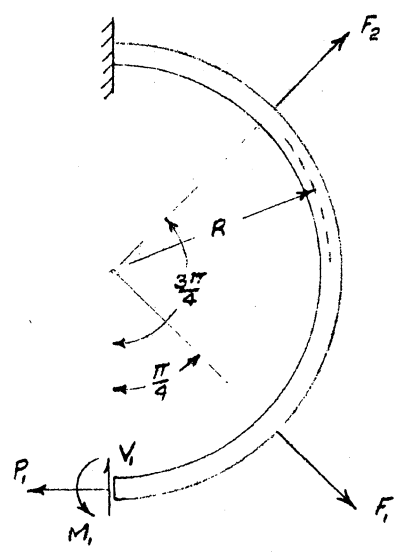


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TITLE
DEFLECTION OF TAIL BEARING STRUCTURE

DEFLECTIONS BY
CASTIGLIANO'S THEOREM



STRAIN ENERGY = U

$$U = \frac{1}{2} \int_0^l \frac{M^2}{EI} ds \quad (\text{APPROX. - USING BENDING MOMENT ONLY})$$

DEFLECTION AT LOAD

$$\delta_F = \frac{\partial U}{\partial F} = \int_0^l \frac{M}{EI} \frac{\partial M}{\partial F} ds \quad (\text{HERE } ds = R d\theta \text{ WITH LIMITS FROM } 0 \text{ TO } \pi)$$

BOUNDARY CONDITIONS

$$\phi = \frac{\partial U}{\partial M_1} = 0$$

$$\delta_{P_1} = \frac{\partial U}{\partial P_1} = 0$$

$$\delta_{V_1} = \frac{\partial U}{\partial V_1} = 0$$

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TITLE <u>DEFLECTION OF TAIL BEARING STRUCTURE</u>		
$\theta = 0 \quad \text{to} \quad \theta = \frac{\pi}{4}$ $M = M_1 - V_1 R \sin \theta - P_1 R (1 - \cos \theta)$ $\frac{\partial M}{\partial M_1} = 1$ $\frac{\partial M}{\partial V_1} = -R \sin \theta$ $\frac{\partial M}{\partial P_1} = -R (1 - \cos \theta)$ $\frac{\partial M}{\partial F_2} = 0$ $\frac{\partial M}{\partial F_1} = 0$		
$\theta = \frac{\pi}{4} \quad \text{to} \quad \theta = \frac{3\pi}{4}$ $M = M_1 - V_1 R \sin \theta - P_1 R (1 - \cos \theta) + F_1 R \sin(\theta - \frac{\pi}{4})$ $\frac{\partial M}{\partial M_1} = 1$ $\frac{\partial M}{\partial V_1} = -R \sin \theta$ $\frac{\partial M}{\partial P_1} = -R (1 - \cos \theta)$ $\frac{\partial M}{\partial F_2} = 0$ $\frac{\partial M}{\partial F_1} = R \sin(\theta - \frac{\pi}{4})$		

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TITLE

DEFLECTION OF TAIL BEARING STRUCTURE

$$\theta = \frac{3\pi}{4} \quad \text{to} \quad \theta = \pi$$

$$M = M_1 - V_1 R \sin \theta - P R (1 - \cos \theta) + F_1 R \sin(\theta - \frac{\pi}{4}) + F_2 R \sin(\theta - \frac{3\pi}{4})$$

$$\frac{\partial M}{\partial M_1} = 1$$

$$\frac{\partial M}{\partial V_1} = -R \sin \theta$$

$$\frac{\partial M}{\partial P} = -R(1 - \cos \theta)$$

$$\frac{\partial M}{\partial F_1} = R \sin(\theta - \frac{\pi}{4})$$

$$\frac{\partial M}{\partial F_2} = R \sin(\theta - \frac{3\pi}{4})$$

SOLVING FOR M_1 IN TERMS OF $V_1, P, F_1, \& F_2$

$$\phi = \frac{\partial U}{\partial M_1} = 0 = \int_0^{\pi} \frac{M}{EI} \frac{\partial M}{\partial M_1} R d\theta$$

$$0 = \int_0^{\pi} \frac{[M_1 - V_1 R \sin \theta - P R (1 - \cos \theta)] [1] R d\theta}{EI}$$

$$+ \int_{\frac{\pi}{4}}^{\pi} \frac{[F_1 R \sin(\theta - \frac{\pi}{4})] R d\theta}{EI}$$

$$+ \int_{\frac{3\pi}{4}}^{\pi} \frac{[F_2 R \sin(\theta - \frac{3\pi}{4})] R d\theta}{EI}$$

BUT

$$\sin(\theta - \frac{\pi}{4}) = (\sin \theta \cos \frac{\pi}{4} - \cos \theta \sin \frac{\pi}{4})$$

AND

$$\sin(\theta - \frac{3\pi}{4}) = (\sin \theta \cos \frac{3\pi}{4} - \cos \theta \sin \frac{3\pi}{4})$$

