VLBA ACQUISITION MEMO #366

National Radio Astronomy Observatory

New Mexico August 17, 1993

To: VLBA Data Acquisition Group

From: Bryan Martin Summer Student NRAO, NM

Subject: Methods of remotely monitoring power supply voltages in VLBA equipment racks

Introduction:

It is desirable to remotely monitor the power supply voltages in the recorders, D racks, and C racks at the VLBA sites. This would aid in diagnosing problems with these components. Currently, this monitoring is not being done. I was assigned the task of investigating methods of remotely monitoring the power supply voltages.

There are 12 power supply voltages to monitor in each recorder. The analog power supply puts out five: +15V, -15V, +12V, -12V, and variable write. The digital power supply puts out two: +5V and -5.2V. The Honeywell unregulated power supply puts out two: +33V and -33V. The Honeywell regulated power supply puts out three: +12V, -12V, and +5V. The D rack is powered by five power supplies: two 15 volt supplies and three 5 volt supplies. The C rack is powered by three power supplies: +15V, -15V, and +5V. This gives a total of 32 power supply voltages to monitor at each VLBA site building.

Discussion:

Power Monitoring can be easily provided in the C rack. Two modules in this rack use VLBA standard interface boards to communicate with the MCB bus: the round-trip phase monitor and the maser interface. The maser interface has four open analog channels and the round-trip phase monitor has seven. Both modules have plenty of room to add the necessary circuitry to monitor the power supplies.

Unfortunately, the recorders and all of the modules in the D racks use a modified version of the standard interface; the modification 'consists of incorporating the interface into another board and eliminating the analog monitoring capabilities entirely. Because of this design decision, some other method of monitoring the power supply voltages must be found.

I considered five methods of monitoring the power supply voltages in the recorders and D racks. These are: using the R122 analog I/O board, using an alternative analog VME interface board, adding the analog circuitry to the existing MCB interface, using a new module designed around a VLBA standard interface board, and monitoring the D rack via a module in the C rack.

Analog I/O board R122:

The recorder has an analog board in it; a Xycom XVME-540. This analog I/O board provides some analog monitoring capability. The analog I/O board does not interface directly with the MCB bus; It interfaces with the VME bus in the recorder rack. The analog I/O board has both A/D and D/A capabilities. The A/D section is configured for 16 differential inputs. The input voltage to each channel is limited to + or - 10 volts. Five of the 16 channels are currently in use, leaving only 11 for expansion; at least 12 channels are required.

Since there are not enough open channels left for monitoring the power supplies, either the present boards would have to be modified or a second board would have to be acquired for each recorder. I believe the first option, modifying the boards, is impractical. The boards are already very densely packed with components; there is no room for expansion. The second option, acquiring additional boards, would be very expensive; the list price of these modules from Xycom is \$1700 each.

The D racks have no analog monitoring capability built into them at all. The same analog board used in the recorder could be added to the formatter chassis in the D rack to add analog monitoring capability. But again, the cost would be high.

Many of the voltages in the recorders and D racks are out of the maximum input voltage range of the R122 boards. Because of this, an additional module would have to be added to each rack to convert the voltages to a form usable by the R122 boards. These new modules might add up to \$300 per rack to the cost. The recorder rack uses NIM type modules while the D rack uses NRAO type modules. This means that different converter modules must be used for the recorders and D racks. The R134 analog conditioner module might be modified do this job in the recorder but a new module must be built for the D rack.

This plan calls for adding one or two new modules in each rack and possibly modifying another module. There are enough empty slots in both the recorder and the D racks to implement this solution. Using the Rl22 boards for monitoring the power supplies would also require modifications to the VME controller firmware. A change which may have adverse implications for non-NRAO users of the recorders and formatters. The per-station cost of this plan would be about 6000 ($1700 \times 3 + 300 \times 3$).

Alternative analog VME interface board:

An alternative to acquiring more R122 boards would be to obtain or

build a much simpler analog board for the recorders and D racks to interface with the VME bus. The R122 board contains 16 A/D inputs and four D/A outputs. This complexity is not necessary for monitoring the power supplies.

The Xycom XVME-500/l is one VME bus board that would work for this application. This board can be configured for 16 single ended analog inputs and lists for \$725. This board has the same input voltage limitations as the R122 board so separate voltage conversion modules (at \$300 each) would also be required with this board.

This plan would cost about \$1000 per rack or \$3000 per station; which is much less expensive than obtaining more R122 boards. However, it would still require modifying the firmware in the VME controllers.

