VLBA Scientific Memo 41

# On S-band Observations with the VLBA

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September 27, 2023

#### Abstract

The VLBA has been operated with filters for S-band on 7 of the 10 telescopes suppressing signals outside of the range about 2.2 - 2.4 GHz. The current study is intended to determine whether these filters should remain in, or be removed from, the system. The results suggest that RFI makes the VLBA S-band system unreliable whether these filters are present or removed from the system.

#### 1 Introduction

VLBA antennas have two sets of filters in the S-band system designed to limit the response of the telescope. The wide filters allow signals from about 2.0 to 2.8 GHz, while the narrow filters limit the observations to about 2.18 through 2.4 GHz. These narrow filters are present in 7 antennas, but are absent from FD, MK, and PT. It has been noticed that these filters select frequencies which include ubiquitous strong satellite broadcasts, prompting the usefulness of the filters to be questioned. Six data sets were obtained on the VLBA to study this question. The first TY040A was observed 15 October 2020 and included a single scan on 3C345 with 4 spectral windows ("SPWs") covering 2.076 - 2.528 GHz with filters present on all antennas except FD, MK, and the VLA (in Y1 mode). The second TS044A was observed on 10 December 2020 at the same frequencies and with filters in all but FD, MK, and PT. A total of 16 sources were observed over 140 minutes. The third and fourth data sets, called TS044B0 and TS044B1, were observed 1 April 2021 using 3 sources in strict rotation and alternating between 2 frequencies covered an overlapping 2.376 to 2.888 GHz. These data had the narrow S-band filters (at least) bypassed. The remaining data sets TS044C0 and TS044C1 were observed on 9 April 2021 with an identical setup but with the filters re-enabled.

Mark Claussen caused these data to be taken and wrote a report on the first two sessions. In general, he found that SPW 4 appeared to be usable with normal Tsys, but only when the narrow filter was not present. He was puzzled by the lack of fringes in SPW 1 on most baselines except those to PT. I have looked at the data from TS044B and TS044C and will describe what I have found in this memo. I will refer to the higher frequency SPWs as SPW 5 through 8 although SPW 5 actually starts in the middle of SPW 3. These SPWs are summarized in Table 1. I should note that these data were taken before the construction of a cell tower near PT, so that station will appear to be better than it is likely to be now.

#### 2 The data

The data were taken on three sources, 3C345, J1648+4104, and J1651+4002 in a strict rotation. Thirty minutes (5 cycles of the sources) was spent on one set of frequencies followed by the second set of frequencies and then repeat. 3C345 is quite strong, J1648+4104 is easily detected, and J1651+4002 is rather weak. The observations with the filters bypassed shows strong fringes in SPWs 2 through 8. As was found by Mark, SPW 1 has almost no detected signal except for baselines between the antennas with no filters (FD, KP, PT).

| SPW | $F_{min}$ | $F_{max}$ | Projects         |
|-----|-----------|-----------|------------------|
|     | GHz       | GHz       |                  |
| 1   | 2.076     | 2.203875  | TS044B0, TS044C0 |
| 2   | 2.204     | 2.331875  | TS044B0, TS044C0 |
| 3   | 2.332     | 2.459875  | TS044B0, TS044C0 |
| 4   | 2.460     | 2.587875  | TS044B0, TS044C0 |
| 5   | 2.376     | 2.503875  | TS044B1, TS044C1 |
| 6   | 2.504     | 2.631875  | TS044B1, TS044C1 |
| 7   | 2.632     | 2.759875  | TS044B1, TS044C1 |
| 8   | 2.760     | 2.887875  | TS044B1, TS044C1 |

Table 1: Spectral window definitions

Whatever was done to "remove" the narrow filters seems to have filtered out frequencies below 2.2 GHz. Curiously, when the filters are in, the fringes are detected clearly down to 2.18 GHz. The filters are quite effective at suppressing any response below 2.18 GHz and above 2.41 GHz.

Figures 1 through 4 are illustrative. Baselines between BR, KP, LA, and MK with PT are shown, illustrating 3 baselines affected by the filters and one (MK-PT) not so affected. Mark reports that there are actually 2 filters, the narrow band 2.2 - 2.4 GHz on 7 stations and a broader one 2.0 - 2.8 on all stations. It is not clear that the broad-band filter was bypassed at FD, MK, or PT. Mark was unsure about the filter at SC, but the data from TS044C suggests that the narrow-band filter is installed there.

## 3 RFI

In VLBI, local sources of RFI normally do not appear in the cross-correlation data either because the source of the RFI is not visible to both antennas or the RFI fringe rate differs from the target source fringe rate by a large amount. It is clear from Figures 1 and 3 that this does not always work. SPW 1 has significant RFI and almost no sensitivity to the astronomical signal. There are 3 general bands of RFI in the cross-correlations from 2.320 - 2.324, 2.328 - 2.336, and 2.342 - 2.345 GHz and RFI affecting KP baselines from about 2.352 - 2.358 GHz.

Unfortunately, calibration of VLBI data requires an accurate measure of the system temperature at each antenna. RFI that affects only one antenna can still ruin this measurement and thus make calibration difficult or impossible. The actual Tsys from these data will be examined in the next section. In the next paragraph, we examine the autocorrelation data from these observations to see what we expect from the single-station RFI.

