

VLA-VLBA Interference Protection Memo #35

VLA Site-Generated RFI Control Plan

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Abstract

EVLA RF emissions limits and site building architectural shielding are summarized. Tables of existing or potential site-based RF emitters, and EVLA module and rack shielding are presented. The emissions limits are created from EVLA Memo #106 and Interference Protection Memos 34, the architectural shielding values are estimated from VLA-VLBA Interference Protection Memos 29 and 32, and the emissions and shielding data from documented IPG test data.

1 INTRODUCTION

Radio frequency interference (RFI) generated by electronic devices located at the VLA site has the potential to significantly disrupt current VLA, and future EVLA and LWDA observations. Measures have been in place for over a decade to reduce the effects of emissions from site-based 2-way radios and personal computers via notifications and voluntary, equipment time-of-use limitations by site personnel. However, as digital electronic equipment at the VLA site has proliferated, and new EVLA higher-sensitivity and wider bandwidth observing programs prepare to go on-line, additional RFI control and mitigation measures are now necessary.

2 PURPOSE

The purpose of this VLA Site Generated RFI Control Plan is to:

- 1) Re-document the detrimental thresholds, and establish RF emission zone limits around the VLA site.
- 2) Inventory suspected RFI generating equipment currently installed at the VLA site,
- 3) Describe emissions tests performed or planned for existing equipment,
- 4) Describe mitigation measures taken or planned for existing equipment,
- 5) Establish new equipment screening procedures, as well as new equipment limitation guidelines.

3 STATUS

As of the time of the writing of this report (December, 2006), a relatively small number of commercial electronic equipment items, and a large number of EVLA RF and digital modules have been RF emissions tested. In addition, most of the proposed rack and module hardware has been tested in order to quantify shielding effectiveness. Most of these emissions and shielding tests were performed in the EVLA/ALMA shielded chamber, which is located in the north-east corner of the VLA site warehouse. The tests have been performed over the 4 years since the chamber was assembled, by seven different Cooperative Exchange students, as supervised by three different electrical engineers. As a result of this diversity of testers, test procedures were not uniformly executed, and test results are not uniformly documented. Where possible, the original shielding and emissions data has been re-analyzed according to the current conventions before inclusion in this report.

4 REQUIREMENTS

The received power flux density (PFD) limitations for RF emissions have been detailed in-general for radio astronomy observing by A.R. Thompson of NRAO¹, and lately for the EVLA by Rick Perley². The detrimental limits for each observing band follow the 10% of T_{sys} variation criterion established by Thompson, and incorporated into the ITU R-RA.769 recommendation, and Perley's EVLA series memos 46, 104, and 106. The limits proposed in EVLA Memo #106 attempt to take into account the attenuation provided by fringe rotation when the observing instrument is an interferometer array, observing a source greater than 5 degrees away from the celestial North Pole³. Perley's VLA-VLBA Interference memo #34 ("Notes on RFI Management") expands on the detrimental limits of EVLA Memo #106 by defining the detrimental limits in terms of power units (Watts) as captured by an EVLA antenna, per an astronomically significant bandwidth, from an RFI source at a reference distance of 1 m. Table 1, below, which was constructed from equation (9) of EVLA memo #106, and equation (7) of Interference memo #34, details the detrimental power limits for the center of each of the proposed EVLA receiving bands, in a bandwidth (BW) determined by the spectral line width of an astronomical source corresponding to a velocity width of 3 Km/sec. The detrimental power, maximum emission levels for an RFI source at any other distance may be easily calculated by adding the appropriate $20 \log_{10}(\text{separation distance})$ flux spreading factor to the detrimental power limit. From the same interference memo, equation (8) may be used to determine the additional shielding required to reduce emissions from an excessively-strong source to below the detrimental limits at the nearest EVLA antenna.

The T_{sys} values used for the two, sub-GHz bands are taken from the VLA Observational Status Summary, Table 4⁴. For the bands above 1 GHz, the T_{sys} is taken from the EVLA Project Book⁵, chapter 5, Table 5-1.

