

NATIONAL RADIO ASTRONOMY OBSERVATORY
VLA ELECTRONICS MEMORANDUM NO. 143
VLA ELECTRONICS BLOCK DIAGRAM REVISIONS

S. Weinreb
March 22, 1974

The following changes have been made between March 1973 and March 1974:

1. Change 500, 1250, and 1750 MHz to 600, 1200, and 1800 MHz.

The original system required multiplying 250 MHz by x5 and x7. These multipliers are not as phase-stable as x2 and x3 units with input at 600 MHz. This change causes many frequencies throughout the system to change.

2. Provide Variable Bandwidth.

Computer-selectable bandwidths of 50, 24, 12, 4, 1.5 and 0.5 MHz have been incorporated in Unit 1016.

3. Antenna LO Simplification .

The original LO was tunable at the antenna in 5 MHz steps. A simplified system shown on page 2 of Block 04 allows tuning in 20 or 30 MHz steps at a cost savings of ~\$20,000 per antenna. A final LO in the control room allows tuning in steps of 10 Hz.

4. Lobe Rotation at Antenna.

The original system provided lobe rotation in the control room. By moving the lobe rotation to the antenna and increasing the phase-switching frequency the allowable level of spurious signals in the IF transmission system has been increased from -60 dB to -30 dB (See VLA Electronics Memos #116 and 122). Lobe rotation at the antenna is also a step needed for digital transmission of IF signals.

5. Phase-Switch Detection at Sampler.

The phase-switching pattern applied at the antenna will be removed by applying the same pattern at each sampler (in lieu of the computer as originally planned). This allows faster phase switching and reduces the computer load.

6. Alternate Front-End Input.

A computer-controlled coaxial switch to allow input of an alternate front-end having 1-2 GHz IF output has been provided in Block 02.

7. Polarization Transfer Switch.

A computer-controlled transfer switch has been incorporated at the input of the Frequency Converter, Block 02. This will allow the back-ends used for the

two polarizations to be exchanged. The purpose is to determine and eliminate effects due to small differences in the back-ends.

8. Alternate Digital-Data Transmission Channel.

Tests of the breadboard system indicated that the digital monitor and control data carried on the 1800 MHz carrier may interfere with LO phase information on this same carrier. A separate 1975 MHz carrier, FM modulated by digital data, has been incorporated as an alternative. Tests of the Antenna 1-2 system will determine which method will be used.

9. Low-Frequency LO Output.

An output from unit (0437) provides LO outputs at $n \times 50 \pm 10$ MHz for $n=1$ to 20. This is a by-product of the 2.8 to 3.8 GHz LO and should be useful for low frequency front-ends.

10. Change IF Transmission Transmit-Receive Repetition Rate.

This rate has been changed from 20 Hz to 19.20 Hz to reduce the effect of 60 Hz power line pickup in the system. The 19.2 Hz has period 52.0833... ms and 192 cycles will give exactly 10 seconds of integration (in lieu of the original 9.6 seconds).

11. Transmission of Timing Pulse to Antenna.

A fast-rise time (~50 ns) pulse, labeled TP on block diagrams, will be provided by keying the 1200 and 1800 MHz carriers to each antenna at a 6.4 Hz rate. This pulse, in conjunction with the 5 MHz and 600 MHz LO signals and a 0.1 Hz bit in the data system, provides a fixed time relation between every antenna and the control room. This time relation is stable to 3 ps, unambiguous to 10s, and is recovered after a power failure. Without the timing pulse, ambiguities of 0.2 μ s could exist and would effect the accuracy of the antenna lobe rotator. The TP pulse will occur 50 μ s after the T/R pulse.

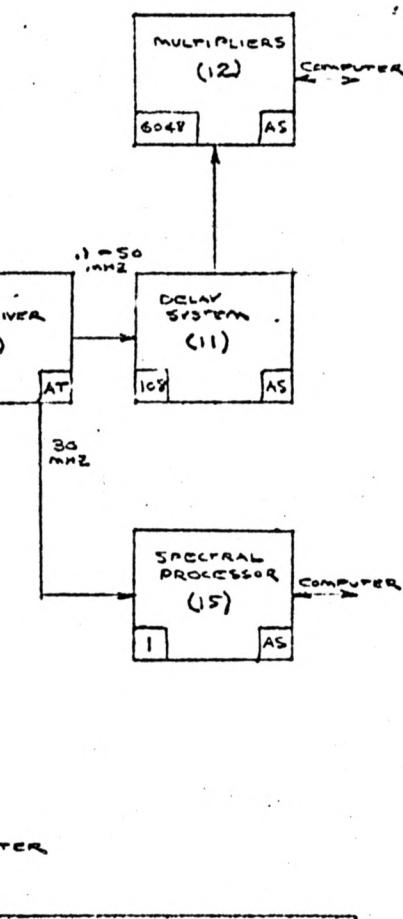
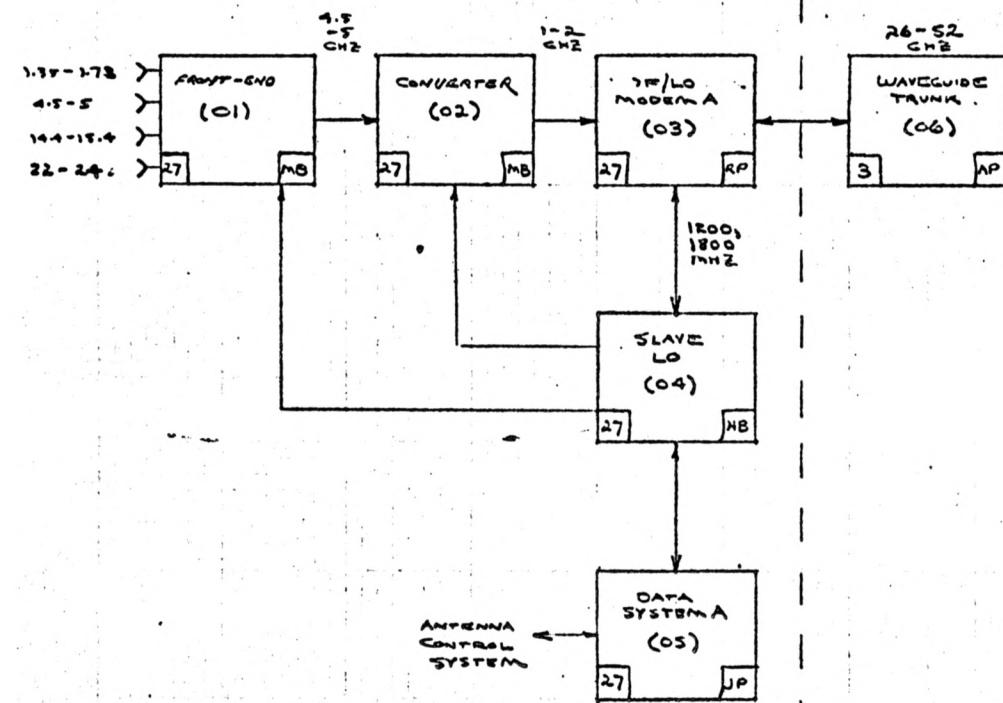
12. Additional Voltage-Controlled Oscillators (VCO's).

A crystal 50 MHz VCO has been added in the master and slave multiplier chains to eliminate spurious 5 MHz sidebands on high-frequency carriers. Cavity VCO's at 1200 and 1800 MHz have replaced voltage controlled phase-shifters in circuitry to narrow-band filter received carriers; the voltage controlled phase-shifter circuitry was too slow and unstable.