Adding the analog circuit to existing MCB interface:

The MCB interface for the recorder is built into the recorder transport module. There is not enough room on this board to install the Burr-Brown SDM854 data acquisition circuit used in the standard MCB interface; this circuit (see Figure 1) is way too large. However, the SDM854 is an old design; newer designs are available which are much smaller. The Burr-Brown SDM862 (see Figure 2) has capabilities and specifications very similar to the SDM854 but is less than one-fourth the size. An SDM862 installed in an adapter socket (see Figures 3,4,and 5) would just fit on the transport module circuit board (Figure 6) and would provide 16 single-ended input channels. Wiring would have to be added to the recorder to route the 12 power supply voltages to the transport module for monitoring.

The SDM862 requires a + and -15 volt power supply. This supply is not available on the transport module but is available in the recorder rack. The SDM862 could be supplied with + and -15 volts either by tapping off the power supply in the recorder rack or by installing a DC/DC converter, such as the TW1.8-12-15 from Polytron Devices (Figure 7), on the transport module.

SDM862s cost \$104 each. The DC/DC converter lists for \$34 each. The total cost for materials to implement this modification should be less than \$300 per recorder. This plan requires no firmware changes. MCB address space is available for this expansion; for instance addresses 20-2F are not currently in use.

This plan would not work for the D rack. None of the modules in The D rack that interface with the MCB bus have room for the necessary circuitry. Figure 8 shows the layout of the Formatter timing and control module, which contains the MCB interface. The other modules in the D rack have even less room for expansion.

VLBA Standard Interface Board:

I next considered using a system designed around the VLBA standard interface board. This board has an A/D circuit with eight differential analog inputs built into the board and can easily be expanded to include up to 64 analog channels. The standard interface board and voltage conversion circuitry could be built into an NRAO type module and installed in an open slot in the D rack.

The conversion circuitry is required to convert the power supply voltages down to the + or - 10 volt range required by the A/D converter. This would provide eight analog input channels. A similar plan could be used in the recorder but would require different packaging unless the interface for both the recorder and D rack were built to fit in a 2/3 height VME bus slot.

One slot in the D rack (Bin C, Slots 11-12) is already wired for an interface module; all of the power supply voltages and the MCB lines are routed to the rear connector in this slot. The installation would consist of removing a blank plate, sliding the module into the empty slot, and installing some new software on the station computer. No firmware changes are required.

The standard interface boards cost about \$400; the additional circuitry and hardware might add \$300 more to the cost for a total of \$700 per rack, or \$2100 per station if used in both recorders and the D rack.

Monitoring the D rack via the C rack:

The C rack and D rack are adjacent to each other at the VLBA sites. The C rack has enough open analog channels available to monitor the power supplies in both racks. The three voltages in the C rack could be monitored in the maser interface module where there are four open channels, and the five voltages from the D rack could be monitored in the round-trip phase monitor module where there are seven open channels. It would be easy to route a cable from the power supply terminals in the D rack to the round-trip phase monitor module in the C rack. Some additional circuitry would be required in these modules but there is plenty of room available. This plan would involve very little additional cost, probably about \$100.

Conclusion:

Adding remote monitoring of the C rack can be done easily and with very little cost because of the open channels on the standard interface boards already in this rack. The D rack can also be monitored from the C rack for an additional cost of about \$100. A cleaner, although more expensive solution for the D rack would be to add an MCB interface module, at a cost of \$700. The recorder has some analog capability, but not enough. The best solution for the recorder is to add the analog monitoring capability to the MCB interface on the transport module at a cost of \$300 per recorder. The material cost of adding remote monitoring of the power supplies in the C and D racks and two recorders would thus range from about \$700 on up.

BURR-BROWNS

SDM854

FOR A COMPLETE DATA SHEET, SEE PDS-423D

HYBRID DATA ACQUISITION SYSTEM

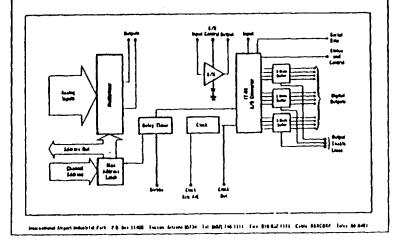
FEATURES

The SDA1834 is a complete data acquisition system

• 12 BIT, 10012% LINEARITY ERROR • INPUTS UP TO 210 VOLTS • WIGE TEMPERATURE RANGE • RELECTABLE 18 BINGLE. B DIFFERENTIAL INPUTS • THREE-STATE OUTPUT BUFFERS

DESCRIPTION

contained in a minimuture 2.2" a 1.7" a 0.22" (35.9 min a 43.2 min a 3.6 mm) creaning package. This system offers all the functions similable in large modular data acquisition systems. Inputs up to 2.10V can be accepted and low-level inputs can be accommisdated by connecting an external instrumentation amplifier to the output of the multiplears and to the input of - the sample/hold amplifier. Digital resolution is 12 bits with accuracy of 20.024% at a throughput rate of 22% (17