Figures 5 through 10 illustrate the autocorrelation data from all 9 antennas (HN was absent) with the plots cut off below 0.0 and above 1.6. The plots are generated by VBRFI and are of the mean autocorrelation (in green), the mean rms in purple, and the mean of the rms divided by mean in cyan. The broad features in green are the bandpass shapes of the autocorrelation, whilst the narrow features are RFI. The rms plots reflect instability over time, a characteristic of many types of RFI. VBRFI combines the two polarizations although any difference in the two polarizations increases the rms. Note that there are significant frequency ranges free of obvious RFI, but that RFI is present in almost all SPWs. The RFI has similarities among the antennas, but also very significant differences. The plot scale causes a number of channels to be omitted; the numbers across the upper portions of the plots give the number omitted in each SPW. At the higher frequencies, some sites are relatively quiet (BR, FD, MK, PT) while others (KP, LA, NL, SC) have numerous sources of RFI. These are weaker than the RFI signals around 2.32 - 2.36 GHz which are dominant on most antennas in autocorrelation and even cross correlation.

Autocorrelation data are used in calibration only to make corrections for the digital samplers. The mean autocorrelation in each spectral window should be 1.0 and ACCOR adds gains to the calibration to insure this.

After a bandpass function is found, usually from cross-correlation data, ACSCL makes a further adjustment to insure that the bandpass-corrected autocorrelation averages 1.0. When the autocorrelation data are affected by strong RFI, this second correction will introduce gain errors when the bandpass shape is not ideal (which is the case here).

## 4 Tsys

The Tsys values in the TY table from TS044B0 are summarized in Table 2. Recorded values range from -2060000 to 941000 Dgrees Kelvin and there are only a few SPWs which appear entirely well behaved. SPW 1 is omitted to allow the table to fit on one page and since there is little interferometric sensitivity there. LA, MK, and PT appear more stable, but the last is certainly no longer true. The most unstable of the Tsys are not always correlated with the RFI seen in Figure 5.

Looking at SNPLT of the TY table, from TS044B0 and B1 and only for values from 0 to 110 degrees Kelvin, the following comments may be made. BR was questionable in SPW 3 and SPWs 5-8 seem too low, but the values are pretty stable. FD is poor-bad in SPWs 2L, 3R, 3L, 5R, 5L, and 8L; the rest are maybe okay. KP SPWs 2-4, 6, and 7 are too high; 5 and 8 maybe okay. LA had a bad scan in SPW 4 and was low but relatively stable in SPWs 5-8. MK was amazingly stable. NL was mostly off scale, SPWs 5-8 L perhaps okay. OV had SPW 3, 6R and 8R high; the rest perhaps okay. PT had 8L off scale, the rest (before the cell tower) quite okay. SC SPW 2, 4, 5, and 8 okay; rest bad. It is clear that a usable TY table may be produced by TYSM0 if applied with a firm hand to flag extreme values and values differing from a median window filter by more than a little, replacing the flagged values with values from the filter.

Table 3 lists the statistics from TS044C0 for the two SPWs passed by the narrow filters. Plotting these SPWs along with the same ones from TS044B0, the following comments may be made. FD, MK, and PT lack filters and have quite similar Tsys in both data sets. NL and SC are also rather similar. The B0 Tsys are rather better for BR and LA and are also better in SPW 2 for KP and NL. For KP and NL SPW 3, the C0 Tsys are rather better. HN did not participate in the B0 observations. We should note that the 2.2 - 2.4 GHz filter suppresses about half of SPW 3 which may account for the KP and NL results.

For completeness, Tables 4 and 5 list the Tsys statistics for TS044B1.

## 5 Calibrating the data

One of the first tasks in the standard sequence of VLBA calibration is ACCOR which determines gain amplitudes to insure that the average autocorrelation is 1.0. Figure 11 shows a plot of the spectral average autocorrelation as a function of time for the TS044C0 data set with the input flag table and with an added clip operation to remove obvious RFI (> 5 Jy), and for TS044B0 with default flagging. It is clear that stable ACCOR gains are encouraged by the narrow filters (of the C0 data) and that RFI in the autocorrelation must not be deleted before ACCOR.

This figure brings out an aspect of calibration with ACCOR which is seen in many VLBA data sets. The first 6 - 12 seconds of data in each frequency session should probably be flagged while the system stabilizes.

Examining similar plots for all usable SPWs, we note that the average autocorrelation in TS044C0 is near 1.0 for all antennas in SPW 2 and near 1.6 to 2.0 for most antennas in SPW 3. Stations that are (or were) less plagued by RFI, MK and PT, had the average SPW 3 near 1.0 although PT was noisier in both SPWs. The two polarizations are quite similar. In the TS044B0 data set, the average autocorrelations are mostly relatively stable in each SPW and polarization, although those rough averages vary from 0.6 to 1.1 for some antennas. Again, MK has a very narrow range and SC SPW 2 R is very noisy. Finally, in TS044B1, looking at all 4 SPWS 5 - 8, we again see that the averages are generally relatively stable over time. The averages can be as low as 0.5 or as high as 1.1. PT in SPW 5 is noisy and LA and KP in SPW 8 show significant changes between scans.

4 Page

For comparison purposes, we concentrate on the TS044B0 and TS044C0 data sets. In each, the RFI is flagged at the high end of SPW 2 and lower end of SPW 3, using UVFLG after guidance from FTFLG. A single 3C345 scan was selected in each and VLBAMPCL was run to remove the overall delays. That worked well. Attempting BPASS over all times in each data set produced an over abundance of flagged channels. Using a single half-hour set of scans produced a more usable bandpass correction function.

As described previously, the input Tsys tables are a mess, requiring some editing. TYSMO was run to flag initially all Tsys outside the range 20 - 150 degrees Kelvin, to run a median window filter of width 15 minutes and flagging all points more than 25 degrees Kelvin away from the median, and finally replacing all flagged points with the values of the median filter. This produced some significant flagging of data, but a generally usable representation of Tsys for the rest of the data. The values of Tsys were similar in the two data sets. VLBAAMP was then run to apply ACSCL to change amplitudes due to the effect of bandpass on the autocorrelations and then APCAL to scale the data by the Tsys. Again, the two data sets had similar gain amplitudes. Finally, FRING was run over the data to remove any remaining phase slopes and the data written out by SPLIT.