ANTENNA

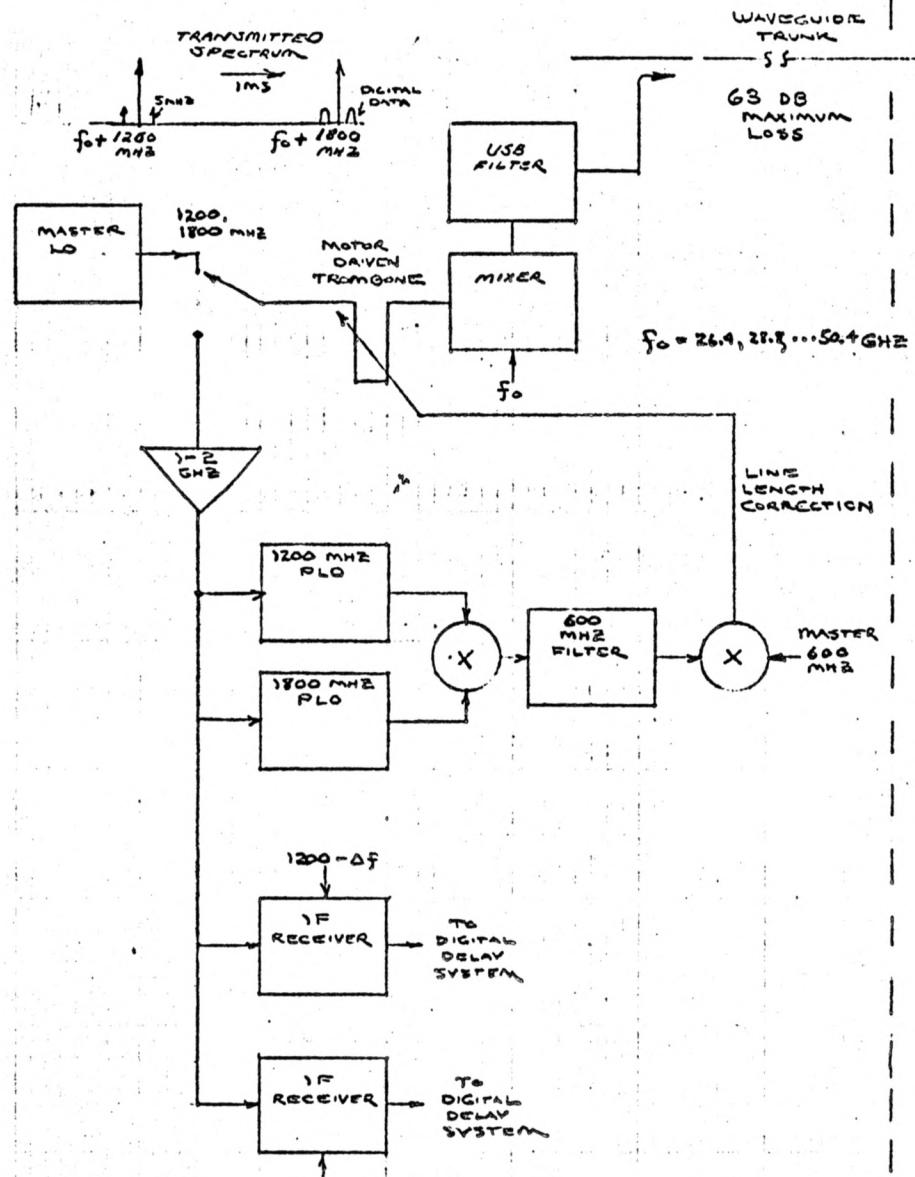
WYE

CONTROL BLDG.