SYSTEM DESCRIPTION

The NDA1834 contains all components necessary to multiplex and consect analog signals up to 210V into cyuralent digital outputs. Throughput sampling cares are from 21849 (12-bit resolution) to 70k117 (8-bit resolution) in the overlap mode of operation. The NDVR19 con be configured to accept either 8 channel differentiator 16 channelsingle ended signals and can be expanded almost withous timit with exceedal moltiplevers. Three-state outputs are priviled after cary interface to inscroprocessor and other howstrocture system. The system components are fluxtrated in Figure 1 and descended in the following paragraphs.

ANALOG MULTIPLEXER

The analog multiple ser consists of two CMUS integrated circuits. Prin interconnects are used to select 18-channel ungle ended of 8 channel differential operation. In ungle-ended operation the multiplearer can be used in a pieudodifferential mode by connecting an external amplifier's inverting input to common remote signal ground. Channel selection is made by an internally latched 3- or 4 bit binary word, for differential or single-ended operation respectively.

SAMPLE/HOLD

Figure 1

A complete stand-atone circuit, the sample/hold amplifice features buffered output, 10µxec acquisition sime, and 100nsec aperture time.

Input, output, and mode control lines are brought out to separate prior. This allows maximum system Resibility for performing functions, such as automatic gain ranging, with no loss of specture time.

ANALOG-TO-DIGITAL CONVERTER

The ADC is a 12-bit, 25pisec converser with 0.01% linearity error its features include positive and negative reference voltage uniputs, asternal gain and offset adjustments, itraight binary or swoll complement output, itrial data and clock outputs, status output, a short cycle feature, and a clock rate contol for higher throughput rates at lower etsulution or accuracy.

THREE-STATE OUTPUT BUFFERS

Digital outputs of the ADC are internally buffered by LSTT4 three-state buffers. Three separate enable lines are brought outfor easy interfacing to 4-, 8- or 16-bit data buses. MSB and BUSY are also buffered by separate three state devices, each with its own enable line.

ADDRESS LATCH

Outputs of the 4-bit LSTEL register latch are connected to the address inputs of the multiple.ser. This latch serves as an address storage register for the selected analog input. It may be loaded through 4 address inputs. Other inputs are LOAD and CLEAR. The 3 least significant bits are used for 8-channel differential mode addressing

DELAY TIMER

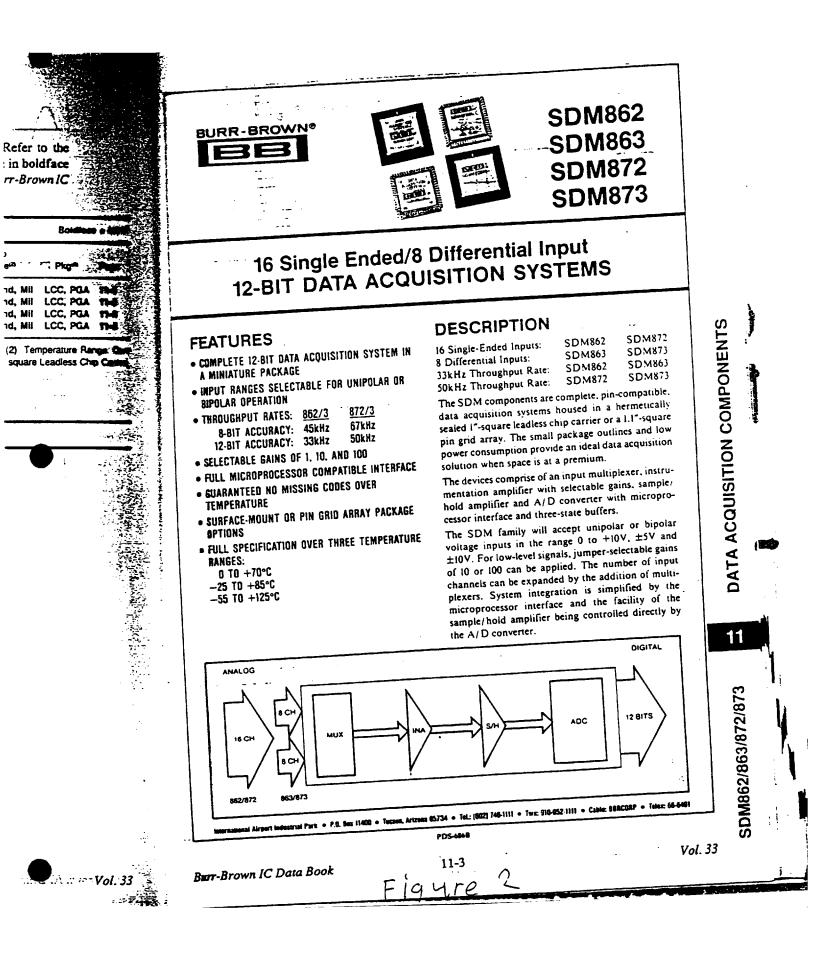
A delay timer allows settling time for the multiple set and sampler hold circuits before conversion begins. The delay is adjustable over a wide range by use of an external resistor or capacitor. This allows for longer settling time if an asternal instrumentation amplifier is used and it operating at high gains, or shorter setting time for lower resolution uperation.

