

VLBA ACQUISITION MEMO #152

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5 June 1989

Area Code 508

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To: VLBA Data Acquisition Group
From: Alan E.E. Rogers
Subject: A Magnetic circuit model for the VLBA headstack

The VLBA narrow track headstacks have a gap length of $0.33 \mu\text{m}$, width of $38 \mu\text{m}$ and thus a gap reluctance $R_g = 180 \text{ Ma/Wb}$ (mega amp-turn/weber) for a depth of gap equal to $38 \mu\text{m}$ reluctance for the rest of the magnetic circuit as follows (assuming a relative permeability of ferrite equal to 700).

$$R_c \text{ (ferrite through coil)} \approx 5 \text{ Ma/Wb}$$

$$R_t \text{ (ferrite in tip plate)} \approx 2 \times 30 \text{ Ma/Wb}$$

unless there is significant reluctance in the contact gap between the "tip" plate and "fluxor". For example:

$$R_b \text{ (contact gap)} = 160 \text{ Ma/Wb for } 30 \mu\text{m}$$

contact thickness. Figure 1 shows the magnetic circuit geometry. In addition to the gap reluctance and series reluctance there is magnetic field leakage which acts as reluctance in parallel. I estimate the following leakage field reluctances:

$$R_a \text{ (apex angle leakage)} \approx 3000 \text{ Ma/Wb}$$

$$R_o \text{ (head coupling)} \approx 150 \text{ Ma/Wb}$$

The leakage reluctance is primarily between heads with two paths from one head to each adjacent head. The Table gives the magnetic flux paths, their reluctance and the inductances which results from these paths. Figure 2, the equivalent circuits for evaluating the head efficiency as a function of the gap reluctance and the cross-talk between heads.

In summary the series reluctance in the ferrite tip plate results in about 3 dB loss for an initial depth of gap of 38 microns, so that the head performance is expected to improve by 3 dB as the head wears. The leakage between heads can produce significant record cross-talk of about -4 dB in the worst case when interference from adjacent heads are in phase. The record cross-talk can be eliminated by ensuring that the circuitry connected to the undriven head produces only a small current in response to the voltage cross-talk and steps are being taken to reduce the loading of the undriven heads in both the MKIIIA and VLBA recorders. It might also be possible to eliminate the record cross-talk by reducing the speed of the record current risetime. [The record cross-talk consists of very narrow ($\approx 8 \text{ ns}$) pulses which are just sufficiently strong to magnetize the particles

in the gap at the time of the pulse.] In the long term it may also be possible to reduce the flux leakage between heads by reducing the cross section of the fluxor ferrite in future headstack designs.

<u>Item</u>	<u>Length μm</u>	<u>Area $\mu\text{m} \times \mu\text{m}$</u>	<u>Relative Permeability</u>	<u>Reluctance Ma/W</u>	<u>Inductance μH</u>
Head Gap	0.33	38 x 38	1	180	
Tip Plate	150	150 x 38	700	30 ⁺	
Coil	400	300 x 300	700	5	
Leakage between heads	400	800 x 1400 *(1200 x 1800)	1	150	
Apex leakage			3000		
Coil					23
Mutual between heads					7