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TITLE DEFLECTION OF TAIL BEARING STRUCTURE		
<p>SOLVING FOR M_1, IN TERMS OF V_1, P_1, F_1 & F_2 (cont)</p> $0 = \int_0^{\pi} [M_1 - 4RS \sin \theta - P_1 R (1 - \cos \theta)] R d\theta$ $+ \int_{\pi/4}^{\pi} F_1 R [\sin \theta \cos \frac{\pi}{4} - \cos \theta \sin \frac{\pi}{4}] R d\theta$ $+ \int_{\frac{3\pi}{4}}^{\pi} F_2 R [\sin \theta \cos \frac{3\pi}{4} - \cos \theta \sin \frac{3\pi}{4}] R d\theta$ $0 = \left\{ M_1 \pi + 4R \cos \theta - P_1 R (\theta - \sin \theta) \right\}$ $+ \left\{ F_1 R [-\cos \frac{\pi}{4} \cos \theta - \sin \frac{\pi}{4} \sin \theta] \right\}$ $+ \left\{ F_2 R [-\cos \frac{3\pi}{4} \cos \theta - \sin \frac{3\pi}{4} \sin \theta] \right\}$ $0 = \left\{ M_1 \pi - 24R - P_1 R \pi \right\} + \left\{ 0.707 F_1 (2.414) \right\} + \left\{ F_2 R (0.707) (-1 + 0.707 + 0.707) \right\}$ $0 = M_1 \pi - 24R - P_1 R \pi + F_1 R (1.7070) + F_2 R (0.2927)$ $M_1 = \frac{24R}{\pi} + P_1 R - F_1 R \left(\frac{1.7070}{\pi} \right) - F_2 R \left(\frac{0.2927}{\pi} \right)$ $M_1 = \frac{R}{\pi} (24 + P_1 \pi - 1.7070 F_1 - 0.2927 F_2)$		

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DEFLECTION OF TAIL BEARING STRUCTURE

SOLVING FOR V_1 IN TERMS OF P_1 , F_1 & F_2

$$\delta_{V_1} = 0 = \frac{\partial U}{\partial V_1} = \int_0^{\pi} \frac{M \frac{\partial M}{\partial V_1}}{EI} R d\theta$$

$$0 = \int_0^{\pi} [M_1 - V_1 R \sin \theta - P_1 R (1 - \cos \theta)] [-R \sin \theta] R d\theta$$

$$+ \int_{\frac{\pi}{4}}^{\pi} [F_1 R \sin(\theta - \frac{\pi}{4})] [-R \sin \theta] R d\theta$$

$$+ \int_{\frac{3\pi}{4}}^{\pi} [F_2 R \sin(\theta - \frac{3\pi}{4})] [-R \sin \theta] R d\theta$$

$$0 = \int_0^{\pi} [-M_1 R \sin \theta + V_1 R \sin^2 \theta + P_1 R (\sin \theta - \frac{1}{2} \sin 2\theta)] d\theta$$

$$+ \int_{\frac{\pi}{4}}^{\pi} F_1 R [-\cos \frac{\pi}{4} \sin^2 \theta + \sin \frac{\pi}{4} (\frac{1}{2} \sin 2\theta)] d\theta$$

$$+ \int_{\frac{3\pi}{4}}^{\pi} F_2 R [-\cos \frac{3\pi}{4} \sin^2 \theta + \sin \frac{3\pi}{4} (\frac{1}{2} \sin 2\theta)] d\theta$$

$$0 = \left\{ M_1 \cos \theta + V_1 R (\frac{1}{2} \theta - \frac{1}{4} \sin 2\theta) + P_1 R (-\cos \theta + \frac{1}{4} \cos 2\theta) \right\}$$

$$+ \left\{ F_1 R [-\cos \frac{\pi}{4} (\frac{1}{2} \theta - \frac{1}{4} \sin 2\theta) + \sin \frac{\pi}{4} (\frac{1}{4} \cos 2\theta)] \right\}$$

$$+ \left\{ F_2 R [-\cos \frac{3\pi}{4} (\frac{1}{2} \theta - \frac{1}{4} \sin 2\theta) + \sin \frac{3\pi}{4} (\frac{1}{4} \cos 2\theta)] \right\}$$

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DEFLECTION OF TAIL BEARING STRUCTURE

SOLVING FOR V_1 IN TERMS OF P , F_1 & F_2 (Cmc)

$$0 = -2M_1 + V_1 R \left(\frac{\pi}{2} - 0 \right) + P_1 R \left(2 + \frac{1}{4} - \frac{1}{4} \right) + F_1 R \left[(0.707) \left(\frac{3\pi}{8} + \frac{1}{4} \right) - (0.707) \left(\frac{1}{4} - 0 \right) \right] + F_2 R \left[+0.707 \left(\frac{\pi}{8} - 0 - \frac{1}{4} - \frac{1}{4} \right) \right]$$

$$0 = -2M_1 + V_1 R \frac{\pi}{2} + 2P_1 R + F_1 R (-1.1864) + F_2 R (-0.0759)$$

$$M_1 = \frac{R}{\pi} (2V_1 + P_1 \pi - 1.7070 F_1 - 0.2927 F_2)$$

SUBSTITUTING

$$0 = -\frac{2R}{\pi} (2V_1 + P_1 \pi - 1.7070 F_1 - 0.2927 F_2) + V_1 R \frac{\pi}{2} + 2P_1 R + F_1 R (-1.1864) + F_2 R (-0.0759)$$