CHANNEL EXPANSION

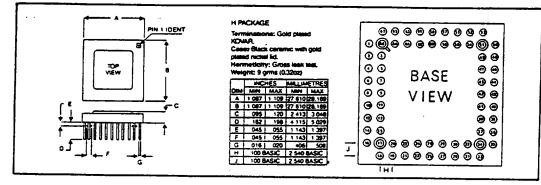
The number of analog input channels of the SDM834 can be easily increased by using Burr Brown's MPCID 65 channel differentials and MPCIDs (16 channel singleended) multipleates. These are facto-free devices which contain internel binary decoding at TTL or MOS kiels and may be integrated into a system with minimal casts nall ligit.

SYSTEM PERFORMANCE

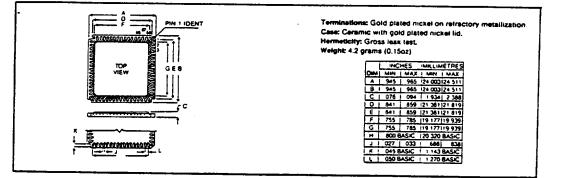
The SDM854 is configured for random channel selection. With the addition of an external counter they can be configured to continuously sequence through all ar-log channels or sequence through all analog channels of command from an external trigger.



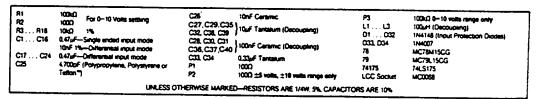
P.G.A. MECHANICAL OUTLINE



LC.C. MECHANICAL OUTLINE



P.C.B. COMPONENTS PARTS LIST



ORDERING INFORMATION"

Model	Input	LCC. PGA Pitg.	Accuracy [% FSR]	Throughput	Temp. Range (*C)	Model	Input	LCC, PGA Pkg.	Accuracy (% FSR)	Throughput	Toma. Range (*C
SDM862J [®] SDM862K SDM862A SDM862A SDM862B SDM862R SDM862S	165E 165E 165E 165E 165E		±0.024 ±0.012 ±0.024 ±0.012 ±0.024 ±0.012	33kHz 33kHz 33kHz 33kHz 33kHz 33kHz	0 to +70 0 to +70 -25 to +85 -25 to +85 -55 to +125 -55 to +125	SDM863J SDM863K SDM863A SDM8638 SDM863R SDM863S	8DIF 8DIF 8DIF 8DIF 8DIF 8DIF		±0.024 ±0.012 ±0.024 ±0.012 ±0.024 ±0.024 ±0.012	33kHz 33kHz 33kHz 33kHz 33kHz 33kHz 33kHz	0 to +7; 0 to +7; -25 to +8; -25 to +8; -55 to +12; -55 to +13;
SDM872J SDM872K SDM872A SDM872B SDM872R SDM872S	165E 165E 165E 165E 165E 165E	*****	± 0.024 ± 0.012 ± 0.024 ± 0.012 ± 0.012 ± 0.024 ± 0.012	SORHZ SORHZ SORHZ SORHZ SORHZ SORHZ	0 to +70 0 to +70 -25 to +85 -25 to +85 -55 to +125 -55 to +125	SOM873J SDM873K SDM873A SDM873B SDM873R SDM873R	8DIF 8DIF 8DIF 8DIF 8DIF 8DIF 8DIF		± 0.024 ± 0.012 ± 0.024 ± 0.012 ± 0.012 ± 0.024 ± 0.024 ± 0.012	50kHz 50kHz 50kHz 50kHz 50kHz 50kHz	0 10 + 73 0 10 + 73 - 25 10 + 68 - 25 10 + 68 - 55 10 + 73 - 55 10 + 730

NOTES: (1) LCC Evaluation Board Part Number: PC852/853-1. PGA Evaluation Board Part Number: PC852/853-2. (2) 16 single-ended result L23 package, with accuracy of 0.024% FSR. Temp Range of 0° C to 70° C and throughput of 33kHz = SDM862/L. Tefles** E.L de Post de Nexeers & Co.