The resulting time averaged spectra in each baseline looked pretty good except for NL in TS044B0 which was essentially zero with much noise. Each spectrum had both flat phase and amplitude over spectral channel. However, when one examined the average amplitude as a function of time for each baseline, it was clear that the C0 data set had much larger and better behaved fringe amplitudes. The B0 amplitudes are rather scattered in time and often an order of magnitude smaller.

Making images with IMAGR and self-calibrating with CALIB confirmed these differences. The C0 images reached a total flux density of about 3 Jy with a couple of rounds of phase self-cal. Following one round of phase and amplitude self-cal, the final image had a total flux density of 2.83 Jy and an rms noise of 8 mJy/beam. The B0 image never got above density 0.65 Jy. Note that 3C345 should probably have a flux density closer to 6 Jy at this frequency, so even the C0 result is problematical.

The TS044B1 data set was also processed in a similar fashion. The best total flux densities obtained were 1.4 Jy with an rms of 4 mJy/beam.

At Walter Brisken's suggestion, I have run FRING on J1648+4104 in both the B0 and C0 data sets. On the B0 data set, FRING found 692 solutions and failed on 388; on the C0 data set, FRING found 640 good solutions and failed on 260. These are rather high failure rates for a SOLINT of 2 minutes. The mean and rms of the SNRs reported by FRING are summarized in Table 6 and 7. SPW 2 is the only SPW fully sampled by the 2.2 - 2.4 GHz filters. The SNRs tend to be significantly higher with the filters for those antennas that have filters and similar for the antennas (2, 6, 9) without. The numbers for OV are an exception to this rule and the large number of blank cells attests to the significant amount of the data that ends up flagged during the calibration.

### 6 Conclusion

The "obvious" conclusion at the start of this project was to remove the narrow filters to make a much wider bandwidth available to the users. This was thought to be obvious in part because of the significant RFI found in the cross-correlations with those filters and not seen at other frequencies over the rest of S band. However, the failure to calibrate the data in SPWs 2 and 3 usefully when the narrow filters were removed suggests a quite different conclusion. It would appear that those filters, even though they are only on 7 antennas, reduce the RFI depressing and destabilizing the receivers in a significant fashion. The recent construction of a cell tower near PT suggests that adding a filter to PT and perhaps FD would be wise. MK appears to be safe from RFI so far. Even with the use of the narrow filters, the visibility amplitudes after calibration are less than satisfactory. Phase accuracy was not measured in the present study. Therefore, declaring S-band on the VLBA as "shared risk" would, I think, be justified. We certainly cannot guarantee good data for our users.

(BR, HN, KP here) and are quite effective in limiting the response to 2.18 - 2.41 GHz. SPW 1 shows fringes in the region between SPWs 2 and 3. on the baseline with no filters (MIK - PT). Note also considerable RFI in the cross correlations in SPW 1 and Figure 1: TS044C0 average spectrum of 3C345 for 4 baselines as labeled. The filters are in the usual antennas





Figure 2: TS044C1 average spectrum of 3C345 for 4 baselines as labeled. The filters are in the usual antennas (BR, HN, KP here) and are quite effective in limiting the response to frequencies above about 2.41 GHz. baseline. Fringes are seen at all frequencies on the baseline with no filters (MK - PT). Note also the lack of RFI on that

Figure 3: TS044B0 average spectrum of 3C345 for 4 baselines as labeled. The filters have been bypassed. SPW 1 does not show fringes in either polarization for antennas that have the bypassed filters. Note also considerable RFI in the cross correlations in SPW 1 and in the region between SPWs 2 and 3.









Figure 5: TS044B0 average autocorrelation spectrum of 3C345 for 3 antennas in green. The mean rms/mean in cyan and the rms is purple. The filters have been bypassed. Data points outside the range 0 to 1.6 or so have been omitted.



Figure 6: TS044B0 average autocorrelation spectrum of 3C345 for 3 antennas in green. The mean rms/mean in cyan and the rms is purple. The filters have been bypassed. Data points outside the range 0 to 1.6 or so have been omitted.



Figure 7: TS044B0 average autocorrelation spectrum of 3C345 for 3 antennas in green. The mean rms/mean in cyan and the rms is purple. The filters have been bypassed. Data points outside the range 0 to 1.6 or so have been omitted.



Figure 8: TS044B1 average autocorrelation spectrum of 3C345 for 3 antennas in green. The mean rms/mean in cyan and the rms is purple. The filters have been bypassed. Data points outside the range 0 to 1.6 or so have been omitted.



Figure 9: TS044B1 average autocorrelation spectrum of 3C345 for 3 antennas in green. The mean rms/mean in cyan and the rms is purple. The filters have been bypassed. Data points outside the range 0 to 1.6 or so have been omitted.



Figure 10: TS044B1 average autocorrelation spectrum of 3C345 for 3 antennas in green. The mean rms/mean in cyan and the rms is purple. The filters have been bypassed. Data points outside the range 0 to 1.6 or so have been omitted.