$$0 = -V_1 \left(\frac{4R}{\pi} - \frac{R\pi}{2} \right) + P_1 (2R - 2R) + F_1 \left(\frac{3.414R}{\pi} - 1.1864R \right) + F_2 (0.1863R - 0.0759R)$$

$$0 = -V_1 (-0.2984) - 0.0997 F_1 + 0.1104 F_2$$

$$V_1 = 0.3341 F_1 - 0.3700 F_2$$

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SOLVING FOR P_1 IN TERMS OF F_1 & F_2 .

$$\delta_{P_1} = 0 = \frac{\partial U}{\partial P_1} = \int_0^{\pi} \frac{M \frac{\partial M}{\partial P_1}}{EI} R d\theta$$

$$0 = \int_0^{\pi} [M_1 - V_1 R \sin \theta - P_1 R (1 - \cos \theta)] [-R (1 - \cos \theta)] R d\theta$$

$$+ \int_{\frac{\pi}{4}}^{\pi} F_1 R [\sin(\theta - \frac{\pi}{4})] [-R (1 - \cos \theta)] R d\theta$$

$$+ \int_{\frac{3\pi}{4}}^{\pi} F_2 R [\sin(\theta - \frac{3\pi}{4})] [-R (1 - \cos \theta)] R d\theta$$

$$0 = \int_0^{\pi} [-M_1 (1 - \cos \theta) + V_1 R (\sin \theta - \frac{1}{2} \sin 2\theta) + P_1 R (1 - 2 \cos \theta + \cos^2 \theta)] d\theta$$

$$+ \int_{\frac{\pi}{4}}^{\pi} F_1 R [-\cos \frac{\pi}{4} (\sin \theta - \frac{1}{2} \sin 2\theta) + \sin \frac{\pi}{4} (\cos \theta - \cos^2 \theta)] d\theta$$

$$+ \int_{\frac{3\pi}{4}}^{\pi} F_2 R [-\cos \frac{3\pi}{4} (\sin \theta - \frac{1}{2} \sin 2\theta) + \sin \frac{3\pi}{4} (\cos \theta - \cos^2 \theta)] d\theta$$

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<p>SOLVING FOR P IN TERMS OF F & F₂ (Cont.)</p> $0 = \int_0^{\pi} -M_1(\theta - \sin\theta) + V_1 R(-\cos\theta + \frac{1}{4} \cos 2\theta) + P_1 R(\theta - 2\sin\theta + \frac{1}{2}\theta + \frac{1}{4} \sin 2\theta) \left\{ \right.$ $+ \left. \int_{\frac{\pi}{4}}^{\pi} F_1 R \left[\cos \frac{\pi}{4} (-\cos\theta + \frac{1}{4} \cos 2\theta) + \sin \frac{\pi}{4} (\sin\theta - \frac{1}{2}\theta - \frac{1}{4} \sin 2\theta) \right] \right\}$ $+ \left. \int_{\frac{3\pi}{4}}^{\pi} F_2 R \left[\cos \frac{3\pi}{4} (-\cos\theta + \frac{1}{4} \cos 2\theta) + \sin \frac{3\pi}{4} (\sin\theta - \frac{1}{2}\theta - \frac{1}{4} \sin 2\theta) \right] \right\}$ $0 = \left\{ -M_1(\pi - 0) + V_1 R(2 + \frac{1}{4} - \frac{1}{4}) + P_1 R(\frac{3}{2} \pi) \right\}$ $+ \left\{ F_1 R \left[0.707(1 + 0.707 + \frac{1}{4}) + 0.707(-0.707 - \frac{3\pi}{8} + \frac{1}{4}) \right] \right\}$ $+ \left\{ F_2 R \left[0.707(1 - 0.707 + \frac{1}{4} - 0) + 0.707(0.707 - \frac{\pi}{8} - \frac{1}{4}) \right] \right\}$ $0 = -M_1 \pi + 2V_1 R + \frac{3}{2} \pi P_1 R - 2.5396 F_1 R - 0.5703 F_2 R$ <p><u>SUBSTITUTING FOR M₁</u></p> $0 = -R(2V_1 + P_1 \pi - 1.7070 F_1 - 0.2927 F_2) + 2V_1 R + \frac{3}{2} \pi P_1 R$ $- 2.5396 F_1 R - 0.5703 F_2 R$ $0 = \frac{\pi}{2} P_1 - 0.8330 F_1 - 0.2776 F_2$ $P_1 = 0.5303 F_1 - 0.1967 F_2$		