**Table 1: EVLA Detrimental levels Used
(Within the BW width listed in column 2)**

Freq (GHz)	BW (KHz)	T_{sys} (K)	PFD-detrimental (W/m ²) @ EVLA antenna	dBPFD-detrimental (dBW/m ²) @ EVLA antenna	P-detrimental (EIRP max) (dBW) @ RFI source @ 1 m [†]
0.0738	0.738	1000	2.81363E-20	-196	-184
0.328	3.28	150	3.70519E-19	-184	-173
1.5	15	26	6.1425E-18	-172	-161
3	30	26	4.914E-17	-163	-152
6	60	26	3.9312E-16	-154	-143
10	100	30	2.1E-15	-147	-136
15	150	37	8.74125E-15	-141	-130
23	230	59	5.02497E-14	-133	-122
34	340	53	1.45818E-13	-128	-117
45	450	74	4.72028E-13	-123	-112

[†] Assuming isotropic emission ($G_{e,dBi}, G_{r,dBi} = 0$) and no shielding ($S_{dB} = 0$). From eq (9) of VLA/VLBA Interference Memo #34, "Notes on RFI Management":

$$P_e < -180.6 + 20 \log_{10}(r_m) + 30 \log_{10}(v_G) + 10 \log_{10}(T_{sys}) - G_{e,dBi} - G_{r,dBi} + S_{dB} \text{ (dBW)},$$

With r_m being the distance between the emitter and antenna in meters,

v_G being the frequency in GHz,

and T_{sys} the temperature in K.

¹ IEEE Trans. Ant. Prop., AP-30, 450-456, 1982.

² EVLA series memos 46, 104, and 106.

³ EVLA series memo #106, section 5.

⁴ <http://www.vla.nrao.edu/astro/guides/vlas/current>.

⁵ <http://www.aoc.nrao.edu/evla/pbook.shtml>.