Figure 11: TS044 BR autocorrelation averaged over spectral channels as a function of time for SPWs 2 and 3. Top for C0 data with standard flagging, middle for C0 data with a clip applied to the data, and bottom for B0 data with standard flagging. The red color is SPW 2 R polarization, yellow-green is SPW 2 L polarization, blue-green is SPW 3 R polarization, and blue is SPW 3 L polarization.

| Ant | SPW    | S      | Ngood | Max        | Min        | Avg                   | Rms              | Median           | Madrms              | Nblank | Station   |
|-----|--------|--------|-------|------------|------------|-----------------------|------------------|------------------|---------------------|--------|-----------|
| 1   | 2      | 1      | 134   | 149.520    | 21.930     | 40.890                | 17.956           | 37.990           | 10.438              | 0      | BR        |
| 1   | 2      | 2      | 134   | 71.730     | 18.870     | 30.363                | 8.592            | 27.530           | 7.250               | 0      | BR        |
| 1   | 3      | 1      | 134   | 949.510    | -3253.350  | 6.492                 | 334.802          | 14.210           | 61.899              | 0      | BR        |
| 1   | 3      | 2      | 134   | 4388.810   | -4050.770  | 17.982                | 567.254          | 16.260           | 53.299              | 0      | BR        |
| 1   | 4      | 1      | 134   | 2355.500   | -2154.250  | 16.764                | 302.871          | 23.150           | 17.361              | 0      | BR        |
| 1   | 4      | 2      | 134   | 293.010    | -764.730   | 10.832                | 88.453           | 17.200           | 10.690              | 0      | BR        |
| 2   | 2      | 1      | 134   | 178.200    | 31.410     | 73.354                | 31.748           | 62.560           | 23.069              | 0      | FD        |
| 2   | 2      | 2      | 126   | 511.340    | 58.780     | 217.933               | 102.033          | 212.980          | 125.309             | 8      | FD        |
| 2   | 3      | 1      | 134   | 11670.710  | -2725.190  | 291.378               | 1594.979         | 79.780           | 360.168             | 0      | FD        |
| 2   | 3      | 2      | 126   | 3102.470   | -48395.520 | -577.128              | 4485.779         | 45.940           | 299.159             | 8      | FD        |
| 2   | 4      | 1      | 134   | 9033.990   | -1426.790  | 173.560               | 814.452          | 80.730           | 42.269              | 0      | FD        |
| 2   | 4      | 2      | 126   | 3235.810   | -2754.710  | 83.071                | 553.547          | 57.550           | 34.218              | 8      | FD        |
| 4   | 2      | 1      | 134   | 263.090    | 64.610     | 116.520               | 32.404           | 111.920          | 28.244              | 0      | KP        |
| 4   | 2      | 2      | 134   | 293.290    | 66.220     | 139.878               | 44.838           | 125.670          | 36.561              | 0      | KP        |
| 4   | 3      | 1      | 134   | 4565.790   | -17155.600 | 15.204                | 1791.005         | 229.990          | 136.429             | 0      | KP        |
| 4   | 3      | 2      | 134   | 26497.609  | -6725.880  | 662.307               | 2821.418         | 352.570          | 821.197             | 0      | KP        |
| 4   | 4      | 1      | 134   | 1147.380   | 70.110     | 172.508               | 116.649          | 139.130          | 45.545              | 0      | KP        |
| 4   | 4      | 2      | 134   | 9879.580   | 68.750     | 231.289               | 843.336          | 139.650          | 49.296              | 0      | KP        |
| 5   | 2      | 1      | 134   | 1437.070   | 24.540     | 54.830                | 120.703          | 42.830           | 12.350              | 0      | LA        |
| 5   | 2      | 2      | 134   | 578.660    | 30.870     | 52.711                | 47.282           | 45.650           | 10.215              | 0      | LA        |
| 5   | 3      | 1      | 134   | 208.770    | 21.500     | 36.302                | 17.091           | 32.190           | 6.983               | 0      | LA        |
| 5   | 3      | 2      | 134   | 299.060    | 23.490     | 43.594                | 24.324           | 38.780           | 6.449               | 0      | LA        |
| 5   | 4      | 1      | 134   | 1982.530   | -1624.390  | 42.842                | 283.319          | 44.570           | 23.188              | 0      | LA        |
| 5   | 4      | 2      | 134   | 735.340    | -8216.730  | -23.297               | 773.409          | 54.340           | 22.565              | 0      | LA        |