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$\delta_{F_2} = \frac{\partial U}{\partial F_2} = \int_0^{\pi} \frac{M}{EI} \frac{\partial M}{\partial F_2} R d\theta$ $\delta_{F_2} = \frac{1}{EI} \int_0^{\frac{\pi}{4}} [M_1 - UR \sin \theta - PR(1 - \cos \theta)] [0] R d\theta$ $+ \frac{1}{EI} \int_{\frac{\pi}{4}}^{\frac{3\pi}{4}} [M_1 - UR \sin \theta - PR(1 - \cos \theta) + FR \sin(\theta - \frac{\pi}{4})] [0] R d\theta$ $+ \frac{1}{EI} \int_{\frac{3\pi}{4}}^{\pi} [M_1 - UR \sin \theta - PR(1 - \cos \theta) + FR \sin(\theta - \frac{\pi}{4}) + \frac{1}{2} R \sin(\theta - \frac{3\pi}{4})] [R \sin(\theta - \frac{3\pi}{4})] R d\theta$ $\delta_{F_2} = \frac{R^2}{EI} \int_{\frac{3\pi}{4}}^{\pi} \left\{ M_1 (\cos \frac{3\pi}{4} \sin \theta - \sin \frac{3\pi}{4} \cos \theta) - UR (\cos \frac{3\pi}{4} \sin^2 \theta - \frac{1}{2} \sin \frac{3\pi}{4} \sin 2\theta) \right.$ $- PR [\cos \frac{3\pi}{4} (\sin \theta - \frac{1}{2} \sin 2\theta) - \sin \frac{3\pi}{4} (\cos \theta - \cos^2 \theta)]$ $+ FR [\cos \frac{3\pi}{4} \cos \frac{\pi}{4} \sin^2 \theta - \frac{1}{2} \cos \frac{3\pi}{4} \sin \frac{\pi}{4} \sin 2\theta - \frac{1}{2} \cos \frac{\pi}{4} \sin \frac{3\pi}{4} \sin 2\theta$ $\left. + \sin \frac{3\pi}{4} \sin \frac{\pi}{4} \cos^2 \theta \right\} d\theta$ $+ \frac{1}{2} R [\cos^2 \frac{3\pi}{4} \sin^2 \theta - \cos \frac{3\pi}{4} \sin \frac{3\pi}{4} \sin 2\theta + \sin^2 \frac{3\pi}{4} \cos^2 \theta]$		

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$$\delta_{F_2} = \frac{R^2}{EI} \left\{ M_1 \left(\cos \frac{3\pi}{4} \cos \theta - \sin \frac{3\pi}{4} \sin \theta \right) - V_1 R \left[\cos \frac{3\pi}{4} \left(\frac{1}{2} \theta - \frac{1}{4} \sin 2\theta \right) + \frac{1}{4} \sin \frac{3\pi}{4} \cos 2\theta \right] - P_1 R \left[\cos \frac{3\pi}{4} \left(-\cos \theta + \frac{1}{4} \cos 2\theta \right) - \sin \frac{3\pi}{4} \left(\sin \theta - \frac{1}{2} \theta - \frac{1}{4} \sin 2\theta \right) + F_1 R \left[\cos \frac{3\pi}{4} \cos \frac{\pi}{4} \left(\frac{1}{2} \theta - \frac{1}{4} \sin 2\theta \right) + \frac{1}{4} \cos \frac{3\pi}{4} \sin \frac{\pi}{4} \cos 2\theta + \frac{1}{4} \cos \frac{\pi}{4} \sin \frac{3\pi}{4} \cos 2\theta + \sin \frac{3\pi}{4} \sin \frac{\pi}{4} \left(\frac{1}{2} \theta + \frac{1}{4} \sin 2\theta \right) \right] + F_2 R \left[\cos^2 \frac{3\pi}{4} \left(\frac{1}{2} \theta - \frac{1}{4} \sin 2\theta \right) + \frac{1}{2} \cos \frac{3\pi}{4} \sin \frac{3\pi}{4} \cos 2\theta + \sin^2 \frac{3\pi}{4} \left(\frac{1}{2} \theta + \frac{1}{4} \sin 2\theta \right) \right] \right\}$$

$$\delta_{F_2} = \frac{R^2}{EI} \left\{ M_1 \left[(0.707)(-1+0.707) - 0.707(0-0.707) \right] - V_1 R \left[(-0.707) \left(\frac{\pi}{8} - \frac{1}{4} \right) + 0.707 \left(\frac{1}{4} \right) \right] - P_1 R \left[-0.707 \left(1-0.707 + \frac{1}{4} - 0 \right) - 0.707 \left(0-0.707 - \frac{\pi}{8} - \frac{1}{4} \right) \right] + F_1 R \left[-0.500 \left(\frac{\pi}{8} - \frac{1}{4} \right) - 0.500 \left(\frac{1}{4} - 0 \right) + 0.500 \left(\frac{1}{4} - 0 \right) + 0.500 \left(\frac{\pi}{8} + 0 + \frac{1}{4} \right) \right] + F_2 R \left[0.500 \left(\frac{\pi}{8} - 0 - \frac{1}{4} \right) - 0.500 \left(\frac{1}{2} - 0 \right) + 0.500 \left(\frac{\pi}{8} + 0 + \frac{1}{4} \right) \right] \right\}$$

$$\delta_{F_2} = \frac{R^2}{EI} \left\{ 0.2927 M_1 - 0.0759 V_1 R - 0.5703 P_1 R + 0.2500 F_1 R + 0.1427 F_2 R \right\}$$