5 EMITTER LOCATIONS/ SITE LAYOUT

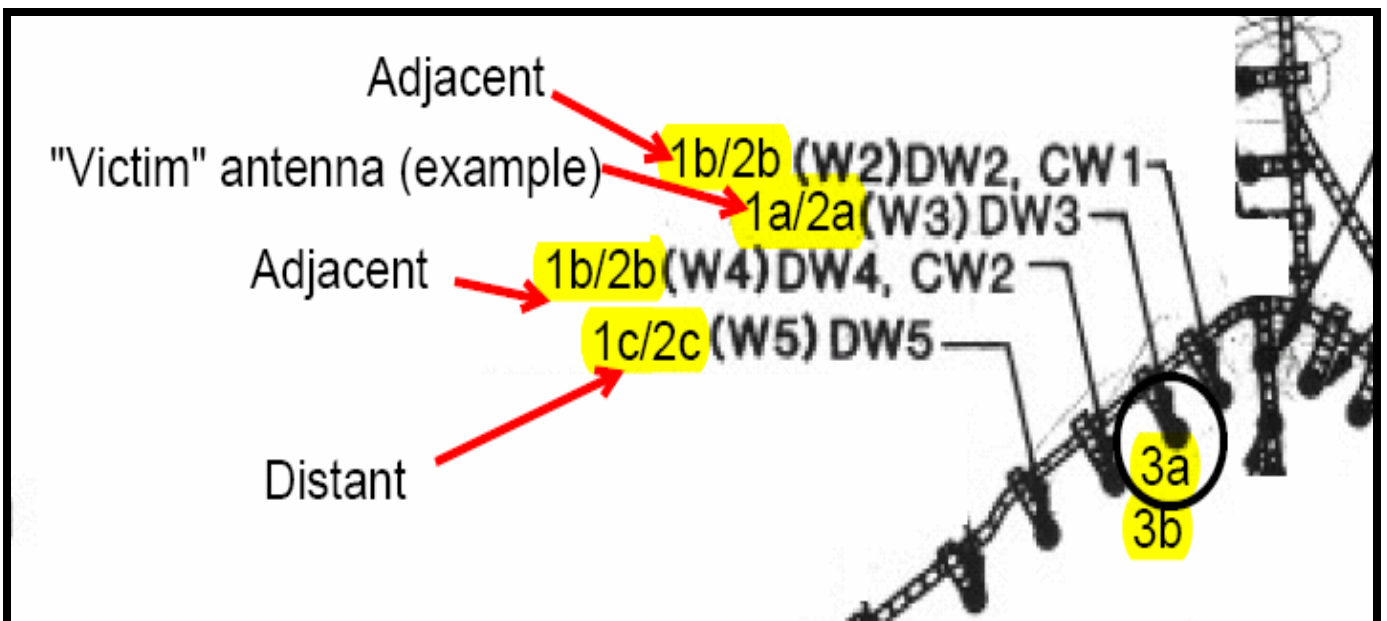
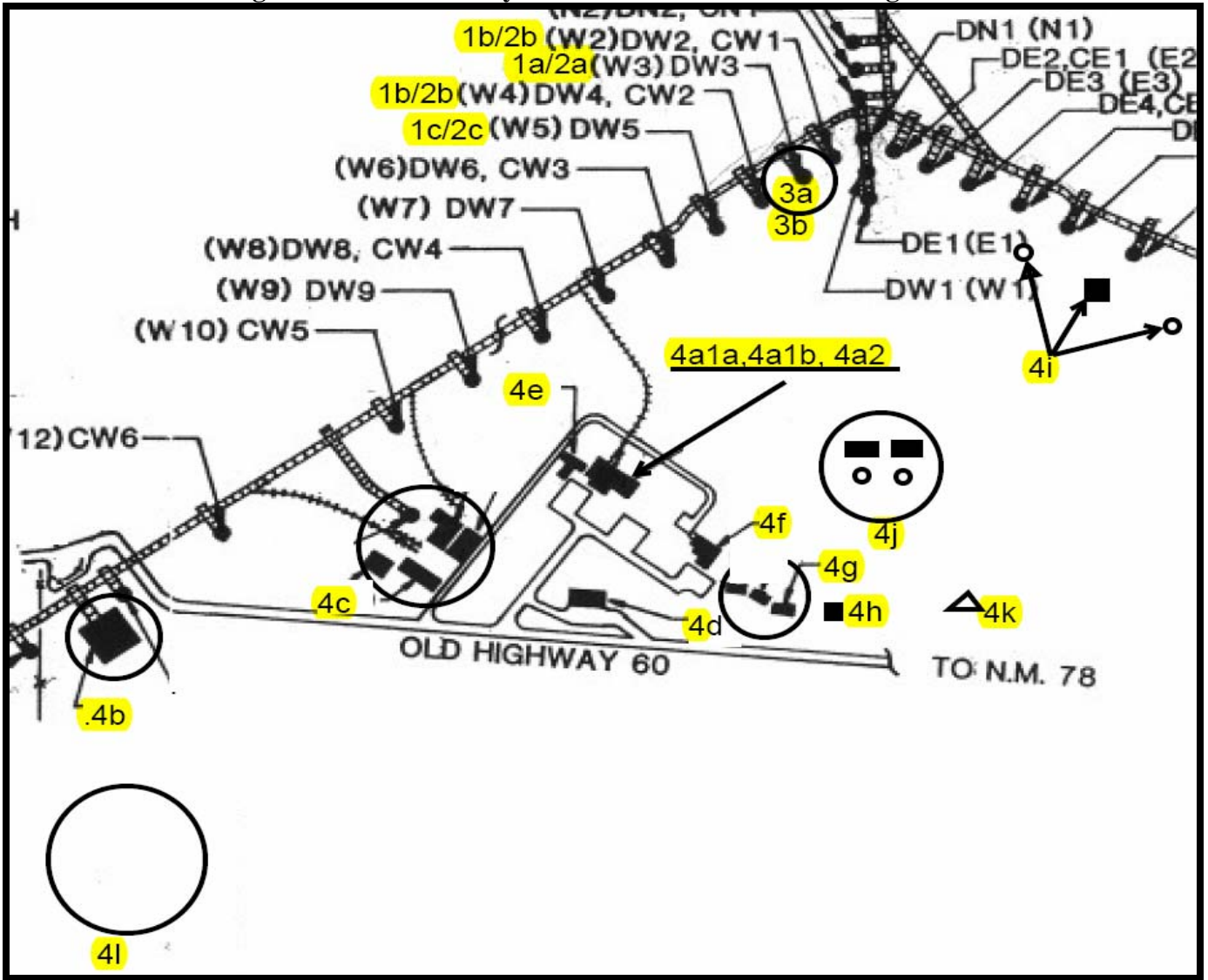
The RFI-generating equipment source locations can be broken down into the following broad categories, as itemized in List 1, and shown on the site layout (Diagram 1) below.

List 1: RF Emitter Location Designators.