| 6   | 2      | 1      | 134   | 57.060     | 34.920     | 44.378                | 6.139            | 42.950           | 7.650               | 0      | MK        |
| 6   | 2      | 2      | 134   | 54.860     | 35.420     | 44.443                | 5.973            | 43.160           | 7.710               | 0      | MK        |
| 6   | 3      | 1      | 134   | 98.910     | 47.710     | 67.209                | 9.660            | 66.260           | 9.385               | 0      | MK        |
| 6   | 3      | 2      | 134   | 116.130    | 47.000     | 63.680                | 11.599           | 61.450           | 9.044               | 0      | MK        |
| 6   | 4      | 1      | 134   | 46.870     | 31.810     | 38.491                | 4.487            | 37.190           | 5.041               | 0      | MK        |
| 6   | 4      | 2      | 134   | 45.900     | 31.160     | 36.811                | 4.106            | 35.720           | 4.196               | 0      | MK        |
| 7   | 2      | 1      | 129   | 5311.180   | 58.490     | 141.717               | 457.907          | 95.060           | 26.687              | 0      | NL        |
| /   | 2      | 1      | 129   | 206.150    | 53.550     | 81.701                | 21.531           | /7.380           | 14.930              | 0      | INL<br>NI |
| 7   | 3      | 1      | 129   | -315.060   | -2731.430  | -034.798              | 267.782          | -604.790         | 191.522             | 0      | INL       |
| 7   | 3      | 1      | 129   | -02.07U    | -3710.200  | -105.445<br>0.465E+02 | 2 11EE . 0E      | -141.000         | 55.125<br>1.042E±02 | 0      | INL       |
| 7   | 4      | 2      | 129   | 9.412E+03  | -2.200E+00 | -9.403E+03            | 2.115E+03        | 1.439E+03        | 1.043E+03           | 0      | NI        |
| 2   | 4<br>2 | ∠<br>1 | 129   | 24273.971  | -24755.971 | 347.083<br>42.122     | 15 071           | 207.970          | 210.224             | 0      | OV        |
| 8   | 2      | 2      | 134   | 167.050    | 21.100     | 43.123                | 15.071<br>28.049 | 38.230<br>48.510 | 18 132              | 0      | OV        |
| 8   | 2      | 2<br>1 | 134   | 77089 219  | -6256 920  | 135.466               | 6795 648         | 40.010<br>96.350 | 358 967             | 0      | OV        |
| 8   | 3      | 2      | 134   | 151321 609 | -0250.720  | 1244 146              | 13031 237        | 126 960          | 207 742             | 0      | OV        |
| 8   | 4      | 1      | 134   | 65 270     | 23 320     | 33 057                | 6 562            | 32 840           | 5 589               | 0      | OV        |
| 8   | 4      | 2      | 134   | 57 610     | 11 450     | 22 001                | 6 316            | 22.040           | 5 975               | 0      | OV        |
| 9   | 2      | 1      | 134   | 174 980    | 36 200     | 81 281                | 31 670           | 75 950           | 37 421              | 0      | PT        |
| 9   | 2      | 2      | 134   | 157 330    | 29.830     | 81.384                | 25 983           | 78 990           | 23 084              | 0      | PT        |
| 9   | 3      | 1      | 134   | 3278 430   | -3838 720  | 92 725                | 448 116          | 67 270           | 31 431              | 0      | PT        |
| 9   | 3      | 2      | 134   | 209302 609 | -211 520   | 1699.512              | 18002 785        | 92 760           | 39 630              | 0      | PT        |
| 9   | 4      | 1      | 134   | 36.190     | 18.440     | 27.555                | 3.807            | 27.750           | 4,729               | 0      | PT        |
| 9   | 4      | 2      | 134   | 44.360     | 19.370     | 33.588                | 4.733            | 33.840           | 3.736               | 0      | PT        |
| 10  | 2      | 1      | 134   | 363.820    | -11369.390 | -8.745                | 986.713          | 54.990           | 20.919              | 0      | SC        |
| 10  | 2      | 2      | 134   | 76.240     | 27.740     | 40.509                | 6.562            | 39.680           | 5.263               | 0      | SC        |
| 10  | 3      | 1      | 134   | 1.153E+04  | -4.069E+05 | -2.578E+03            | 3.509E+04        | 3.072E+02        | 2.158E+02           | 0      | SC        |
| 10  | 3      | 2      | 134   | 1159.400   | -9455.390  | 138.612               | 845.155          | 169.360          | 78.607              | 0      | SC        |
| 10  | 4      | 1      | 134   | 242.360    | 46.450     | 78.831                | 30.995           | 67.970           | 20.089              | 0      | SC        |
| 10  | 4      | 2      | 134   | 102.550    | 29.560     | 44.000                | 10.559           | 39.960           | 5.575               | 0      | SC        |