*Effective Cross Section Area

⁺ Approximate estimate only - geometry is complicated

Table. The Reluctance of Magnetic Flux Paths in the VLBA Heads

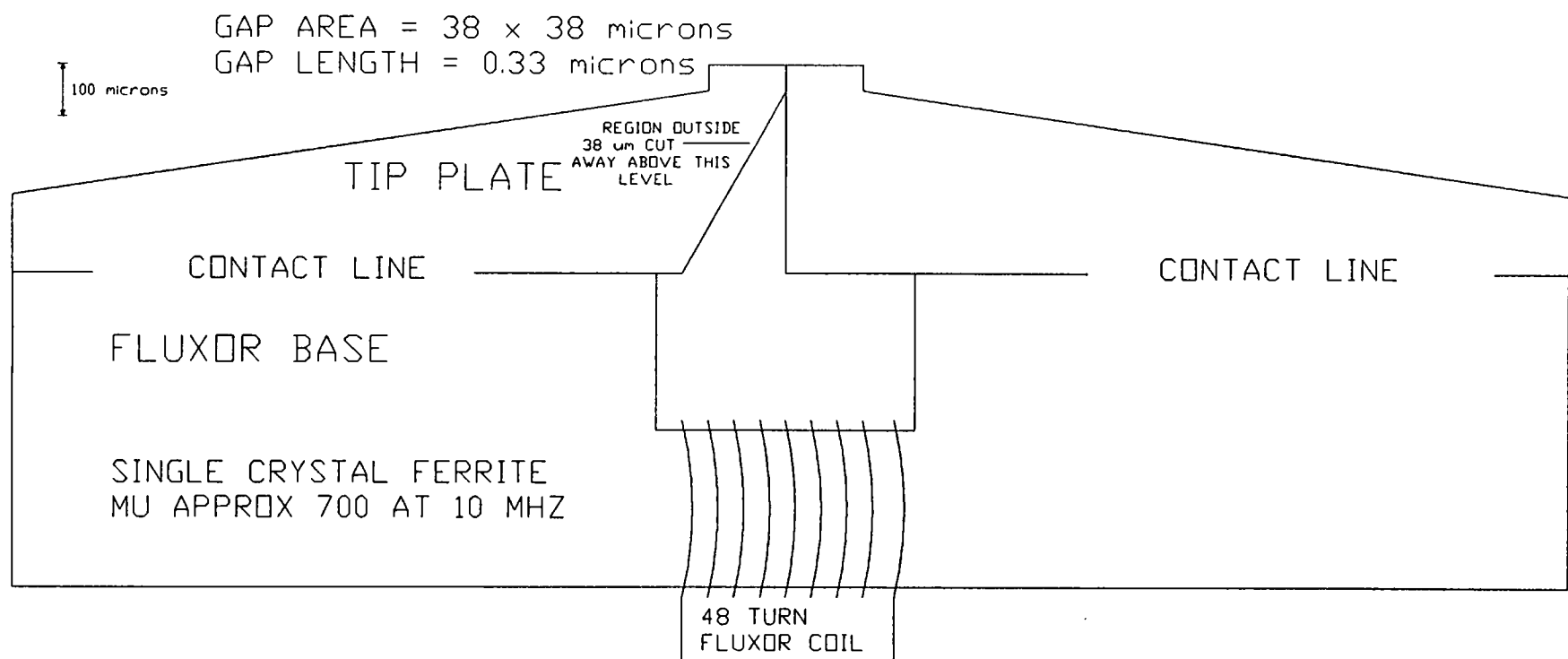
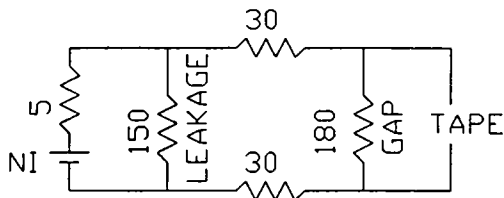
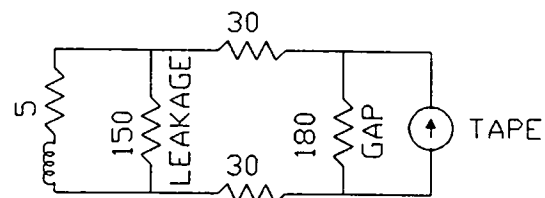


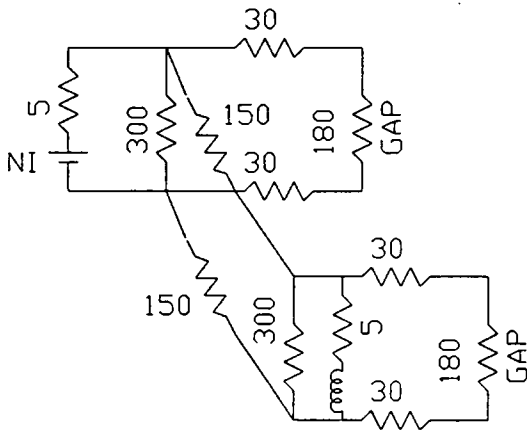
FIGURE 1 MAGNETIC CIRCUIT GEOMETRY (GAP AREA SHOWN FOR DEPTH OF GAP = 38 MICRONS)



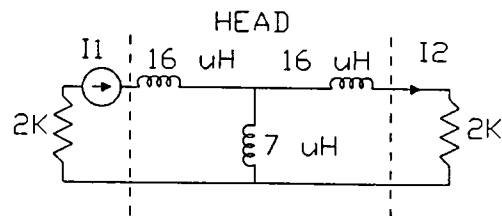
"DC" FIELD CIRCUIT FOR
RECORD EFFICIENCY AND
INDUCTANCE
(-3 dB relative to zero gap
depth, inductance = 23 mH)



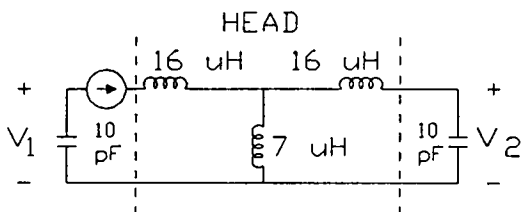
"DC" FIELD CIRCUIT FOR
REPRO EFFICIENCY
(-3 dB relative to zero
gap depth)



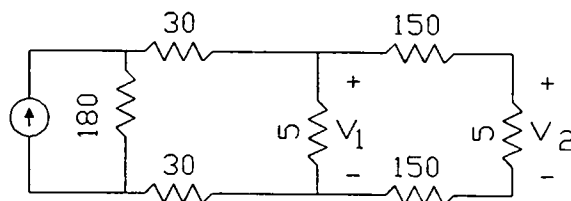
"DC" FIELD CIRCUIT FOR ESTIMATION
OF MUTUAL INDUCTANCE
(coupling coeff. 0.3
mutual inductance = 7 uH)



EQUIVALENT CIRCUIT FOR
RECORD CROSS-TALK
(record cross-talk = $I_2/I_1 = -10$ dB
in HF limit or -4 dB from "in phase"
interference from both adjacent heads)



EQUIVALENT CIRCUIT FOR HF
REPRO CROSS-TALK TO BE ADDED
TO LF CROSS-TALK
($V_2/V_1 = -27$ dB at 4 MHz)



EQUIVALENT CIRCUIT FOR LF
REPRO CROSS-TALK
($V_2/V_1 = -36$ dB)

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FIGURE 2 EQUIVALENT CIRCUITS FOR VLBA
RECORDER HEADS