- 1) Antenna vertex room
 - 1a) Same antenna vertex room
 - 1b) Adjacent antenna vertex rooms (adjacent pads, D configuration)
 - 1c) Distant antenna vertex rooms (> 1 pad, or 40m away⁶)
- 2) Antenna Pedestal room
 - 2a) Same antenna pedestal room
 - 2b) Adjacent antenna pedestal rooms
 - 2c) Distant antenna pedestal rooms (> 1 pad, or 40m away⁶)
- 3) Site grounds
 - 3a) Immediate proximity to antennas (distance \leq 40m away⁶)
 - 3b) Distant outdoor areas (distance > 40m away⁶)
- 4) Site buildings
 - 4a) Control Building (CB)
 - 4a1) Shielded CB areas
 - 4a1a) Operations control room
 - 4a1b) VLA Correlator room
 - 4a1c) EVLA Correlator room
 - 4a2) Unshielded areas (all other CB areas)
 - 4b) AAB (including attached buildings, paint shop, and trailers.
 - 4c) Tech Services building cluster (including MOS, Auto, Electrical, Carpentry, Warehouses)
 - 4d) Visitor's Center
 - 4e) SLOB building/FO Lab
 - 4f) Cafeteria
 - 4g) VSQ buildings
 - 4h) RF-EMS shelter
 - 4i) API shelter and antennas
 - 4j) ATF site trailers and antennas
 - 4k) ATF source tower
 - 4l) LWDA site shelter and antennas

⁶ Minimum VLA pad-to-pad distance, from "VLA Site – WYE Layout" drawing, B219001.

Diagram 1: VLA Site Layout with Emitter Location Designators.



6 PROPAGATION LOSSES AND SHIELDING FACTORS

Each location can have a propagation factor assigned to it according to the following key parameters:

6-1 FLUX SPREADING LOSSES

The strength of the electro-magnetic field flux dissipates proportionally to the expanding surface area of a sphere centered on the source, by a factor proportional to $1/(\text{distance}^2)$. Thus the PFD from a source with an effective Isotropic Radiated Power (EIRP) in the direction of the receiving antenna is equal to the pfd @ $r = 1\text{m}$, divided by the distance^2 factor listed above. The table 2, following, summarizes the distances used for calculating the flux spreading “loss” assumptions used in subsequent analysis.

6-2 ARCHITECTURAL SHIELDING LOSSES

The VLA Operations room in the Control Building was originally constructed with wire-mesh shielding installed in the walls, windows, ceiling, and floor. An attempt at characterizing the effective shielding of the room was made by Clint Janes in the mid 1990s, and yielded a figure of around 30 dB⁷—15 dB will be used for Interference Protection Group (IPG) analysis, as a conservative figure based on the results of C. S. Patcheck/IPG tests of 2002⁸. The VLA correlator room in the CB was originally designed to show greater than 90 dB of shielding to 1 GHz⁹. Age, use, and penetrations have deteriorated the shielding effectiveness of this room—50 dB will be used for IPG analysis, as estimated from the results of C. S. Patcheck/IPG tests of 2002¹⁰. The EVLA correlator room in the CB was originally designed to show greater than 100 dB of shielding to 10 GHz¹¹. Post installation penetrations have deteriorated the shielding effectiveness of this room to less than 80 dB, as estimated from tests of April, 2006¹². Subsequent improvements to the connector bulkhead should have improved this weak-point—90 dB will be used for IPG analysis. Other VLA site buildings (including the non-shielded areas of the CB) are constructed of various materials, such as corrugated steel, brick, press-board and glass, each yielding different, but not substantial shielding values—5 dB will be used for IPG analysis, by conservative estimate from the results of C. S. Patcheck/IPG tests of 2002¹³. The ALMA site trailers are of corrugated steel, and have wire-mesh shielding added to the windows. The minimal shielding value of the original construction (~ 10 dB, at best¹⁴), was improved later to a value of 30 dB in L-band¹⁵—20 dB will be used for IPG analysis based on these results. Tests by Philstrom and Mertely in August 2006 showed the shielding of the LWA shelter to be in the 30 dB range from VHF to C-band¹⁶--the RF-EMS and API shelters are assumed to have similar shielding. The table 2, following, summarizes the architectural shielding assumptions used in subsequent analysis.

⁷ Draft “EVLA Overall RFI Hardware Plan”, Appendix D, Table 2. Email dated 20020520. Clint Janes.

⁸ VLA-VLBA Interference Protection Memo #32, pg 27

⁹ By analogy with the EVLA correlator room, OEM default specification—See ***

¹⁰ VLA-VLBA Interference Protection Memo #32, pg 23

¹¹ USC Test Plan, “3.0 Test Specification Limits”.