Substituting for M_1

$$\delta_{F_2} = \frac{R^2}{EI} \left\{ \frac{0.2927 R}{\pi} (2\psi + P_1 \pi - 1.7070 F_1 - 0.2927 F_2) - 0.0759 V_1 R - 0.5703 P_1 R + 0.2500 F_1 R + 0.1427 F_2 R \right\}$$

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DEFLECTION OF TAIL BEARING STRUCTURE

$$S_{F_2} = \frac{R^3}{EI} \left\{ +0.1104 V_1 - 0.2776 F_1 + 0.0910 F_2 + 0.1154 F_2 \right\}$$

SUBSTITUTING FOR V_1 & F_1

$$S_{F_2} = \frac{R^3}{EI} \left\{ -0.0193 F_1 + 0.0256 F_2 \right\}$$

$$S_{F_1} = \frac{\partial U}{\partial F_1} = \int_0^{\pi} \frac{M}{EI} \frac{\partial M}{\partial F_1} R d\theta$$

$$S_{F_1} = \frac{1}{EI} \int_0^{\frac{\pi}{4}} [M_1 - V_1 R \sin \theta - P R (1 - \cos \theta)] [0] R d\theta$$

$$+ \frac{1}{EI} \int_{\frac{\pi}{4}}^{\pi} [M_1 - V_1 R \sin \theta - P R (1 - \cos \theta) + F_1 R \sin(\theta - \frac{\pi}{4})] [R \sin(\theta - \frac{\pi}{4})] R d\theta$$

$$+ \frac{1}{EI} \int_{\frac{3\pi}{4}}^{\pi} [F_2 R \sin(\theta - \frac{3\pi}{4})] [R \sin(\theta - \frac{\pi}{2})] R d\theta$$

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$\delta_F = \frac{R^2}{EI} \int_{\frac{\pi}{4}}^{\pi} \left\{ M_1 (\sin \theta \cos \frac{\pi}{4} - \cos \theta \sin \frac{\pi}{4}) - 4R (\cos \frac{\pi}{4} \sin^2 \theta - \frac{1}{2} \sin \frac{\pi}{4} \sin 2\theta) \right.$ $- PR \left[(\cos \frac{\pi}{4}) (\sin \theta - \frac{1}{2} \sin 2\theta) - \sin \frac{\pi}{4} (\cos \theta - \cos^2 \theta) \right]$ $+ FR \left[\cos^2 \frac{\pi}{4} \sin^2 \theta - \sin \frac{\pi}{4} \cos \frac{\pi}{4} \sin 2\theta + \sin^2 \frac{\pi}{4} \cos^2 \theta \right] \Big\} d\theta$ $+ \frac{R^2}{EI} \int_{\frac{3\pi}{4}}^{\pi} \left\{ \frac{1}{2} R \left[\cos \frac{\pi}{4} \cos \frac{3\pi}{4} \sin^2 \theta - \frac{1}{2} \cos \frac{\pi}{4} \sin \frac{3\pi}{4} \sin 2\theta - \frac{1}{2} \sin \frac{\pi}{4} \cos \frac{3\pi}{4} \sin 2\theta \right. \right.$ $\left. \left. + \sin \frac{\pi}{4} \sin \frac{3\pi}{4} \cos^2 \theta \right] \right\} d\theta$ $\delta_F = \frac{R^2}{EI} \int_{\frac{\pi}{4}}^{\pi} \left\{ M_1 (\cos \frac{\pi}{4} \cos \theta - \sin \frac{\pi}{4} \sin \theta) - 4R (\cos \frac{\pi}{4}) (\frac{1}{2} \theta - \frac{1}{4} \sin 2\theta) \right.$ $+ \frac{1}{4} \sin \frac{\pi}{4} \cos 2\theta \Big\} - PR \left[\cos \frac{\pi}{4} (-\cos \theta + \frac{1}{4} \cos 2\theta) \right.$ $- \sin \frac{\pi}{4} (\sin \theta - \frac{1}{2} \theta - \frac{1}{4} \sin 2\theta) \Big] + FR \left[\cos^2 \frac{\pi}{4} (\frac{1}{2} \theta - \frac{1}{4} \sin 2\theta) \right.$ $\left. + \frac{1}{2} \sin \frac{\pi}{4} \cos \frac{\pi}{4} \cos 2\theta + \sin^2 \frac{\pi}{4} (\frac{1}{2} \theta + \frac{1}{4} \sin 2\theta) \right] \Big\}$ $+ \frac{R^2}{EI} \int_{\frac{3\pi}{4}}^{\pi} \left\{ \frac{1}{2} R \left[\cos \frac{\pi}{4} \cos \frac{3\pi}{4} (\frac{1}{2} \theta - \frac{1}{4} \sin 2\theta) + \frac{1}{4} \cos \frac{\pi}{4} \sin \frac{3\pi}{4} \cos 2\theta \right. \right.$ $\left. \left. + \frac{1}{4} \sin \frac{\pi}{4} \cos \frac{3\pi}{4} \cos 2\theta + \sin^2 \frac{\pi}{4} \sin \frac{3\pi}{4} (\frac{1}{2} \theta + \frac{1}{4} \sin 2\theta) \right] \right\}$		