11-24

Figure 3

Burr-Brown IC Data Book

Val M

SURF!

Burr-Brown offe mount packages. of a PC board, off these functions. N cavities and may concentrates prim number of leads:

SOIC

Plastic small-outlin example, the SOIC

LCC

Ceramic leadless c. ample, the LCC-20

STAY UP TO I

Burr-Brown is conti surface mount packa resentative. See the i

Brown IC Data Book

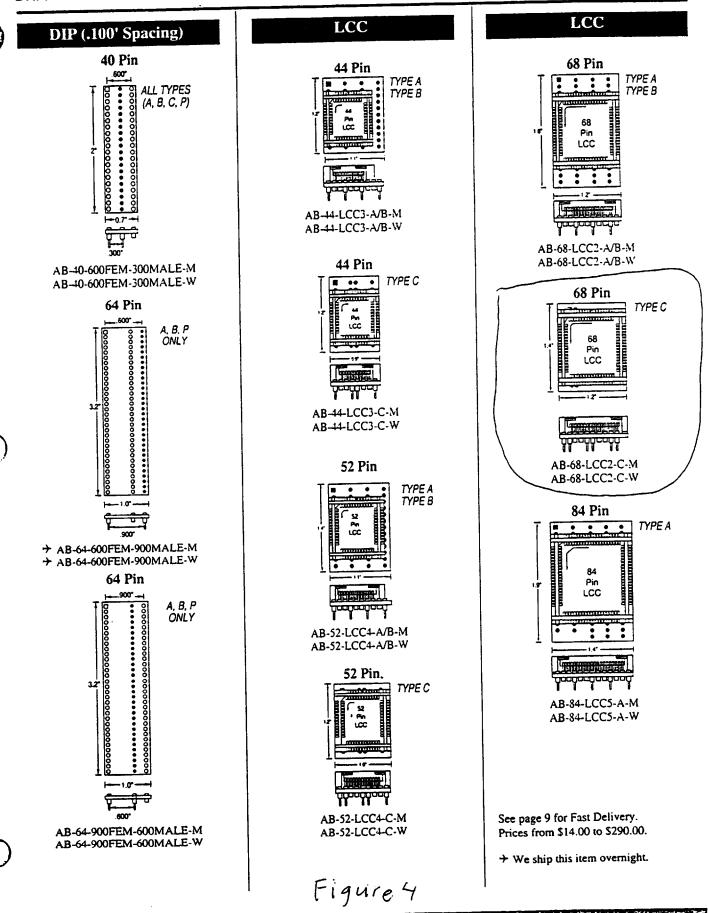
Emulation Technologies

DRAWINGS ARE NOT TO SCALE

ביוון ביות ביול איר ביויין בייני בייל איר בייל בייל איר ב

and and the second s

PROTOTYPING ADAPTERS



Don't forget our Overnight Delivery! 111

Emulation Technologies

DRAWINGS ARE NOT TO SCALE Ε -PGA PGA 68 Pin 68010 52 Pin TYPE A : TYPE B 9x9 GRID Vaccancen Sec. Sec. Sec. AB-52-PGA6-A/B-M AB-52-PGA6-A/B-W 68 Pin 52 Pin TYPE C 00 :: 9x9 GRID 1* AB-52-PGA6-C-M AB-52-PGA6-C-W 84 Pin 68 Pin 60266 TYPE A : : TYPE B der Meine auswessen mitte

• :

12

→AB-68-PGA1-A/B-M

→AB-68-PGA1-A/B-W

68 Pin

All all and a second

AB-68-PGA1-C-M

AB-68-PGA1-C-W

...

80286

.....

and the fifth of second production of the second second second second second second second second second second