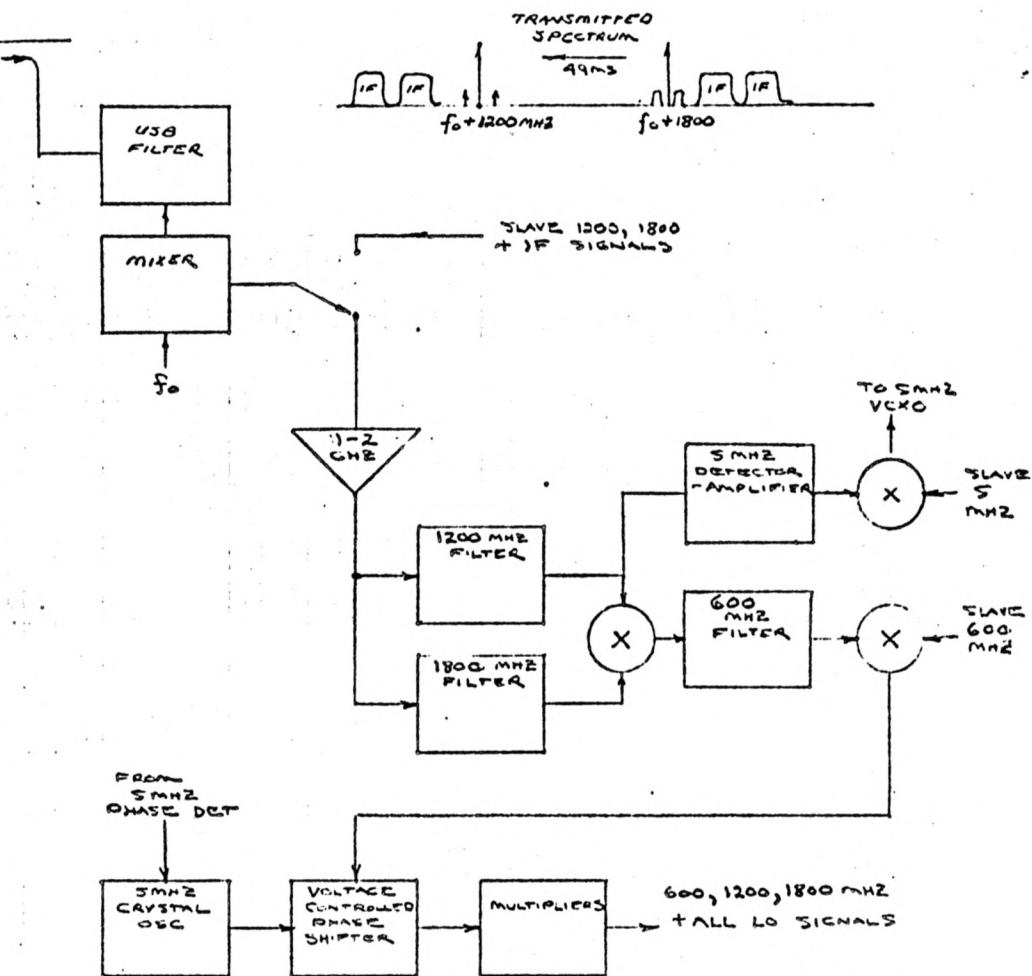


VLA ELECTRONICS
SYSTEM
MAIN BLOCK DIAGRAM
DWG B1301081
S. WEINREB
MARCH 20, 1974

CONTROL ROOM

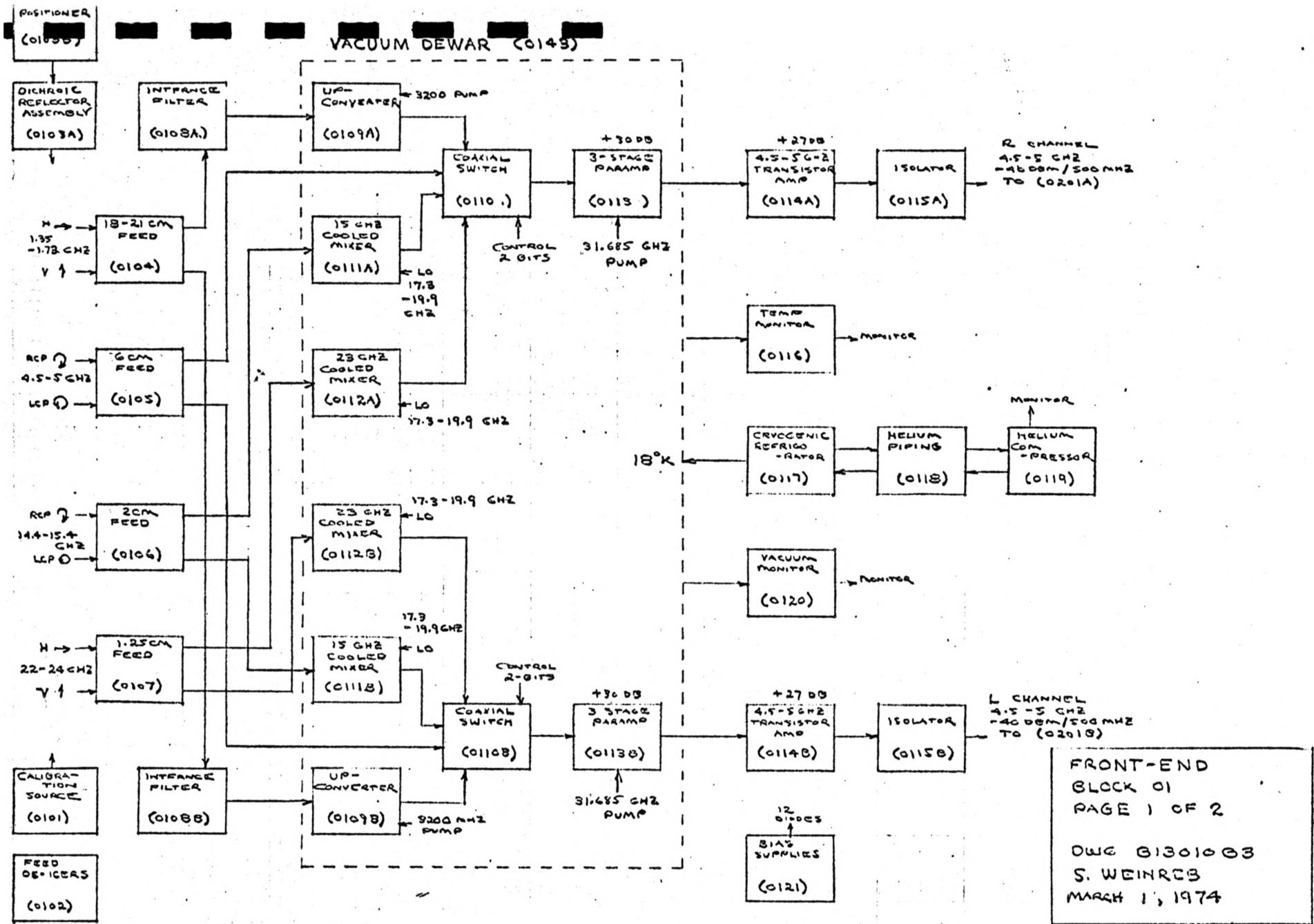


ANTENNA CABIN