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$$\begin{aligned}
S_F = \frac{R^2}{EI} & \left\{ M_1 \left[(-0.707)(-1-0.707) - 0.707(-0.707) \right] - V_1 R \left[0.707 \left(\frac{3\pi}{8} - 0 + \frac{1}{4} \right) \right. \right. \\
& \left. \left. + 0.707 \left(\frac{1}{4} - 0 \right) \right] - P_1 R \left[0.707 \left(1 + 0.707 + \frac{1}{4} - 0 \right) - 0.707 \left(0 - 0.707 - \frac{3\pi}{8} + \frac{1}{4} \right) \right] \right. \\
& \left. + F_1 R \left[0.500 \left(\frac{3\pi}{8} - 0 + \frac{1}{4} \right) + 0.500 \left(\frac{1}{2} \right) + 0.500 \left(\frac{3\pi}{8} + 0 - \frac{1}{4} \right) \right] \right\} \\
& + \frac{R^2}{EI} \left\{ F_2 R \left[-0.500 \left(\frac{\pi}{8} - 0 - \frac{1}{4} \right) + 0.500 \left(\frac{1}{4} \right) - 0.500 \left(\frac{1}{4} \right) + 0.500 \left(\frac{\pi}{8} + 0 + \frac{1}{4} \right) \right] \right\}
\end{aligned}$$

$$S_F = \frac{R^2}{EI} \left\{ 1.7070 M_1 - 1.1864 V_1 R - 2.5396 P_1 R + 1.4280 F_1 R + 0.2500 F_2 R \right\}$$

$$M_1 = \frac{R}{\pi} (2V_1 + P_1 \pi - 1.7070 F_1 - 0.2927 F_2)$$

$$P_1 = 0.5303 F_1 + 0.1767 F_2$$

$$V_1 = 0.3341 F_1 - 0.3700 F_2$$

Then:

$$M_1 = R (0.7996 F_1 - 0.1521 F_2)$$

SUBSTITUTING

$$S_F = \frac{R^3}{EI} (0.0256 F_1 - 0.0193 F_2)$$

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TITLE

DEFLECTION OF TAIL BEARING STRUCTURE

REQUIRED INERTIA OF SECTION IF $F_2 = 0$

$$\delta_F = 0.0256 \frac{R^3 F}{EI}$$

$$I = 0.0256 \frac{R^3 F}{E \delta_F}$$

LET $R = 47$ IN.

$E = 30 \times 10^6$ PSI

$\delta_F = 0.030$ IN.

$F = 367,000$ LBS.

THEN

$$I = \frac{0.0256 (47)^3 (367,000)}{(30 \times 10^6) (0.030)}$$

$I = 1084$ IN.⁴

SECTION ROUGHLY $8\frac{1}{2}$ " X 24"

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TITLE

DEFLECTION OF TAIL BEARING STRUCTURE

A POSITIVE DEFLECTION AT F_1 CAUSES A NEGATIVE DEFLECTION AT F_2 , BUT SUPPOSE THAT LOAD F_2 IS IMPOSED BY A HYDROSTATIC BEARING SUCH THAT

$$F_2 = F_0 \left(\frac{2h}{2h + \delta F_2} \right)^3. \text{ HERE } F_0 \text{ IS THE INITIAL LOAD}$$

WHEN NO WIND MOMENT IS APPLIED, AND 'h' IS THE HYDROSTATIC FILM THICKNESS.

THE FOLLOWING IS A DEVELOPMENT OF THE LOAD-DEFLECTION RELATIONS AT F_1 AND INCORPORATING THE HYDROSTATIC FILM AT F_2 .

WE HAVE THE EQUATIONS:

$$1) \delta F_2 = \frac{R^3}{EI} (-0.0193 F_1 + 0.0256 F_2)$$

$$2) \delta F_1 = \frac{R^3}{EI} (0.0256 F_1 - 0.0193 F_2)$$

$$3) F_2 = F_0 \left(\frac{2h}{2h + \delta F_2} \right)^3$$

SOLVING FOR δF_2 IN EQUATION (3):

$$\delta F_2 + 2h = 2h \sqrt[3]{\frac{F_0}{F_2}}$$

$$\delta F_2 = 2h \left[\sqrt[3]{\frac{F_0}{F_2}} - 1 \right]$$

SUBSTITUTING IN EQUATION (1):

$$2h \sqrt[3]{\frac{F_0}{F_2}} - \sqrt[3]{\frac{F_0}{F_2}} (2h) = \frac{R^3}{EI} (-0.0193 F_1 + 0.0256 F_2) \sqrt[3]{\frac{F_0}{F_2}}$$

FOR SIMPLICITY, LET

$$a = \frac{R^3}{EI}, \quad \sqrt[3]{\frac{F_0}{F_2}} = Y, \quad b = 0.0193, \quad c = 0.0256$$