Table 2: SNRMS output for TY table from TS044B0

| Ant | SPW | S | Ngood | Max        | Min        | Avg      | Rms      | Median   | Madrms  | Nblank | Station |
|-----|-----|---|-------|------------|------------|----------|----------|----------|---------|--------|---------|
| 1   | 2   | 1 | 134   | 858.250    | -8972.320  | 256.807  | 817.623  | 279.020  | 138.119 | 0      | BR      |
| 1   | 2   | 2 | 134   | 219.340    | 48.850     | 122.502  | 36.738   | 117.020  | 42.521  | 0      | BR      |
| 1   | 3   | 1 | 134   | 3066.900   | -4017.100  | -12.646  | 555.631  | 64.170   | 130.973 | 0      | BR      |
| 1   | 3   | 2 | 134   | 3072.230   | -2171.230  | 51.719   | 447.837  | 55.050   | 137.215 | 0      | BR      |
| 2   | 2   | 1 | 134   | 155.040    | 33.180     | 71.081   | 26.982   | 64.610   | 26.791  | 0      | FD      |
| 2   | 2   | 2 | 134   | 398.580    | 58.110     | 207.063  | 98.281   | 192.030  | 129.905 | 0      | FD      |
| 2   | 3   | 1 | 134   | 63321.398  | -35854.898 | 213.902  | 6346.721 | 50.810   | 234.221 | 0      | FD      |
| 2   | 3   | 2 | 134   | 1599.700   | -19768.400 | -154.944 | 1739.686 | 35.900   | 254.800 | 0      | FD      |
| 3   | 2   | 1 | 134   | 1259.530   | 60.390     | 517.712  | 261.662  | 519.770  | 271.390 | 0      | HN      |
| 3   | 2   | 2 | 134   | 566.830    | 54.780     | 210.274  | 126.373  | 167.730  | 113.552 | 0      | HN      |
| 3   | 3   | 1 | 134   | 3036.070   | 30.430     | 207.468  | 375.899  | 120.960  | 55.212  | 0      | HN      |
| 3   | 3   | 2 | 134   | 1380.710   | -1324.480  | 109.191  | 213.016  | 76.850   | 41.231  | 0      | HN      |
| 4   | 2   | 1 | 134   | 340.360    | 57.360     | 133.176  | 55.835   | 125.450  | 54.337  | 0      | KP      |
| 4   | 2   | 2 | 134   | 18426.920  | -13701.480 | 446.198  | 2555.539 | 263.510  | 156.385 | 0      | KP      |
| 4   | 3   | 1 | 134   | 2945.640   | -1818.850  | 170.965  | 341.562  | 125.680  | 46.480  | 0      | KP      |
| 4   | 3   | 2 | 134   | 1373.620   | -12993.390 | 82.259   | 1147.469 | 146.220  | 56.176  | 0      | KP      |
| 5   | 2   | 1 | 134   | 251.050    | 44.080     | 101.606  | 43.139   | 91.940   | 31.995  | 0      | LA      |
| 5   | 2   | 2 | 134   | 166.080    | 58.180     | 91.181   | 18.706   | 90.550   | 16.175  | 0      | LA      |
| 5   | 3   | 1 | 134   | 246.250    | 58.580     | 134.413  | 47.099   | 135.370  | 62.269  | 0      | LA      |
| 5   | 3   | 2 | 134   | 374.590    | 123.240    | 222.171  | 52.320   | 213.140  | 49.356  | 0      | LA      |
| 6   | 2   | 1 | 134   | 56.730     | 33.990     | 43.455   | 6.058    | 42.220   | 7.502   | 0      | MK      |
| 6   | 2   | 2 | 134   | 78.370     | 34.400     | 43.961   | 6.438    | 42.610   | 7.695   | 0      | MK      |
| 6   | 3   | 1 | 134   | 100.410    | 47.620     | 64.891   | 10.775   | 64.510   | 11.683  | 0      | MK      |
| 6   | 3   | 2 | 134   | 81.880     | 46.460     | 61.541   | 8.522    | 61.730   | 9.963   | 0      | MK      |
| 7   | 2   | 1 | 129   | 578.040    | 48.530     | 123.418  | 82.726   | 91.690   | 38.844  | 0      | NL      |
| 7   | 2   | 2 | 129   | 433.880    | 66.580     | 140.580  | 68.928   | 117.790  | 38.503  | 0      | NL      |
| 7   | 3   | 1 | 129   | 103812.148 | 745.970    | 2426.815 | 9007.223 | 1350.320 | 505.329 | 0      | NL      |
| 7   | 3   | 2 | 129   | 2529.710   | 172.720    | 552.088  | 411.870  | 408.540  | 155.910 | 0      | NL      |
| 8   | 2   | 1 | 134   | 415.760    | 38.440     | 166.740  | 87.438   | 140.150  | 59.378  | 0      | OV      |
| 8   | 2   | 2 | 134   | 526.390    | 79.790     | 219.488  | 101.978  | 200.050  | 79.364  | 0      | OV      |
| 8   | 3   | 1 | 134   | 319.700    | 36.180     | 107.028  | 55.039   | 92.420   | 41.201  | 0      | OV      |
| 8   | 3   | 2 | 134   | 2280.170   | 37.740     | 145.043  | 224.392  | 86.400   | 46.643  | 0      | OV      |
| 9   | 2   | 1 | 134   | 210.750    | 33.830     | 81.703   | 34.149   | 76.880   | 41.394  | 0      | PT      |
| 9   | 2   | 2 | 134   | 174.770    | 30.560     | 78.762   | 26.222   | 76.890   | 21.616  | 0      | PT      |
| 9   | 3   | 1 | 134   | 1737.570   | 34.380     | 120.139  | 205.629  | 65.550   | 31.313  | 0      | PT      |
| 9   | 3   | 2 | 134   | 3304.940   | -2448.060  | 85.441   | 372.008  | 81.430   | 33.522  | 0      | PT      |
| 10  | 2   | 1 | 134   | 54.640     | 34.170     | 42.974   | 5.148    | 42.090   | 5.604   | 0      | SC      |
| 10  | 2   | 2 | 134   | 49.350     | 31.010     | 37.238   | 4.078    | 37.340   | 4.685   | 0      | SC      |
| 10  | 3   | 1 | 134   | 631.850    | 120.140    | 208.691  | 72.845   | 190.030  | 39.496  | 0      | SC      |
| 10  | 3   | 2 | 134   | 239.270    | 77.510     | 122.504  | 29.861   | 118.560  | 24.329  | 0      | SC      |