¹² “EVLA Shielded Room re-test report”, Email dated 20060406. D. Mertely

¹³ VLA-VLBA Interference Protection Memo #32, pg 24, 25

¹⁴ VLA-VLBA Interference Protection Memo #32, pg 27

¹⁵ VLA-VLBA Interference Protection Memo #29, pg 1

¹⁶ “LWDA Equipment shelter shielding”, Attached spreadsheet, Position 1 results. Email dated 20060817. Dan Mertely

Table 2: VLA Site Flux Spreading Losses and Architectural Shielding Assumptions used.

BUILDING/AREA	LOCATION DESIGNATOR (LD) (FROM LIST 1)	DISTANCE USED (m)	ARC'TL SHIELDING USED (dB)	TOTAL "LOSSES" USED (dB)
ANT V-ROOM TO SAME ANT	1a	N/A	UNKNOWN	(VARIES) ¹⁷
ANT V-ROOM TO ADJ ANT	1b	40	30 ¹⁸	62
ANT V-ROOM TO DIST ANT	1c	80	30 ¹⁸	68
ANT P-ROOM TO SAME ANT	2a	N/A	UNKNOWN	TBD
ANT P-ROOM TO ADJ ANT	2b	N/A	UNKNOWN	TBD
ANT P-ROOM TO DIST ANT	2c	N/A	UNKNOWN	TBD
SITE GROUNDS, < 40m (PROX)	3a	20	0	26
SITE GROUNDS, > 40m (DIST)	3b	(VARIES)	0	(VARIES)
CB, OPS ROOM	4a1a	200	15	61
CB, VLA CORR ROOM	4a1b	200	50	96
CB, EVLA CORR ROOM	4a1c	200	90	136
OTHER VLA SITE BLDGS	4a2, 4b-4g	160-300	5	49
RF-EMS SHELTER	4h	450	30	83
API SHELTER	4i	100	30	70
ALMA TRAILERS	4j	300	20	70
ALMA TOWER	4k	450	0	53
LWDA SHELTER	4l	400	30	82

Table 3: EIRPmax, unshielded (dBW) allowed for each location by EVLA frequency band.

1a: using Ridgeway measured losses from vertex room to FE input.

All others: using total losses from Table 2, and det EIRP limits from Table 1, Column 6.

Loc Desig	Freq (GHz)	0.0738	0.328	1.5	3	6	10	15	23	34	45
1a		-114	-103	-78	-69	-57	-61	-53	-17	-12	-2
1b		-122	-111	-99	-90	-81	-74	-68	-60	-55	-50
1c		-116	-105	-93	-84	-75	-68	-62	-54	-49	-44
2a		TBD	TBD	TBD	TBD	TBD	TBD	TBD	TBD	TBD	TBD
2b		TBD	TBD	TBD	TBD	TBD	TBD	TBD	TBD	TBD	TBD
2c		TBD	TBD	TBD	TBD	TBD	TBD	TBD	TBD	TBD	TBD
3a		-152	-141	-129	-120	-111	-104	-98	-90	-85	-80
3b		VAR	VAR	VAR	VAR	VAR	VAR	VAR	VAR	VAR	VAR
4a1a		-123	-112	-100	-91	-82	-75	-69	-61	-56	-51
4a1b		-88	-77	-65	-56	-47	-40	-34	-26	-21	-16
4a1c		-48	-37	-25	--16	-07	0	+06	+14	+19	+24
4a2, 4b-4g		-135	-124	-112	-103	-94	-87	-81	-73	-68	-63
4h		-116	-105	-93	-84	-75	-68	-62	-54	-49	-44
4i		-114	-103	-91	-82	-73	-66	-60	-52	-47	-42
4j		-115	-104	-92	-83	-74	-66	-60	-52	-48	-43
4k		-131	-120	-108	-99	-90	-83	-77	-69	-64	-59
4l		-102	-91	-79	-70	-61	-54	-48	-40	-35	-30

7 INSTALLED SOURCES

List 2, following, is a sample of a working document which shall list existing and potential VLA site based RF emitters, and assign a type designator to each. Table 3, following, is a sample of a working document which shall document for each emitter type, the equipment model number, location(s), emissions tests performed, measured EIRP, required shielding, and mitigation measures taken for each

¹⁷ Table 1, "Suppression of Self-Generated RFI Emissions for the EVLA", R. Ridgeway, RFI2004, Penticton, Canada.