ST. DOT

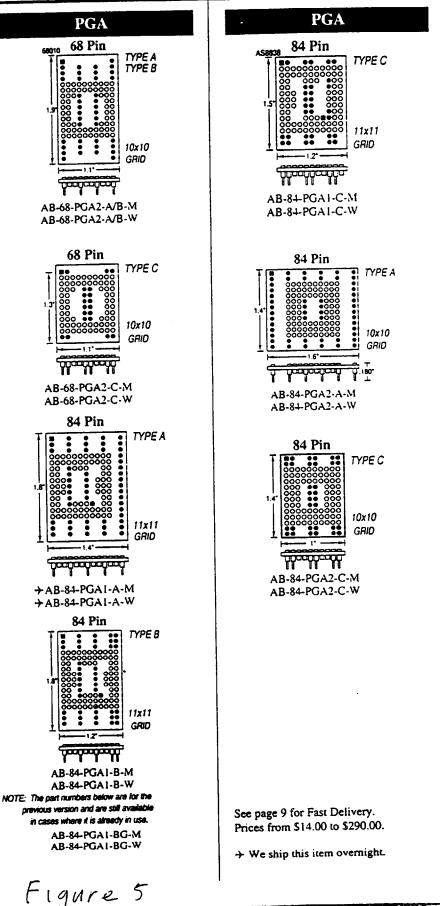
11x11

GRID

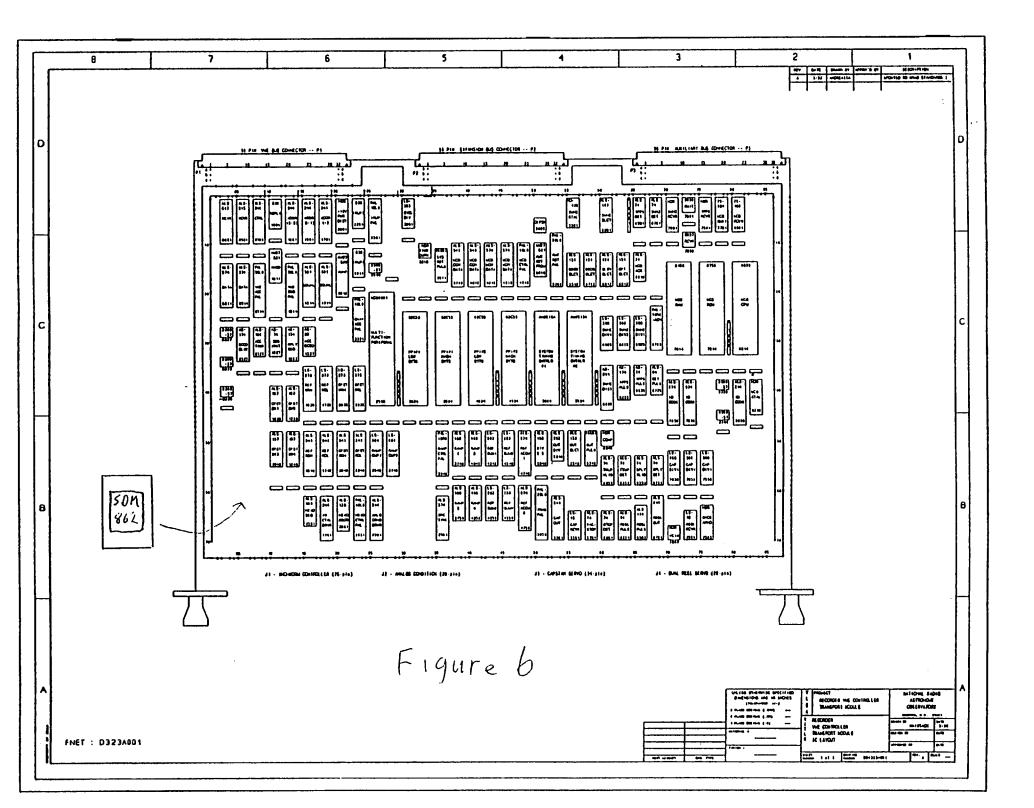
TYPE C

11x11 GRID





5



	4000
$\frac{1}{10} = \frac{1}{10} $	
$\frac{1}{100} = \frac{1}{100} = \frac{1}$	1
$\frac{1}{10} = \frac{1}{10} $	
$\frac{1}{2} = \frac{1}{2} = \frac{1}$	
$\frac{1}{10}$	م میں ملک ملک میں اور میں اور میں میں اور میں میں اور میں
$\frac{1}{200} = \frac{1}{200} = \frac{1}{10} = \frac{1}{10$	
$\frac{112}{210} + \frac{115}{12} + \frac{100}{120} + \frac{100}{100} + \frac{100}{100} + \frac{100}{120} + \frac$	
$\frac{11}{2100} = \frac{112}{22} = \frac{122}{200} = \frac{1112}{100} = \frac{122}{100} = \frac{122}{10} = \frac{122}$	
	م معرف فران مع م این معرف فران معرف این معرف معرف
$\begin{array}{c} 15 & \pm 100 & \frac{1}{100 + 48 + 5} & \frac{300}{200} \\ \hline 15 & \pm 180 & \frac{1}{100 + 48 + 5} & \frac{300}{2100} \\ \hline 12 & \pm 5 & \pm 300 & \frac{1}{100 + 48 + 12} & \frac{3400}{2300} \\ \hline 12 & \pm 12 & \pm 125 & \frac{1}{100 + 48 + 15} & \frac{3300}{2300} \\ \hline 115 & \pm 100 & \frac{1}{100 + 48 + 15} & \frac{3300}{2300} \\ \hline 12 & \pm 15 & \pm 100 & \frac{1}{100 + 48 + 15} & \frac{3400}{2300} \\ \hline 12 & \pm 15 & \pm 100 & \frac{1}{100 + 48 + 15} & \frac{3400}{2300} \\ \hline 12 & \pm 10 & \frac{1}{100 + 15} & \frac{1}{100 + 15} & \frac{1}{100 + 15} \\ \hline 12 & \pm 100 & \frac{1}{100 + 15} & \frac{1}{100 + 15} & \frac{1}{100 + 15} \\ \hline 10 & \frac{1}{100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 $	· · ·
$\begin{array}{c} 15 & \pm 100 & \frac{1}{100 + 48 + 5} & \frac{3200}{2100} \\ \hline 15 & \pm 180 & \frac{1}{100 + 48 + 5} & \frac{3200}{2100} \\ \hline 12 & \pm 5 & \pm 300 & \frac{1}{100 + 48 + 12} & \frac{3200}{2100} \\ \hline 12 & \pm 12 & \pm 125 & \frac{1}{100 + 48 + 15} & \frac{3200}{2100} \\ \hline 115 & \pm 100 & \frac{1}{100 + 48 + 15} & \frac{3200}{2100} \\ \hline 12 & \pm 15 & \pm 100 & \frac{1}{100 + 48 + 15} & \frac{3400}{2100} \\ \hline 12 & \pm 100 & \frac{1}{100 + 48 + 15} & \frac{3400}{2100} \\ \hline 12 & \pm 100 & \frac{1}{100 + 48 + 15} & \frac{1}{2100} \\ \hline 12 & \pm 100 & \frac{1}{100 + 48 + 15} & \frac{1}{2100} \\ \hline 12 & \pm 100 & \frac{1}{100 + 100} \\ \hline 12 & \pm 100 & \frac{1}{100 + 