Table 3: SNRMS output for TY table from TS044C0  $\,$ 

| Ant | SPW | S | Ngood | Max        | Min        | Avg      | Rms       | Median  | Madrms  | Nblank | Station |
|-----|-----|---|-------|------------|------------|----------|-----------|---------|---------|--------|---------|
| 1   | 1   | 1 | 133   | 486.390    | -103.830   | 0.117    | 46.369    | -2.870  | 12.306  | 0      | BR      |
| 1   | 1   | 2 | 133   | 610.600    | -104.680   | 3.400    | 55.387    | 2.090   | 9.652   | 0      | BR      |
| 1   | 2   | 1 | 133   | 3767.160   | -339.910   | 59.209   | 331.418   | 23.270  | 12.587  | 0      | BR      |
| 1   | 2   | 2 | 133   | 79.230     | 26.420     | 36.233   | 5.650     | 36.270  | 2.891   | 0      | BR      |
| 1   | 3   | 1 | 133   | 991.730    | -938.860   | 46.752   | 175.107   | 19.090  | 16.590  | 0      | BR      |
| 1   | 3   | 2 | 133   | 37.780     | 18.930     | 21.324   | 2.598     | 20.840  | 1.038   | 0      | BR      |
| 1   | 4   | 1 | 133   | 432.940    | -390.860   | 9.410    | 74.318    | 9.720   | 29.860  | 0      | BR      |
| 1   | 4   | 2 | 133   | 1690.350   | 30.620     | 84.000   | 141.653   | 66.670  | 16.323  | 0      | BR      |
| 2   | 1   | 1 | 133   | 5980.480   | -10983.970 | -164.590 | 1440.362  | 86.580  | 327.788 | 0      | FD      |
| 2   | 1   | 2 | 133   | 1527.510   | -4977.400  | -97.150  | 818.480   | 48.920  | 250.930 | 0      | FD      |
| 2   | 2   | 1 | 133   | 164.950    | -36495.988 | -225.798 | 3157.176  | 47.620  | 12.899  | 0      | FD      |
| 2   | 2   | 2 | 133   | 425.710    | 14.150     | 38.901   | 39.506    | 29.980  | 10.719  | 0      | FD      |
| 2   | 3   | 1 | 133   | 172.070    | 22.400     | 46.781   | 19.138    | 42.530  | 7.457   | 0      | FD      |
| 2   | 3   | 2 | 133   | 36.210     | 14.270     | 21.946   | 3.643     | 21.380  | 3.158   | 0      | FD      |
| 2   | 4   | 1 | 133   | 425.730    | -387.570   | 94.596   | 80.573    | 85.330  | 28.229  | 0      | FD      |
| 2   | 4   | 2 | 133   | 3303.320   | -3933.270  | 79.580   | 683.965   | 76.840  | 179.825 | 0      | FD      |
| 4   | 1   | 1 | 133   | 460.160    | 22.890     | 47.039   | 40.870    | 37.660  | 9.948   | 0      | KP      |
| 4   | 1   | 2 | 133   | 472.200    | -674.130   | 54.074   | 89.745    | 44.990  | 14.455  | 0      | KP      |
| 4   | 2   | 1 | 133   | 5246.000   | -1821.400  | 163.404  | 823.218   | 79.030  | 124.761 | 0      | KP      |
| 4   | 2   | 2 | 133   | 1233.870   | -6555.090  | -37.150  | 695.923   | 56.330  | 224.036 | 0      | KP      |
| 4   | 3   | 1 | 133   | 22131.510  | -5375.670  | -32.697  | 2062.787  | -69.330 | 68.096  | 0      | KP      |
| 4   | 3   | 2 | 133   | 320769.000 | -7770.350  | 2296.783 | 27742.697 | -73.160 | 48.481  | 0      | KP      |
| 4   | 4   | 1 | 133   | 3777.170   | 20.660     | 58.035   | 324.626   | 24.520  | 2.936   | 0      | KP      |
| 4   | 4   | 2 | 133   | 538.900    | -576.460   | 27.812   | 85.464    | 26.280  | 3.336   | 0      | KP      |
| 5   | 1   | 1 | 133   | 338.670    | 13.070     | 38.891   | 41.903    | 29.630  | 12.839  | 0      | LA      |
| 5   | 1   | 2 | 133   | 101.640    | -100.580   | 33.567   | 17.777    | 30.590  | 8.792   | 0      | LA      |
| 5   | 2   | 1 | 133   | 38.290     | 7.630      | 14.814   | 7.083     | 12.130  | 3.959   | 0      | LA      |
| 5   | 2   | 2 | 133   | 55.820     | 10.080     | 18.136   | 7.467     | 16.780  | 6.049   | 0      | LA      |
| 5   | 3   | 1 | 133   | 25.680     | 7.170      | 9.077    | 1.878     | 8.750   | 1.379   | 0      | LA      |
| 5   | 3   | 2 | 133   | 32.760     | 8.900      | 11.851   | 2.466     | 11.730  | 2.254   | 0      | LA      |
| 5   | 4   | 1 | 133   | 61.450     | 9.480      | 18.865   | 11.363    | 14.560  | 5.041   | 0      | LA      |
| 5   | 4   | 2 | 133   | 205.700    | 11.500     | 31.362   | 24.284    | 26.270  | 17.406  | 0      | LA      |
| 6   | 1   | 1 | 133   | 106.720    | 55.830     | 61.718   | 7.424     | 59.520  | 3.425   | 0      | MK      |
| 6   | 1   | 2 | 133   | 70.330     | 41.530     | 46.813   | 3.984     | 45.160  | 2.713   | 0      | MK      |
| 6   | 2   | 1 | 133   | 41.160     | 28.770     | 33.076   | 3.359     | 32.310  | 4.107   | 0      | MK      |
| 6   | 2   | 2 | 133   | 43.130     | 30.920     | 35.173   | 3.259     | 34.580  | 4.151   | 0      | MK      |
| 6   | 3   | 1 | 133   | 48.090     | 32.600     | 37.725   | 4.078     | 36.640  | 4.077   | 0      | MK      |
| 6   | 3   | 2 | 133   | 45.510     | 30.930     | 36.214   | 3.869     | 35.380  | 4.359   | 0      | MK      |
| 6   | 4   | 1 | 133   | 47.190     | 33.720     | 38.280   | 3.772     | 37.050  | 3.914   | 0      | MK      |
| 6   | 4   | 2 | 133   | 47.840     | 34.310     | 39.390   | 3.825     | 38.190  | 4.107   | 0      | MK      |
| 7   | 1   | 1 | 133   | 2871.330   | 194.420    | 425.436  | 362.693   | 324.830 | 71.565  | 0      | NL      |
| 7   | 1   | 2 | 133   | 270.800    | 27.710     | 62.329   | 27.534    | 56.170  | 11.624  | 0      | NL      |
| 7   | 2   | 1 | 133   | 334.280    | 115.230    | 175.241  | 40.760    | 170.170 | 42.684  | 0      | NL      |
| 7   | 2   | 2 | 133   | 156.020    | 25.710     | 42.291   | 16.847    | 38.380  | 8.406   | 0      | NL      |
| 7   | 3   | 1 | 133   | 142.840    | 82.720     | 99.039   | 11.769    | 95.900  | 9.251   | 0      | NL      |
| 7   | 3   | 2 | 133   | 43.370     | 21.820     | 25.830   | 2.853     | 25.330  | 2.224   | 0      | NL      |
| 7   | 4   | 1 | 133   | 13963.790  | -2040.290  | 465.708  | 1412.190  | 255.310 | 99.646  | 0      | NL      |
| 7   | 4   | 2 | 133   | 194.140    | -1670.810  | 12.871   | 147.523   | 22.610  | 3.025   | 0      | NL      |