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$$\therefore Y^4 + Y \left[\frac{2h}{ac} - \frac{bF_0}{c} \right] - \frac{2h}{ac} \sqrt[3]{F_0} = 0$$

NOW, LET

$$t = \frac{2h}{ac} - \frac{bF_0}{c}, \quad n = \frac{2h}{ac} \sqrt[3]{F_0}$$

$$Y^4 + tY - n = 0$$

FOR SOLUTION OF THIS QUARTIC EQUATION WE HAVE THE FOLLOWING BASE EQUATION:

$$Y^4 + qY^2 + rY + s = 0$$

$$(Y^2 + 2kY + l)(Y^2 - 2kY + m) = 0$$

$$64k^6 + 32qk^4 + 4(q^2 - 4s)k^2 - r^2 = 0$$

IN THIS CASE,

$$q = 0, \quad r = t, \quad s = -n$$

$$64k^6 + 16tk^2 - t^2 = 0$$

$$k^6 + \frac{t}{4}k^2 - \frac{t^2}{64} = 0$$

LET $z = k^2$, AND APPLY CARDAN'S RULES FOR THE SOLUTION OF A CUBIC EQUATION,

$$z^3 + \frac{t}{4}z - \frac{t^2}{64} = 0$$

IN THIS CASE,

$$b = 0, \quad c = \frac{t}{4}, \quad d = -\frac{t^2}{64}$$

$$p = \frac{t}{4}, \quad j = -\frac{t^2}{64}$$

$$S = \frac{1}{27}p^3 + \frac{1}{4}j^2; \quad S = \frac{1}{27}\left(\frac{t^3}{64}\right) + \frac{1}{4}\left(\frac{t^4}{64^2}\right)$$

FINALLY;

$$z = k^2 = \sqrt[3]{\frac{t}{4} + \sqrt{S}} + \sqrt[3]{\frac{t}{4} - \sqrt{S}}$$

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NOW WE CAN SOLVE FOR Y IN GENERAL TERMS.

$$(Y^2 + 2KY + l)(Y^2 - 2KY + m) = 0$$

$$Y = -K \pm \sqrt{K^2 - l} \quad ; \quad Y = K \pm \sqrt{K^2 - m}$$

$$l = \frac{1}{2} \left(\frac{q}{b} + 4K^2 - \frac{F}{2K} \right) = 2K^2 - \frac{F}{4K}$$

$$m = \frac{1}{2} \left(\frac{q}{b} + 4K^2 + \frac{F}{2K} \right) = 2K^2 + \frac{F}{4K}$$

$$Y = -K \pm \sqrt{K^2 - \frac{F - 4K^3}{4K}} \quad ; \quad Y = K \pm \sqrt{K^2 + \frac{F + 4K^3}{4K}}$$

SINCE 'K' CAN BE EITHER POSITIVE OR NEGATIVE AND GIVE THE SAME 'Y' ROOTS, USE 'K' POSITIVE.

THEN:

$$\textcircled{1} Y = -K \pm \sqrt{K^2 - \frac{F - 4K^3}{4K}} \quad ; \quad \textcircled{2} Y = K \pm \sqrt{K^2 + \frac{F + 4K^3}{4K}}$$

SINCE 'K' IS POSITIVE AND 'F' IS ALWAYS A NEGATIVE VALUE, EQUATION $\textcircled{1}$ HAS IMAGINARY ROOTS. TO FOLLOW, FROM EQUATION $\textcircled{2}$ 'Y' HAS ONE POSITIVE ROOT.

$$Y = \sqrt[3]{F_2} = K + \sqrt{K^2 + \frac{F + 4K^3}{4K}}$$

WHERE:

$$K = \sqrt[3]{-\frac{1}{2}j + \sqrt{3}} + \sqrt[3]{-\frac{1}{2}j - \sqrt{3}}$$

$$j = -\frac{1}{\omega^4}$$

$$S = \frac{1}{27} \left(\frac{10^3}{64} \right) + \frac{1}{4} \left(\frac{1^4}{64^2} \right)$$

$$F = \frac{2h}{ac} - \frac{bF_0}{c}$$

$$F = \frac{2h}{ac} \sqrt[3]{F_0}$$

$$a = \frac{E^2}{F_0}$$

$$c = 0.025b$$

$$b = 0.0153$$

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TITLE DEFLECTION OF TAIL BEARING STRUCTURE		
<p>F_2 CAN NOW BE DETERMINED IF F_1 IS KNOWN.</p> <p>δ_{F_2} AND δ_{F_1} CAN THEN BE CALCULATED FROM EQUATION 1 & 2).</p> <p>1) $\delta_{F_2} = \frac{P^3}{EI} (-0.0193 F_1 + 0.0256 F_2)$</p> <p>2) $\delta_{F_1} = \frac{P^3}{EI} (0.0256 F_1 - 0.0193 F_2)$</p>		