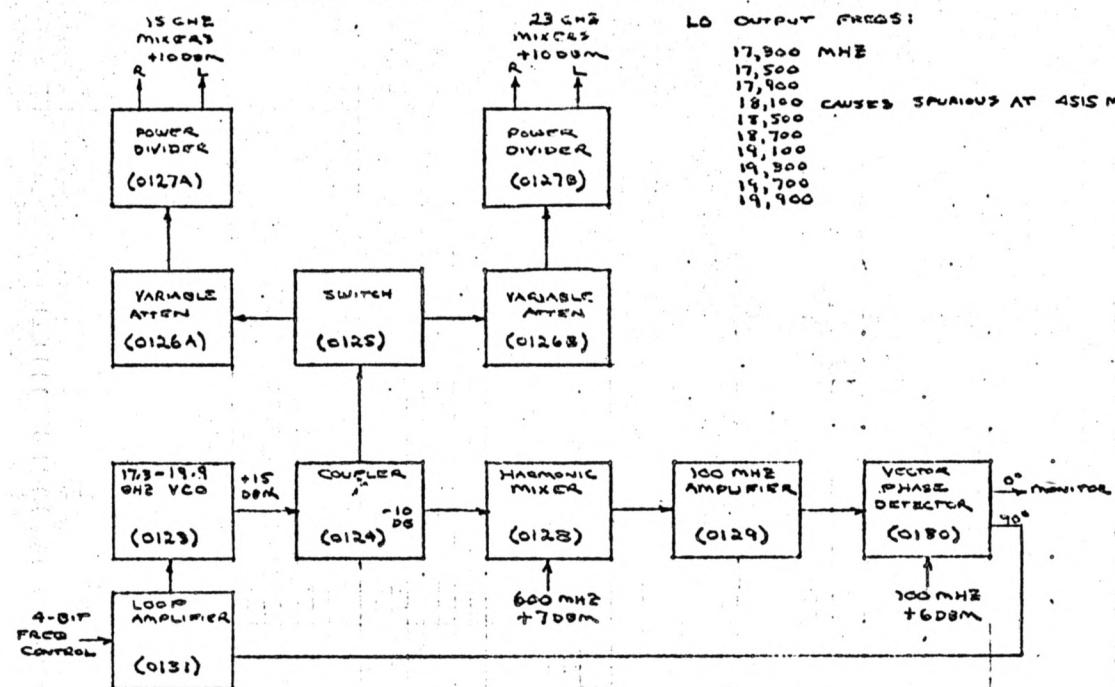


CONCEPTUAL DIAGRAM
VLA IF/LO SYSTEM

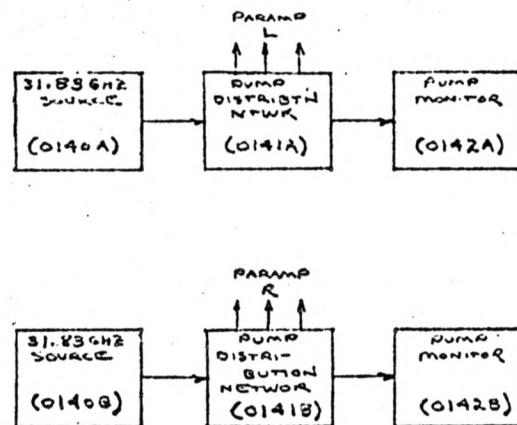
OWG B13010 B2
S. WEINREB
MARCH 20, 1974