¹⁸ EVLA Memo #78, R. Ridgeway, Pg 2.

installation. The working document which includes List 2 and Table 3 shall be maintained by the Interference Protection Office in a group-accessible location on a NRAO server¹⁹.

List 2: RF Emitter designators (sample).

- a) COMMERCIALY PURCHASED EQUIPMENT
 - a1) PC EQUIPMENT
 - a1a) DESK TOP PCs
 - a1b) LAP TOP PCs
 - a1c) PDAS
 - a2) MONITORS/"DUMB" TERMINALS
 - a2a) CRT
 - a2b) LCD
 - a2c) PLASMA
 - a3) PRINTERS
 - a4) LAN EQUIPMENT
 - a4a) MEDIA CONVERTERS
 - a4b) HUBS
 - a4c) ROUTERS
 - a4d) SWITCHES
 - a4e) WIRELESS NETWORKS
 - a5) TEST EQUIPMENT
 - a5a) SIGNAL GENERATORS
 - a5b) SPECTRUM ANALYZERS
 - a5c) OSCILLOSCOPES
 - a5d) VOLT-OHM METERS
 - a6) SITE RADIOS
 - a6a) VHF
 - a6b) UHF
 - a6c) FRS
 - a6d) CB
 - a7) CELL PHONES
 - a7a) NRAO
 - a7b) PRIVATE
 - a8) CORDLESS PHONES
 - a8a) NRAO
 - a8b) PRIVATE
 - a9) POWER SUPPLIES
 - a9a) ON-ANTENNA
 - a9a1) LINEAR
 - a9a2) SWITCHING
 - a9b) BUILDING
 - a9b1) LINEAR
 - a9b2) SWITCHING
 - a10) WELDERS
 - a11) VEHICLES
 - a11a) GASOLINE
 - a11a) DIESEL
 - a12) AM/FM RADIOS
 - a13) TELEVISION MONITORS
 - a14) GPS RECEIVERS
 - a15) FLORESCENT LIGHTING
 - a16) APPLIANCES
 - a16a) OPERATOR'S KITCHEN
 - a16a1) OVENS
 - a16a2) TOASTERS
 - a16a3) COFFEE POTS
 - a16a4) REFRIGERATOR/FREEZERS
 - a16b) GENERAL KITCHEN

¹⁹ [http://www.aoc.nrao.edu/evla//techdocs/RFI/chamber-tests/EVLA-testing-status\[yyyymmdd\].doc](http://www.aoc.nrao.edu/evla//techdocs/RFI/chamber-tests/EVLA-testing-status[yyyymmdd].doc).

- a16b1) OVENS
- a16b2) TOASTERS
- a16b3) COFFEE POTS
- a16b4) REFRIGERATOR/FREEZERS
- a16c) PERSONAL
 - a16c1) OVENS
 - a16c2) TOASTERS
 - a16c3) COFFEE POTS
 - a16c4) REFRIGERATOR/FREEZERS
 - a16d5) SPACE HEATERS
- a17) DIGITAL CAMERAS
 - a17a) NRAO
 - a17b) VISITORS
- a18) AUTOMOBILE REMOTE CONTROLS
- a19) TELEPHONES (WIRED)
 - a19a) ANALOG
 - a19b) DIGITAL
- b) NRAO DESIGNED EQUIPMENT
 - b1) ANTENNA
 - b1a) VLA
 - b1a1) FRONT END RECEIVERS
 - b1a1a) F201 4m
 - b1a1b) F202 90cm
 - b1a1c) F103 20cm
 - b1a1d) A-rack 6cm/2cm
 - b1a1e) F106 4cm
 - b1a1f) F109 1cm
 - b1a1g) F110 6mm
 - b1a2) LO MODULES
 - b1a2a) L1 VCXO
 - b1a2b) L2 HARMONIC GENERATOR
 - b1a2c) L3 LO TRANSMITTER
 - b1a2d) L4 ANTENNA LO RECEIVER
 - b1a2e) L6 SYNTHESIZER
 - b1a2f) L7 FRINGE GENERATOR
 - b1a2g) L8 TIMING GENERATOR
 - b1a2h) F3 MICROWAVE LO
 - b1a3) CONVERTER MODULES
 - b1a3a) F11 4P UPCONVERTER
 - b1a3b) F2 L BAND UPCONVERTER
 - b1a3c) F12 XQ DOWNCONVERTER
 - b1a3d) F4 DOWNCONVERTER
 - b1a3e) F8 IF OFFSET
 - b1a3f) T2 IF COMBINER
 - b1a3g) T1 MODEM
 - b1a4) MONITOR AND CONTROL MODULES
 - b1a4a) F14 FRONT END CONTROL
 - b1a4b) L5 LO CONTROL
 - b1a4c) F5 A-RACK MONITOR AND CONTROL
 - b1a4d) M1 DATA SET
 - b1a4e) M2 DATA TAP
 - b1a4f) M3 CENTRAL BUFFER
 - b1a4g) M4 ANTENNA BUFFER
 - b1a4h) M5 COMMAND SIMULATOR
 - b1a5) POWER SUPPLIES
 - b1a5a) LINEAR
 - b1a5b) SWITCHING
 - b1b) EVLA
 - b1b1) FRONT END RECEIVERS
 - b1b1a) F201 4m
 - b1b1b) F202 90cm
 - b1b1c) F303 20cm