100} \\ \hline 12 & \pm 100 & \frac{1}{100 + 100} \\ \hline 12 & \pm 100 & \frac{1}{100 + 100} \\ \hline 12 & \pm 100 & \frac{1}{100 + 100} \\ \hline 12 & \pm 100 & \frac{1}{100 + 100} \\ \hline 12 & \pm 100 & \frac{1}{100 + 100} \\ \hline 12 & \pm 100 & \frac{1}{100 + 100} \\ \hline 12 & \pm 100 & \frac{1}{100 + 100} \\ \hline 12 & \pm 100 & \frac{1}{100 + 100} \\ \hline 12 & \pm 100 & \frac{1}{100 + 100} \\ \hline 12 & \pm 100 & \frac{1}{100 + 100} \\ \hline 12 & \pm 100 & \frac{1}{100 + 100} \\ \hline 12 & \pm 100 & \frac{1}{100 + 100} \\ \hline 12 & \pm 100 & \frac{1}{100 + 100} \\ \hline 12 & \pm 100 & \frac{1}{100 + 100} \\ \hline 12 & \pm 100 & \frac{1}{100 + 100} \\ \hline 12 & \pm 100 & \frac{1}{100 + 100} \\ \hline 12 & \pm 100 & \frac{1}{100 + 100} \\ \hline 12 & \pm 100 & \frac{1}{100 + 100} \\ \hline 12 & \pm 100 & \frac{1}{100 + 100} \\ \hline 12 & \pm 100 & \frac{1}{100 + 100} \\ \hline 12 & \pm 100 & \frac{1}{100 + 100} \\ \hline 12 & \pm 100 & \frac{1}{100 + 100} \\ \hline 12 & \pm 100 & \frac{1}{100 + 100} \\ \hline 12 & \pm 100 & \frac{1}{100 + 100} \\ \hline 12 & \pm 100 & \frac{1}{100 + 100} \\ \hline 12 & \pm 100 & \frac{1}{100 + 100} \\ \hline 12 & \pm 100 & \frac{1}{100 + 100} \\ \hline 12 & \pm 100 & \frac{1}{100 + 100} \\ \hline 12 & \pm 100 & \frac{1}{100 + 100} \\ \hline 12 & \pm 100 & \frac{1}{100 + 100} \\ \hline 12 & \pm 100 & \frac{1}{100 + 100} \\ \hline 12 & \pm 100 & \frac{1}{100 + 100} \\ \hline 12 & \pm 100 & \frac{1}{100 + 100} \\ \hline 12 & \pm 100 & \frac{1}{100 + 100} \\ \hline 12 & \pm 100 & \frac{1}{100 + 100} \\ \hline 12 & \pm 100 & \frac{1}{100 + 100} \\ \hline 12 & \pm 100 & \frac{1}{100 + 100} \\ \hline 12 & \pm 100 & \frac{1}{100 + 100} \\ \hline 12 & \pm 100 & \frac{1}{100 + 100} \\ \hline 12 & \pm 100 & \frac{1}{100 + 100} \\ \hline 12 & \pm 100 & \frac{1}{100 + 100} \\ \hline 12 & \pm 100 & \frac{1}{100 + 100} \\ \hline 12 & \pm 100 & \frac{1}{100 + 100} \\ \hline 12 & \pm 100 & \frac{1}{100 + 100} \\ \hline 12 & \pm 100 & \frac{1}{100 + 100} \\ $	
$\frac{\frac{115}{12} + \frac{100}{100} - \frac{17W_3 + 48 + 5}{2400}}{\frac{112}{12} + \frac{112}{12} + \frac{175}{100} - \frac{100}{100} + \frac{100}{100} - \frac{100}{100} + \frac{100}{100} - \frac{100}{100} + \frac{100}{100} - \frac{100}{100} + \frac{100}{100} - 10$	