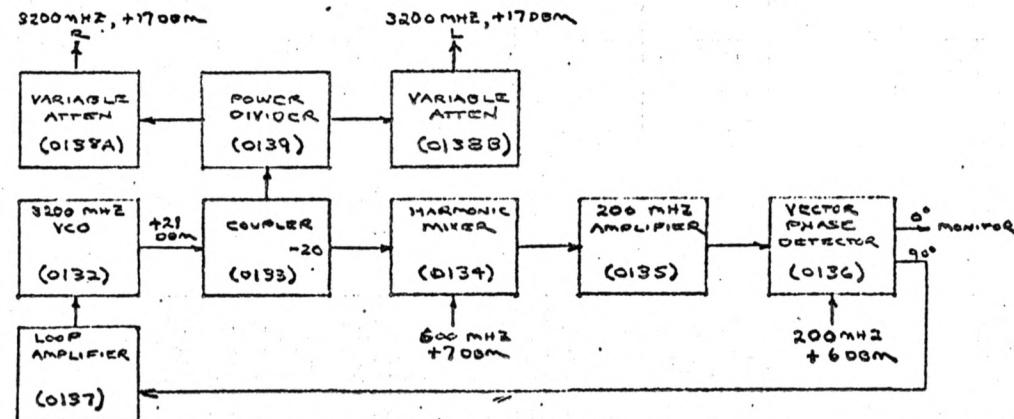
17.3 - 19.9 GHz LOCAL OSCILLATOR



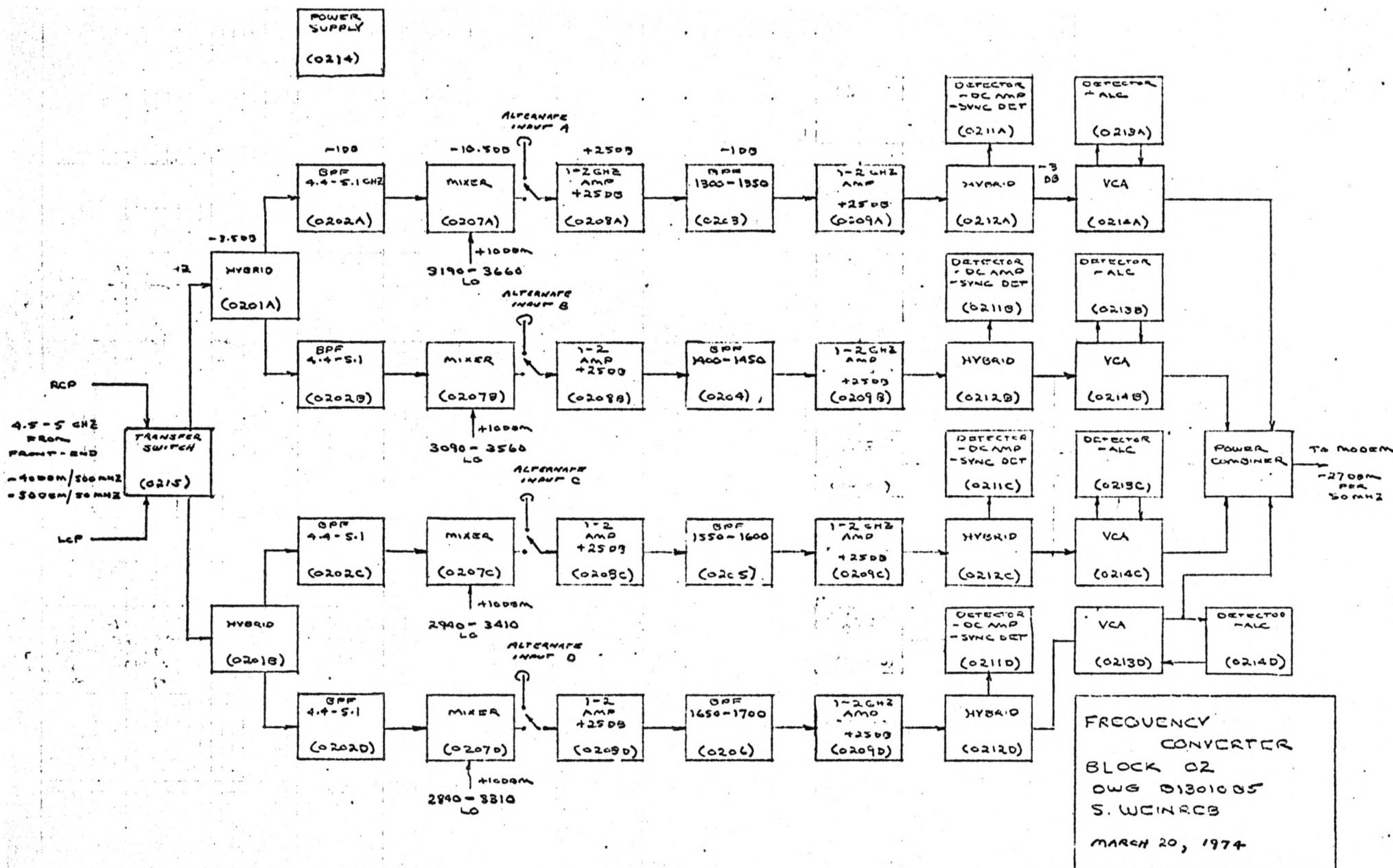
33.85 GHz PARAMP PUMPS

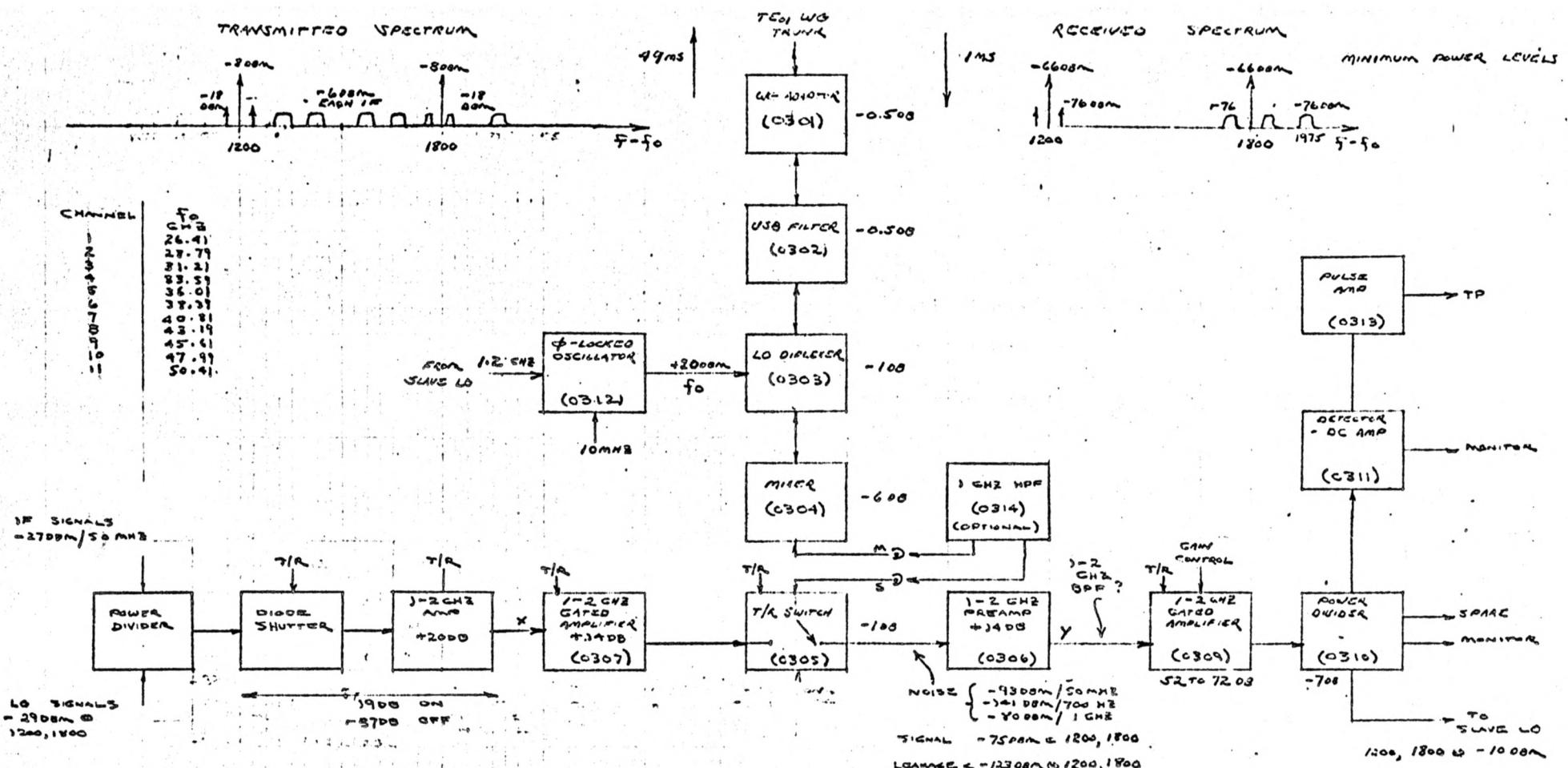


3.20 GHz UP-CONVERTER PUMP