- b1b1d) F304 13cm
- b1b1e) F305 6cm
- b1b1f) F106 4cm
- b1b1g) F109 1cm
- b1b1h) F110 6mm
- b1b2) LO MODULES
 - b1b2a) L304 LO/REF RECEIVER
 - b1b2b) L305 REFERENCE GENERATOR AND DISTRIBUTION
 - b1b2c) L300 REFERENCE GENERATOR
 - b1b2d) L301 SYNTHESIZER
 - b1b2e) L302 SYNTHESIZER
- b1b3) CONVERTER MODULES
 - b1b3a) T301 4P CONVERTER
 - b1b3b) T302 LSC CONVERTER
 - b1b3c) T303 UX CONVERTER
 - b1b3d) T304 DOWN CONVERTER
 - b1b3e) D30X DTS
- b1b4) MONITOR AND CONTROL MODULES
 - b1b4a) F14 TRANSITION FRONT END CONTROL
 - b1b4b) F320 TRANSITION FRONT END CONTROL
 - b1b4c) F317 FRONT END CONTROL
 - b1b4d) T305 DOWNCONVERTER CONTROL
- b1b5) POWER SUPPLIES
 - b1b5a) LINEAR
 - b1b5b) SWITCHING
- b2) SITE BUILDINGS
 - b2a) VLA
 - b2a1) LO MODULES
 - b2a1a) T2 IF COMBINER
 - b2a1b) T1 MODEM
 - b2a2) MONITOR AND CONTROL MODULES
 - b2a2a) M1 DATA SET
 - b2a2b) M2 DATA TAP
 - b2a2c) M3 CENTRAL BUFFER
 - b2a2d) M4 ANTENNA BUFFER
 - b2a2e) M5 COMMAND SIMULATOR
 - b2a3) MARK 5 RECORDERS
 - b2a4) POWER SUPPLIES
 - b2a4a) LINEAR
 - b2a4a) SWITCHING
 - b2a5) CUSTOM TEST EQUIPMENT
 - b2b) EVLA
 - b2b1) LO MODULES
 - b2b1a) L350 REFERENCE GENERATOR AND DISTRIBUTION
 - b2b1b) L351 MASTER OFFSET GENERATOR
 - b2b1c) L354 LO DRIVER
 - b2b1d) L355 DIGITAL TIMING DISTRIBUTOR
 - b2b1e) L353 LO TRANSMITTER SYSTEM
 - b2b2) CONVERTER MODULES
 - b2b2a) T301 4P CONVERTER
 - b2b2b) T302 LSC CONVERTER
 - b2b2c) T303 UX CONVERTER
 - b2b2d) T304 DOWN CONVERTER
 - b2b2e) D30X DTS
 - b2b3) MONITOR AND CONTROL MODULES
 - b2b3a) M350 UTILITY MODULE
 - b2b4) POWER SUPPLIES
 - b2b4a) LINEAR
 - b2b4b) SWITCHING
 - b2B5) CUSTOM TEST EQUIPMENT

		4i 4j 4l			81 80 93	49/8 50/9 37/none	
a2b	LI LCD flat screen TV Model # 42LC2D	4d	emissions PC, mouse, LCD	-73/-83	60-65	51/29	

3 Equipment Screening Guidelines

With the proliferation of new RF and digital equipment being purchased and designed for use at the VLA site, it is critical that RF emissions screening guidelines be established for both commercially-purchased equipment, as well as NRAO designed modules or devices. These screening guidelines will be based on the likelihood that a device will exceed the EVLA detrimental thresholds at the nearest antenna, when installed at the anticipated VLA site “emitter location(s)” of List1/Diagram 1, above. The likelihood of a class of device exceeding the EVLA detrimental thresholds will be determined by the results of prior “emitter class” testing, and/or the engineering judgment of the Interference Protection Office engineering staff.