$\frac{\frac{115}{12} + \frac{100}{100} - \frac{17W_3 + 48 + 5}{2400}}{\frac{112}{12} + \frac{112}{12} + \frac{175}{100} - \frac{100}{100} + \frac{100}{100} - \frac{100}{100} + \frac{100}{100} - \frac{100}{100} + \frac{100}{100} - \frac{100}{100} + \frac{100}{100} - 10$	
$\frac{\frac{115}{12} + \frac{100}{10} - \frac{1}{10249.5} - \frac{34.00}{2100}}{\frac{1}{12} + \frac{1}{12} + \frac{1}$	
$\frac{48}{(45.60-50.40)} = \frac{100}{12} + \frac{100}$	
$\begin{array}{c} 48\\ (45.60-50.40) \\ \hline 12\\ \hline 1$	
$\begin{array}{c} 122 \\ \hline 123 \\ \hline$	
$\begin{array}{c} F(A, t) = 1 \\ \hline F(A, t)$	
$\begin{array}{c} BOTTOM \\ VIEW \\ \hline 23.00 \\ \hline \\ 23.00 \\ \hline \\ 23.00 \\ \hline \\ \hline \\ 23.00 \\ \hline \\$	
$\begin{array}{c} \begin{array}{c} PARCE \\ -9 \ QTY + t \\ \hline 23.00 \\ \hline 115 \\ \hline 10 \\ \hline 115 \\ \hline 115 \\ \hline 10 \\ \hline 10$	•
$\frac{23.00}{23.00} \xrightarrow{-1}{-1}$ $\frac{23.00}{23.00} \xrightarrow{-1}{-1}$ $\frac{32.00}{23.00} \xrightarrow{-1}{-1}$ $\frac{32.00}{23.00} \xrightarrow{-1}{-1}$ $\frac{32.00}{23.00} \xrightarrow{-1}{-1}$ $\frac{32.00}{23.00} \xrightarrow{-1}{-1}$ $\frac{32.00}{-1} \xrightarrow{-1}{-1}$ $\frac{32.00}{-1} \xrightarrow{-1}{-1}$ $\frac{32.00}{-1} \xrightarrow{-1}{-1}$ $\frac{32.00}{-1} \xrightarrow{-1}{-1}$ $\frac{32.00}{-1} \xrightarrow{-1}{-1}$	
$ \frac{22.00}{39.00} = 1 $ $ \frac{21.02}{30.0} = 1 $ $ \frac{1}{22} = 1 $ $ \frac{1}{2} = 1 $ $ \frac$	• •
$\begin{array}{c} 22 \\ 300 \\ 3200 \\ \hline \\ \hline \\ \hline \\ 3200 \\ \hline \\ \hline \\ \hline \\ \hline \\ 3200 \\ \hline \\$	
$\begin{array}{c} \frac{23.00}{39.00} \\ \frac{23.00}{23.00} \\ \frac{39.00}{23.00} \\ \frac{1}{23.00} \\ \frac{1}{23.00}$	
$ \begin{array}{c} \frac{43}{12} \\ \frac{43}{2100} \\ \frac{33}{200} \\ \frac{33}{200}$	
	•
29.00 4+ (15.2) (15.2)	
23.00 (20.3) (10.2) ALL DIMENS (MM) 23.00 (20.3)	
	-
23.00 Sangle DUAL	
2.00	
23.00 IS -VOLTPUT COMMON	
20.00 T	التي ²² رومه د منتخب مي روان د منتخب مي روان
POLYTRON DEVICES, INC.	
345-1264 P.O. BOX 398, PATERSON, N.J. 07544 (201) 345-5885 FAX: (201) 345-1264	وتنه جبك وترجي
	264
	264 ••• D•1989