FRONT-END
BLOCK 01
PAGE 2 OF 2
OWG 013010 04
S. WEINREB
MARCH 20, 1974

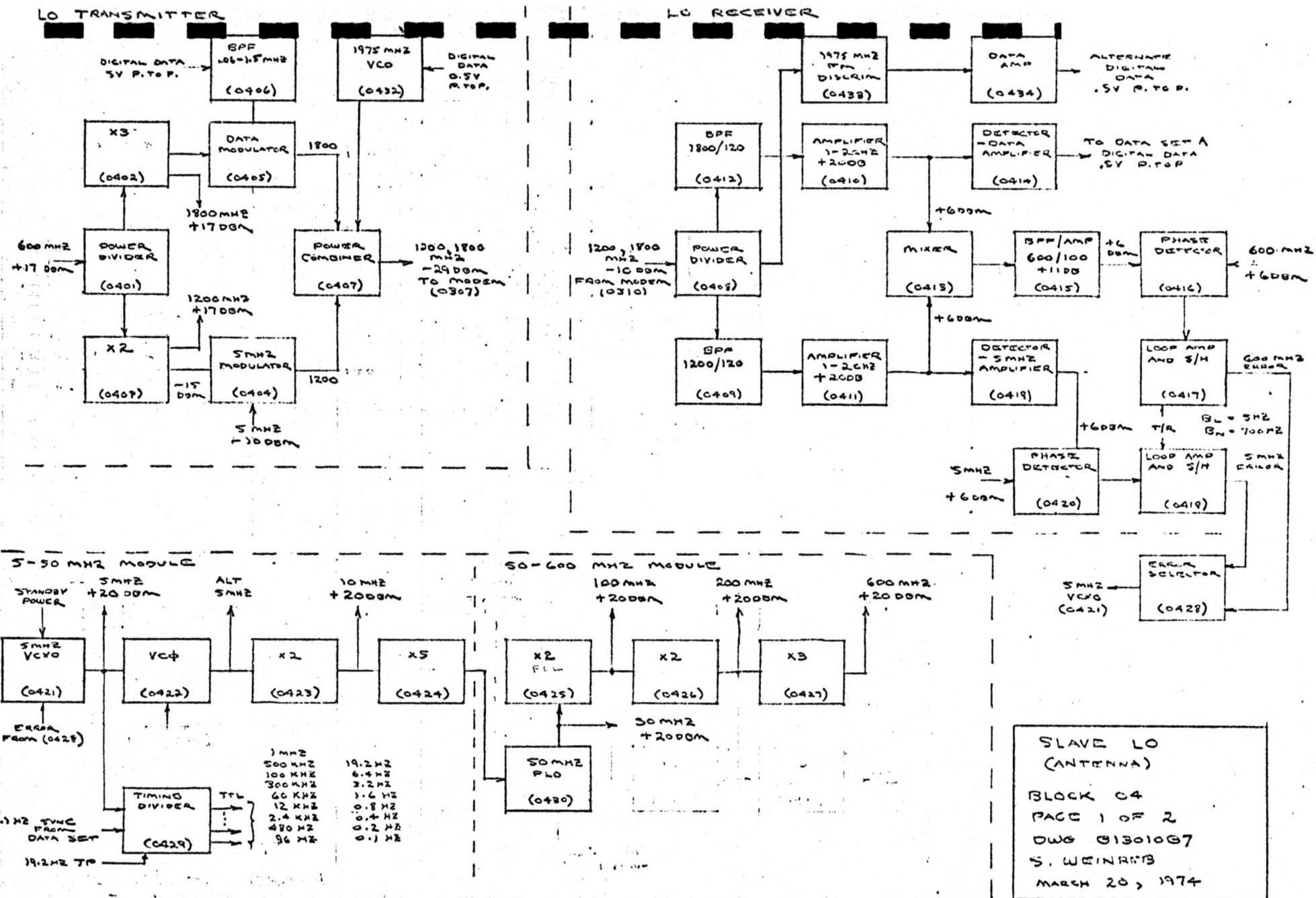


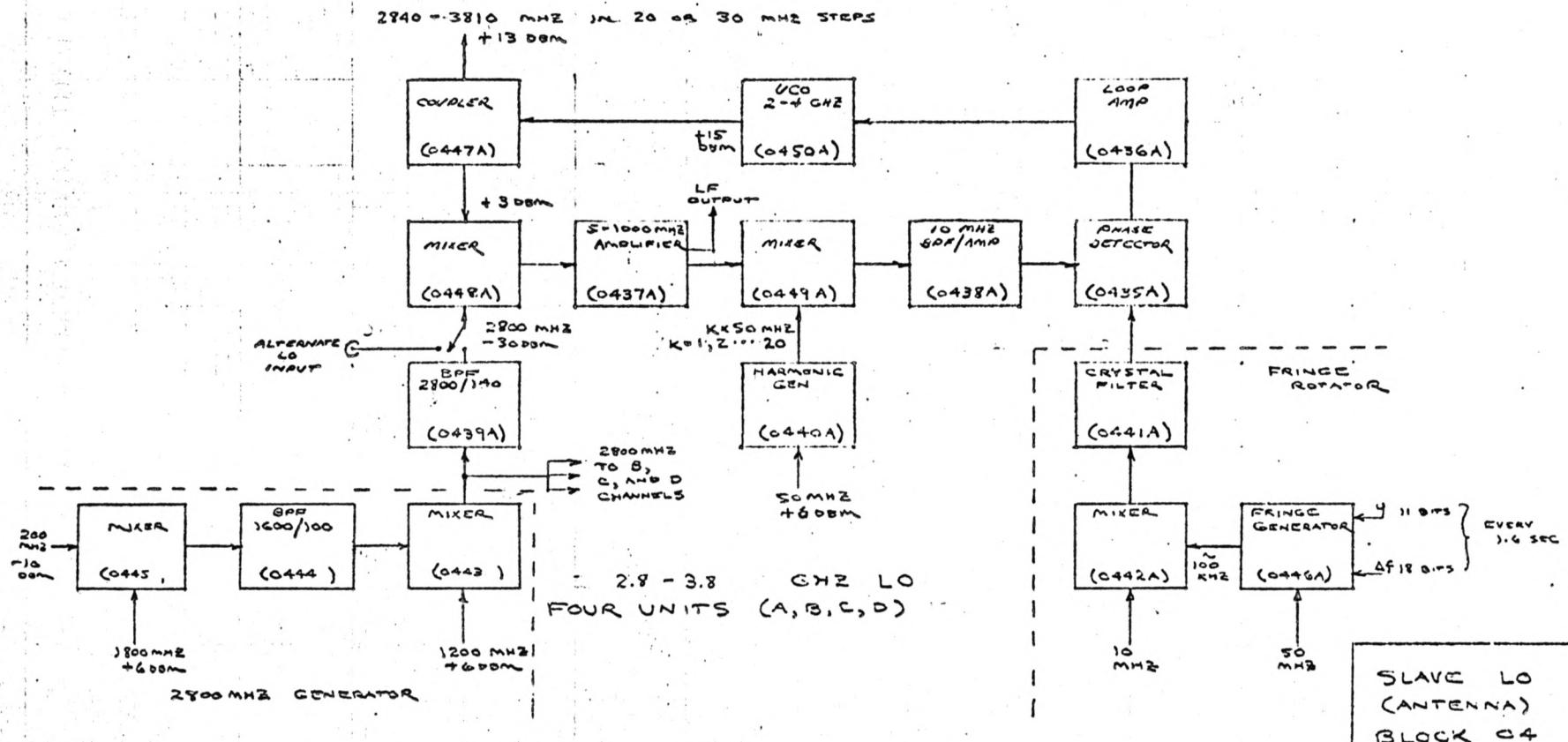


IF/LO MODUL A
(ANTENNA).