Equipment believed to have the greatest risk to EVLA scientific observing will be 100% screened—all such devices will be required to undergo RF emissions screening before they will be allowed to be installed at the VLA site. If emissions testing of such equipment indicates that the device will radiate above the EVLA detrimental thresholds from its anticipated installation point, the equipment will be shielded to below the threshold, or be tagged for turn-off during scientific observations.

Equipment already on-site and falling within the category of devices targeted for 100% screening will be emissions tested and tagged as such over the next year. Equipment found to exceed the EVLA detrimental levels detailed in EVLA memo #106 will be shielded to an emissions level below the detrimental levels, or will be tagged for turn-off during scientific observations.

Equipment of lower risk will be screened by “class”. If the class designation of a new equipment item indicates the likelihood of radiated emissions above the EVLA detrimental levels, the equipment will be shielded to an emissions level below the detrimental levels, or will be tagged for turn-off during scientific observations. If design or performance changes suggest a significant change in radiated power from that recorded during previous emissions tests of devices in a class, a new emissions test will be performed on a representative new equipment model in that class. Future equipment in that class will be required to be shielded to the level determined by the most recent RF emissions test.

The following is the equipment “class” list, listed in order of the likelihood of generating harmful RFI, and identified by the equipment class designator given in List 2, above:

List 3: Equipment Screening Priority.

1. Intentional radiators to be 100% screened:
 - a) COMMERCIALY PURCHASED EQUIPMENT
 - a6) SITE RADIOS
 - a6a) VHF
 - a6b) UHF
 - a6c) FRS
 - a6d) CB
 - a7) CELL PHONES
 - a7a) NRAO
 - a7b) PRIVATE
 - a8) CORDLESS PHONES
 - a8a) NRAO
 - a8b) PRIVATE
2. Un-intentional radiators to be 100% screened:
 - b) NRAO DESIGNED EQUIPMENT
 - b1) ANTENNA
 - b1a) VLA
 - b1a2) LO MODULES
 - b1a2e) L6 SYNTHESIZER

- b1a2h) F3 MICROWAVE LO
- b1a3) CONVERTER MODULES
 - b1a3b) F2 L BAND UPCONVERTER
 - b1a3c) F12 XQ DOWNCONVERTER
- b1b) EVLA
 - b1b2) LO MODULES
 - b1b2c) L300 REFERENCE GENERATOR
 - b1b2d) L301 SYNTHESIZER
 - b1b2e) L302 SYNTHESIZER
 - b1b3) CONVERTER MODULES
 - b1b3a) T301 4P CONVERTER
 - b1b3b) T302 LSC CONVERTER
 - b1b3c) T303 UX CONVERTER
 - b1b3d) T304 DOWN CONVERTER
 - b1b3e) D30X DTS

3. Un-intentional radiators to be sampled by class:

All equipment in List 2 not listed in “1. Intentional radiators” or “2. Un-intentional radiators”, above.

The emissions testing system currently used in the EVLA/ALMA reverberation chamber is unable to test to the EVLA Detrimental levels of EVLA memo #106 across all proposed EVLA receiving bands²⁰. As a result, all unintentional radiators identified for emissions testing will be tested with shielding covers removed or open. The shielding effectiveness of the total, in situ equipment shielding (module, bin, rack, and architectural) shall be tested separately. Shielding values so measured shall be deducted from the EIRP values calculated from the equipment emissions testing, before calculation of the PFD of the equipment emissions at the nearest antenna and comparison with the detrimental PFD levels. Emissions testing will be performed in accordance with the document, “**EVLA/ALMA Reverberation Chamber Emissions Testing Procedure**”²¹. Shielding effectiveness testing will be performed in accordance with the document, “**Reverberation Chambers**”²².

²⁰ As seen in Figure 10, “verizon-VX7000-emissions-test-results1.doc”, Email dated 20060406, D. Mertely, for example.

²¹ <http://www.aoc.nrao.edu/evla/techdocs/RFI/chamber-tests/test-procedures/emissions-test-proc1.doc>

²² <http://www.aoc.nrao.edu/evla/techdocs/RFI/chamber-tests/test-procedures/reverb.pdf>, Section 4.3, pg 6.