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TITLE COMPUTATIONS OF TAIL BEARING DEFLECTION

FOR AN APPLIED LOAD, $F_1 = 350,000 \#$
 AND AN INITIAL LOAD, $F_0 = 75,000 \#$
 WHERE :

$$I = 1000 \text{ IN.}^4 \qquad E = 30 \times 10^6 \text{ PSI}$$

$$R = 50 \text{ IN.} \qquad h = .007$$

THE DEFLECTIONS δ_{F_1} & δ_{F_2} MAY BE CALCULATED.

$$r = t = \left(\frac{2h}{ac} - \frac{b}{c} F_1 \right) = \left\{ \frac{(14 \times 10^{-3})(30 \times 10^6)(10^3)}{(2.56 \times 10^{-2})(12.50 \times 10^4)} - \frac{1.93 \times 10^{-2}}{2.56 \times 10^{-2}} (35 \times 10^4) \right\}$$

$$r = t = 131.25 \times 10^3 - 263.9 \times 10^3$$

$$r = t = -13.265 \times 10^4$$

$$t^2 = 175.96 \times 10^8$$

$$t^4 = 30,962 \times 10^{16}$$

$$n = \frac{2h}{ac} \sqrt[3]{F_0} = \frac{(14 \times 10^{-3})(30 \times 10^6)(10^3)}{(12.50 \times 10^4)(2.56 \times 10^{-2})} \cdot \sqrt[3]{75 \times 10^3}$$

$$n = 131.25 \times 10^3 \times 42.19$$

$$n = 55.374 \times 10^5$$

$$-\frac{1}{2j} = \frac{t^2}{128} = \frac{175.96 \times 10^8}{128} = 1.375 \times 10^8$$

$$S = \left(\frac{1}{27} \right) \frac{n^3}{64} + \left(\frac{1}{4} \right) \frac{t^4}{64^2} = \frac{53.374^3 \times 10^{15}}{27 \cdot 64} + \frac{309,620 \times 10^{15}}{4 \cdot 64^2}$$

$$S = 98.26 \times 10^{15} + 18.9 \times 10^{15}$$

$$S = 11.716 \times 10^{16}$$

$$\sqrt{S} = 3.42 \times 10^8$$

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TITLE COMPUTATIONS OF TAIL BEARING DEFLECTION		
$K^2 = \sqrt[3]{-\frac{1}{2}j + \sqrt{5}} + \sqrt[3]{-\frac{1}{2}j - \sqrt{5}}$ $K^2 = (1.375 \times 10^8 + 3.42 \times 10^8)^{1/3} + (1.375 \times 10^8 - 3.42 \times 10^8)^{1/3}$ $K^2 = (479.5 \times 10^6)^{1/3} - (204.5 \times 10^6)^{1/3}$ $K^2 = 7.83 \times 10^2 - 5.89 \times 10^2$ $K^2 = 194$ $K = 13.93$ $K^3 = 2702.4$ $Y = 13.93 + \sqrt{\frac{-132,650 + 4(2702.4)}{-4(13.93)}}$ $Y = 13.93 + 46.77 = 60.70$ $\sqrt[3]{F_2} = Y = 60.7$ $F_2 = 223,650 \#$ $a = \frac{R^3}{EI} = \frac{50^3}{30 \times 10^6 \times 10^3}$ $a = 4.167 \times 10^{-6}$ $\delta_{F_1} = 4.167 \times 10^{-6} [0.0256(35 \times 10^4) - (0.0193)(223,650)]$ $\delta_{F_1} = (4.167 \times 10^{-6})(46.4 \times 10^2)$ $\delta_{F_1} = .0193''$ $\delta_{F_2} = 4.167 \times 10^{-6} [0.0256(223,650) - (0.0193)(35 \times 10^4)]$ $\delta_{F_2} = -(4.167 \times 10^{-6})(10.3 \times 10^2)$ $\delta_{F_2} = -.0043''$		

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TITLE COMPUTATIONS OF TAIL BEARING DEFLECTION

CHECK :

$$\delta_{F_2} = 2h \left[\sqrt[3]{F_0/F_2} - 1 \right]$$

$$\delta_{F_2} = 14 \times 10^{-3} \left[\sqrt[3]{\frac{7.5 \times 10^4}{22,365 \times 10^4}} - 1 \right]$$

$$\delta_{F_2} = 14 \times 10^{-3} (0.695 - 1)$$

$$\delta_{F_2} = -.0043$$

60

SUMMARY :

$$F_1 = 350,000 \#$$

$$F_2 = 223,650 \#$$

$$\delta_{F_1} = 0.0193 \text{ "}$$

$$\delta_{F_2} = -0.0043 \text{ "}$$

0.0178" + 360
 $1.78 \times 10^{-2} \times 3.6 \times 10^2$
 $\frac{3}{6.4 \text{ seconds}}$

$\frac{0.0193}{600} = \frac{1.93 \times 10^{-2}}{6 \times 10^2}$
 1.78×10^{-2}
 0.0178
 3.22×10^{-4}
 0.322

$0.322 \times \frac{180}{\pi}$
 $\frac{3.22 \times 10^{-4} \times 1.8 \times 10^2}{\pi}$

0.0178