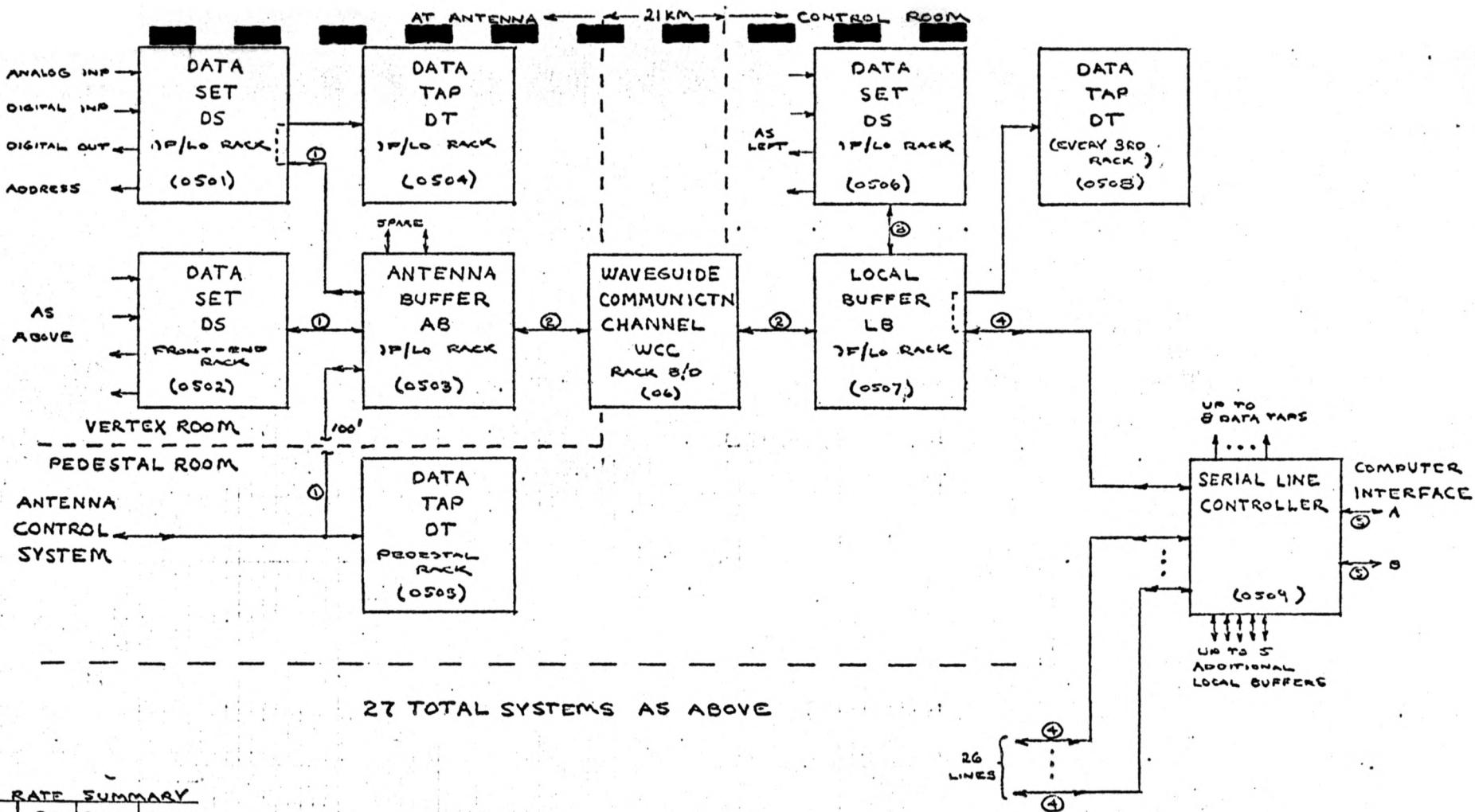
BLOCK 03,
Dwg B1303066

S. WEINREB
MARCH 1, 1974





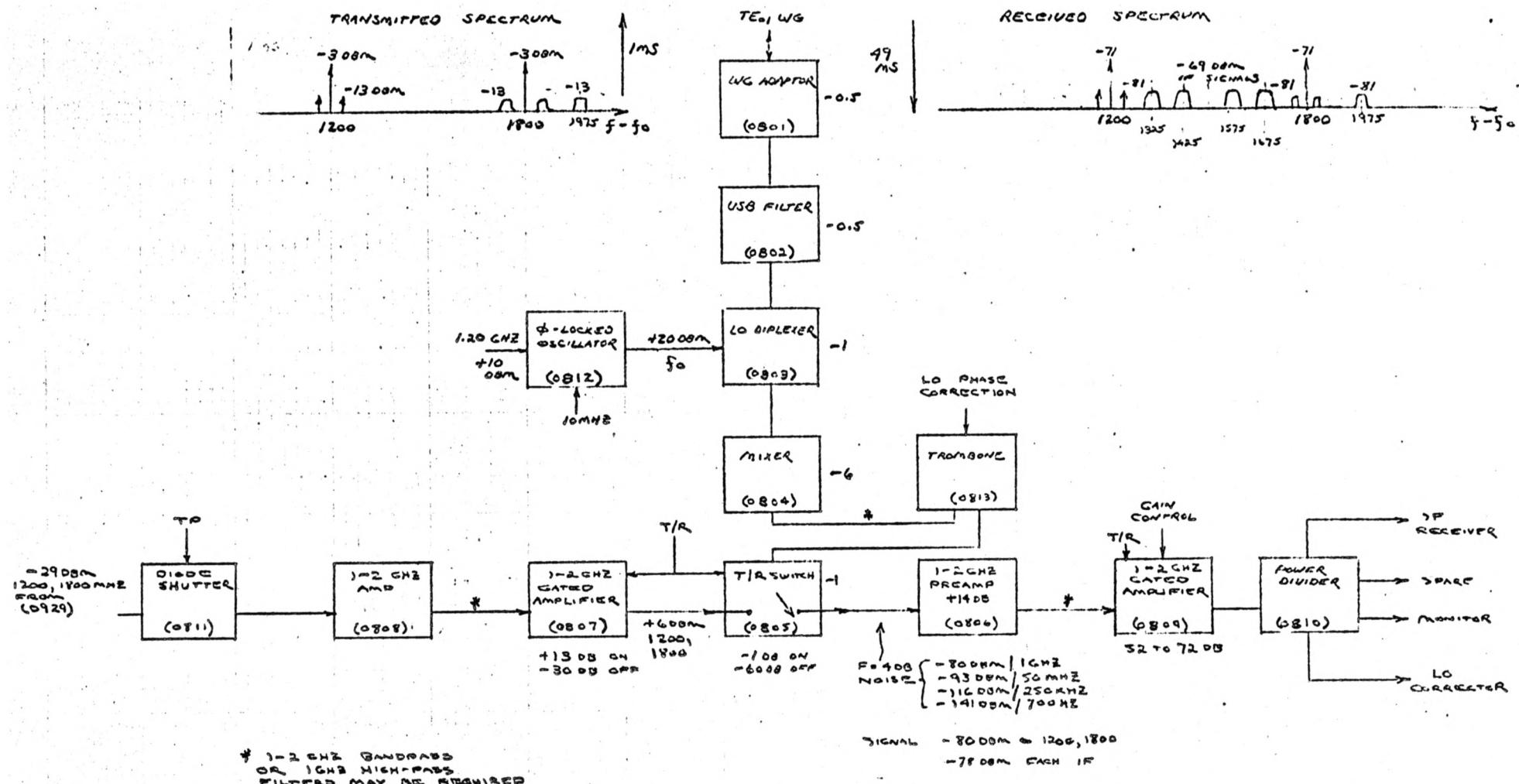
SLAVE LO
(ANTENNA)
BLOCK 04
PAGE 2 OF 2
OWG B1301008
S. WEINREB
MARCH 1, 1974



DATA RATE SUMMARY

PATH	BIT TIME	BITS SEC	CABLE
	PER MS	(AVERAGE)	
① →	10	1800	PAIR
① →	10	3600	PAIR
② →	50	9000	COAX
② →	4	3600	COAX
③ ↓	10	1800	PAIR
③ ↑	10	5400	PAIR
④ →	1	10,800	PAIR
④ ←	1	5,400	PAIR
⑤ →	1	397KB	MULT
⑤ ←	1	153KB	WIRE

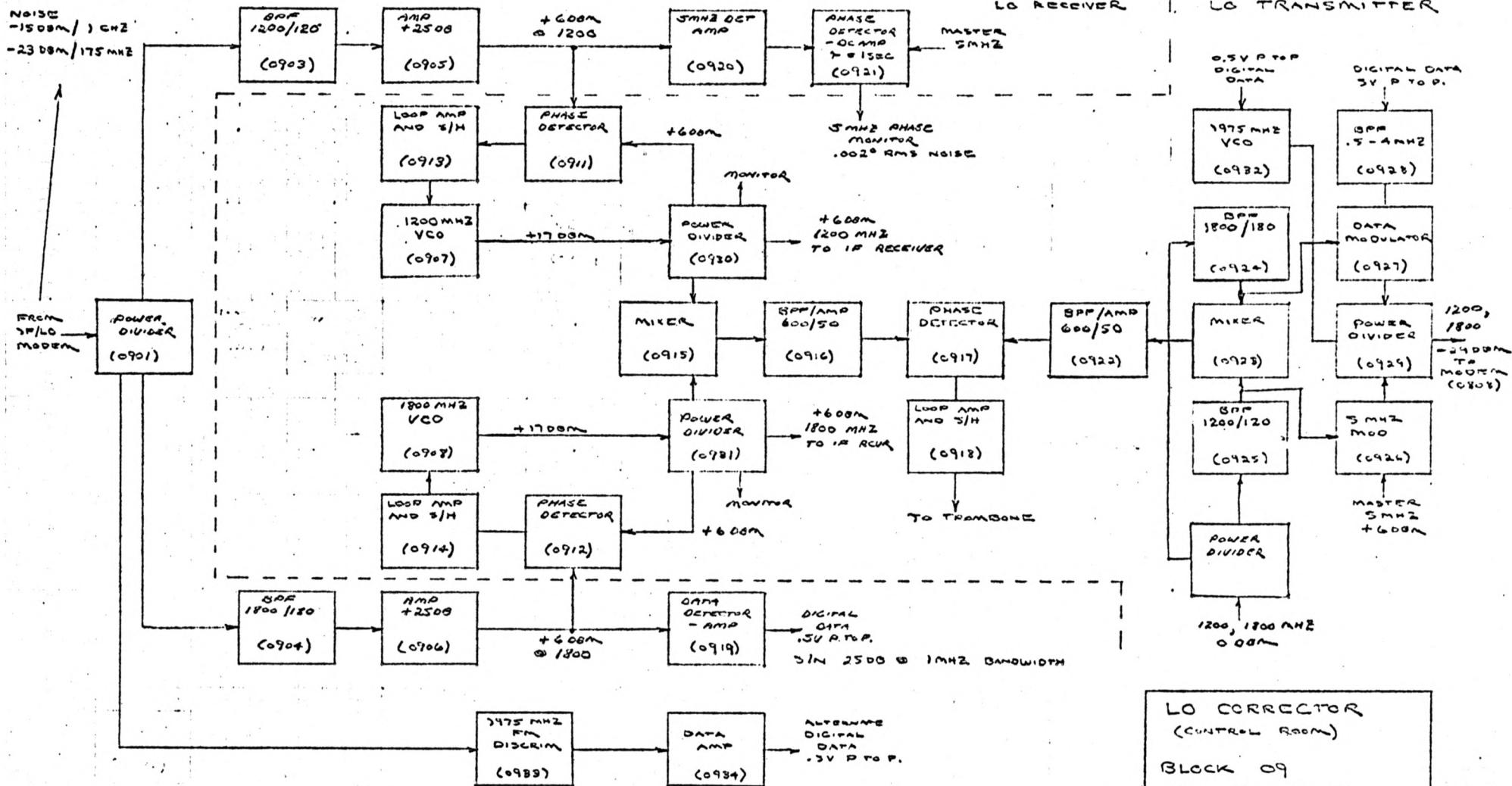
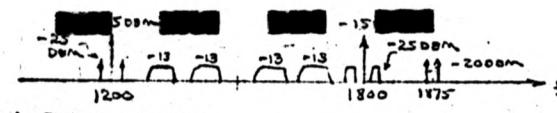
MONITOR AND
CONTROL SYSTEM
BLOCKS OS AND 13
OWG 131305009
S. WEINREB
JUNE 27, 1973



