	213.000 215.000	469.000 471.000		1 16			
	65	193 194	345.000 347.000	217.000 219.000	473.000 475.000	15	15 14			
	67 68	195 196	349.000 351.000	221.000	477.000	13	13			
	69 70	197 198	353.000 355.000	225.000	481.000 483.000	11	11			
	71 72	199 200	357.000 359.000	229.000	485-000	A5- 9	B4-			
	73 74	201	361-000	233.000	487.000 489.000	85- 8 1 7	ا ا			
	75 76	202	363.000 365.000	235.000 237.000	491.000 493.000	6 5	6 5			
	77	204 205	367.000 369.000	239.000 241.000	495.000 497.000	3	3			
	78 79	206 207	371.000 373.000	243.000 245.000	499.000 501.000	į				
	80 81	208 209	375.000 377.000	247.000	503.000 505.000	16	16			
	82 83	210 211	379.000	251.000	507.000	14	15 14			
	84 85	212	381.000 383.000	253.000 255.000	509.000 511.000	13	13			
	86	213 214	385.000 387.000	257.000 259.000	513.000 515.000	11	11			
	87 88	215 216	389.000 391.000	261-000 263-000	517.000 519.000	A6- 9	B3-			
	89 90	217 218	393.000 395.000	265.000 267.000	521.000 523.000	86- 7 6	7			
	91 92	219 220	397.000 399.000	269.000	525.000	5	5			
	93 94	221 222	401.000	271.000 273.000	527.000 529.000	3	3			
	95 96	223	405-000	275.000 277.000	531.000 533.000	1	· <u> </u>			
	97	224 225	407-000 409-000	279.000 281.000	535.000 537.000	1 2	1 2			
	98 99	226 227	411-000 413-000	283.000 285.000	539.000 541.000	3	3			
	100 101	228 229	415.000 417.000	287.000 289.000	543.000 545.000	3	5			
	102 103	230 231	419.000 421.000	291.000 293.000	547.000 549.000	A7- 8	9			
	104 105	232 233	423-000	295.000	551.000	B7- 9	B2-			
	106	234	425.000 427.000	297.000 299.000	553.000 555.000	10	10			
	107	235 236	429.000 431.000	301.000	557.000 559.000	12	12			
	. 109 110	237 238	433.000 435.000	305.000 307.000	561.000 563.000	14	14			
	111	239 240	437.000 439.000	309.000	565.000 567.000	i	- i6			
	113 114	241 242	441.000 443.000	313.000	569.000 571.000	1 2	2			
	115 116	243 244	445.000 447.000	317.000	573.000	3	3			
	117	245	449.000	319.000 321.000	575.000 577.000	5	5			
	118 119	246 247	451-000 453-000	323.000 325.000	579.000 581.000	A8- 8	7			
	120 121	248 249	455.000 457.000	327.000	583.000 585.000	88- 9 10	BI- 9			
	122 123	250 251	459.000	331.000 333.000	587.000 589.000	11	11			
	124 125	252 253	463.000 465.000	335.000	591.000	13	12			
	126 427	254 255	467.000 469.000	337.000 339.000	593.000 595.000	14	14			
			707000	341.000	597.000	116	16			

Figure 9