* 1-2 GHz BANDPASS
OR 1GHz HIGH-PASS
FILTER MAY BE REQUIRED
AT THESE POINTS

SIGNAL -80.00m @ 1200, 1800
-78.00m EACH IF

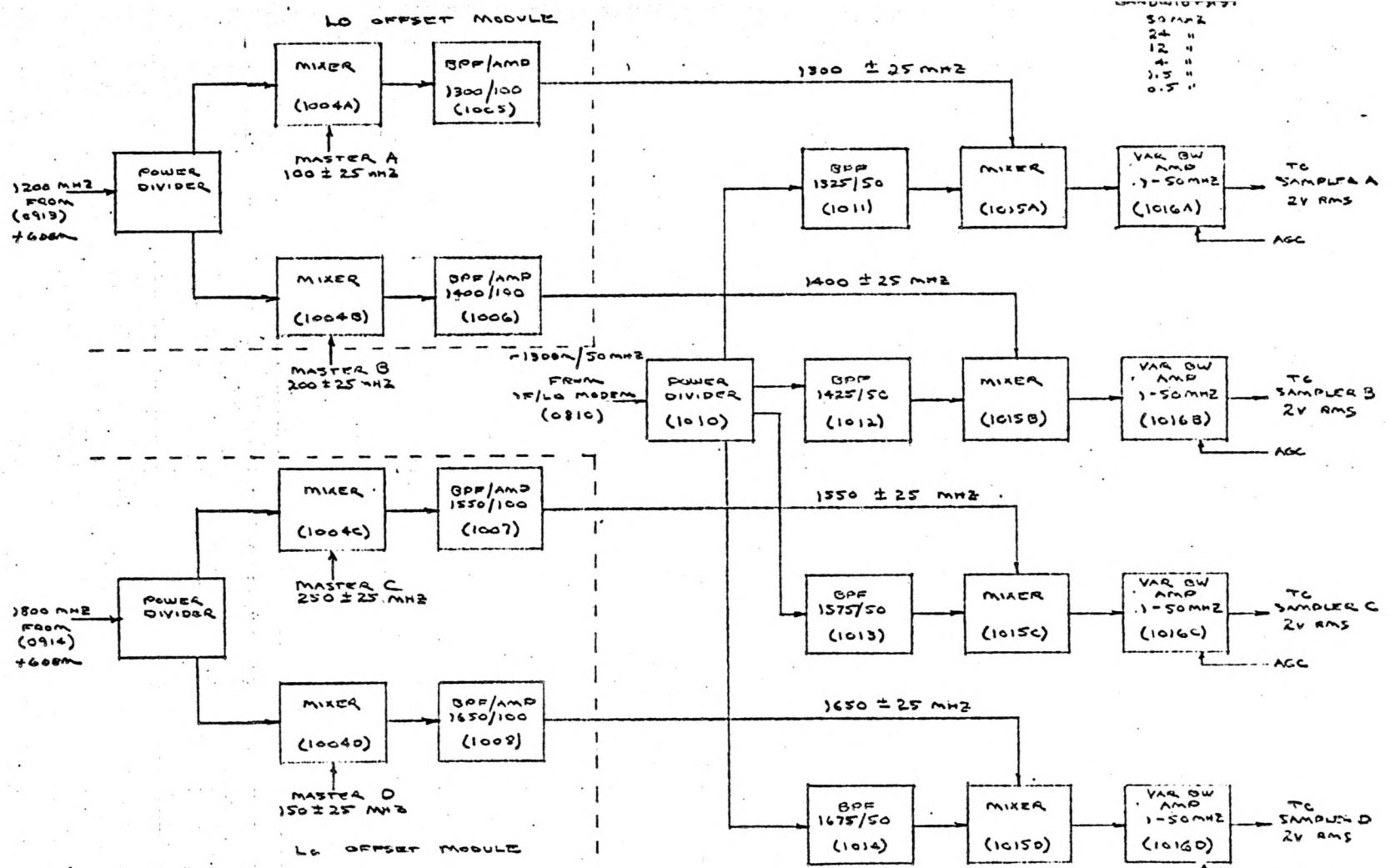
IF/LO MODEM B (CONTROL ROOM)
BLOCK 08
DWG B13010G10
S. WEINBERG
MARCH L, 1974



LO CORRECTOR
(CONTROL ROOM)

BLOCK 09
DWG G13010B11

S. WEINREB
MARCH 20, 1974

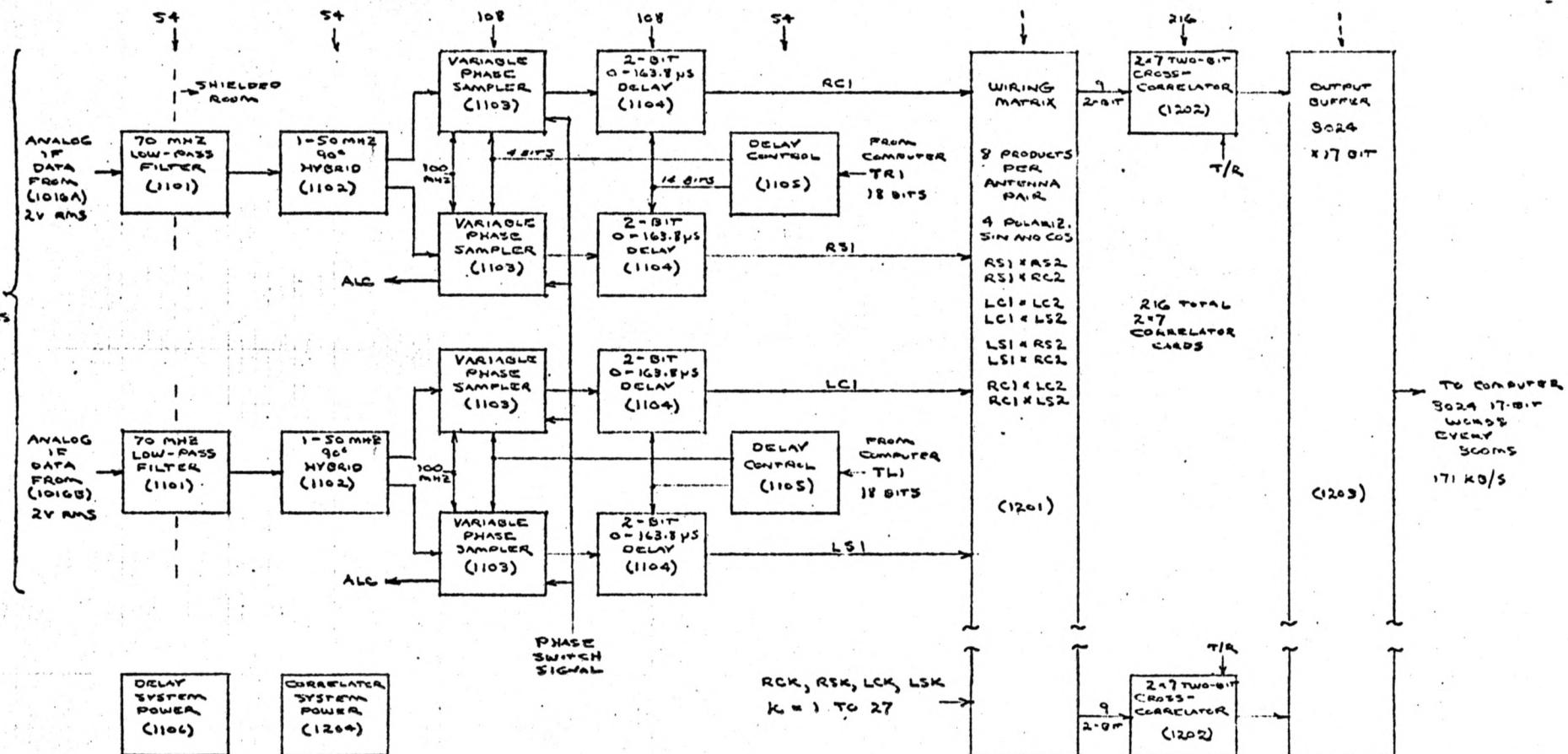


POWER SUPPLY
(1018)

IF RECEIVER
BLOCK 10
DWG @13010B12
S. WEINROB
MARCH 1, 1974

ALL SHOWN BELOW IS FOR ONE 50 MHZ BANDWIDTH; DOUBLE ALL QUANTITIES FOR SECOND CHANNEL.

FOR
EACH
OF
27
ANTENNAS



DIGITAL DELAY AND
CORRELATOR SYSTEM
BLOCKS 11 AND 12

DWG B13010 B13
S. WEINREB

APRIL 6, 1973