Table 4: SNRMS output for TY table from TS044B1

| Ant | SPW | S | Ngood | Max       | Min        | Avg      | Rms      | Median   | Madrms  | Nblank | Station |
|-----|-----|---|-------|-----------|------------|----------|----------|----------|---------|--------|---------|
| 8   | 1   | 1 | 133   | 405.390   | -356.610   | 111.281  | 52.678   | 107.960  | 5.323   | 0      | OV      |
| 8   | 1   | 2 | 133   | 131.980   | -462.000   | 45.360   | 45.448   | 46.990   | 6.390   | 0      | OV      |
| 8   | 2   | 1 | 133   | 486.520   | -216.560   | 128.320  | 55.566   | 125.970  | 25.782  | 0      | OV      |
| 8   | 2   | 2 | 133   | 43.670    | 19.080     | 29.529   | 4.580    | 29.140   | 3.899   | 0      | OV      |
| 8   | 3   | 1 | 133   | 1035.300  | -172.110   | 115.839  | 114.352  | 106.640  | 31.238  | 0      | OV      |
| 8   | 3   | 2 | 133   | 32.210    | 17.750     | 21.841   | 2.484    | 21.510   | 1.883   | 0      | OV      |
| 8   | 4   | 1 | 133   | 1358.400  | -244.790   | 1176.833 | 218.202  | 1222.240 | 72.410  | 0      | OV      |
| 8   | 4   | 2 | 133   | 124.890   | 54.650     | 86.811   | 8.252    | 86.200   | 7.057   | 0      | OV      |
| 9   | 1   | 1 | 133   | 3281.230  | -4416.040  | 17.362   | 594.042  | 48.900   | 18.903  | 0      | PT      |
| 9   | 1   | 2 | 133   | 6780.890  | -139.390   | 97.535   | 582.616  | 41.090   | 9.415   | 0      | PT      |
| 9   | 2   | 1 | 133   | 25.370    | 19.910     | 21.411   | 1.122    | 21.400   | 1.468   | 0      | PT      |
| 9   | 2   | 2 | 133   | 44.360    | 34.870     | 37.034   | 1.664    | 36.960   | 2.120   | 0      | PT      |
| 9   | 3   | 1 | 133   | 33.890    | 24.800     | 26.281   | 1.194    | 26.090   | 1.201   | 0      | PT      |
| 9   | 3   | 2 | 133   | 43.820    | 31.380     | 32.594   | 1.284    | 32.460   | 1.127   | 0      | PT      |
| 9   | 4   | 1 | 133   | 92.260    | 63.660     | 86.288   | 3.530    | 86.610   | 2.891   | 0      | PT      |
| 9   | 4   | 2 | 133   | 156.790   | 105.450    | 147.410  | 5.315    | 147.380  | 4.300   | 0      | PT      |
| 10  | 1   | 1 | 133   | 165.750   | 48.150     | 64.551   | 11.524   | 60.450   | 3.766   | 0      | SC      |
| 10  | 1   | 2 | 133   | 127.570   | 47.300     | 56.888   | 8.000    | 55.110   | 2.639   | 0      | SC      |
| 10  | 2   | 1 | 133   | 9465.670  | -4807.610  | 231.671  | 1197.899 | 135.640  | 65.783  | 0      | SC      |
| 10  | 2   | 2 | 133   | 396.880   | 38.950     | 104.166  | 55.061   | 97.090   | 45.605  | 0      | SC      |
| 10  | 3   | 1 | 133   | 52194.039 | -37766.551 | 634.646  | 6072.357 | 297.210  | 577.250 | 0      | SC      |
| 10  | 3   | 2 | 133   | 12425.740 | -9572.640  | 65.026   | 2209.293 | 164.450  | 701.018 | 0      | SC      |
| 10  | 4   | 1 | 133   | 47.040    | 37.360     | 41.582   | 1.489    | 41.230   | 1.705   | 0      | SC      |
| 10  | 4   | 2 | 133   | 40.010    | 31.540     | 35.268   | 1.348    | 35.160   | 1.972   | 0      | SC      |

Table 5: SNRMS output for TY table from TS044B1

|     |     |   |          | TS044B0 |        | TS044C0  |         |        |
|-----|-----|---|----------|---------|--------|----------|---------|--------|
| Ant | SPW | S | Mean SNR | rms SNR | Number | Mean SNR | rms SNR | Number |
| 1   | 1   | 1 |          |         |        | 2.7      | 2.0     | 15     |
| 1   | 1   | 2 |          |         |        | 4.0      | 2.0     | 15     |
| 1   | 2   | 1 | 41.6     | 5.7     | 14     | 106.4    | 74.6    | 7      |
| 1   | 2   | 2 | 63.5     | 10.6    | 15     | 113.2    | 39.7    | 15     |
| 1   | 3   | 1 | 29.3     | 6.0     | 13     | 35.9     | 26.5    | 14     |
| 1   | 3   | 2 | 50.2     | 7.1     | 15     | 51.9     | 17.7    | 15     |
| 1   | 4   | 1 | 30.8     | 4.1     | 14     |          |         |        |
| 1   | 4   | 2 | 55.7     | 4.7     | 15     |          |         |        |
| 2   | 1   | 1 |          |         |        | 47.5     | 11.7    | 13     |
| 2   | 1   | 2 |          |         |        | 45.8     | 21.6    | 7      |
| 2   | 2   | 1 |          |         |        | 164.0    | 31.4    | 14     |
| 2   | 2   | 2 | 138.5    | 37.0    | 10     | 128.8    | 41.3    | 5      |
| 2   | 3   | 1 |          |         |        | 105.3    | 15.3    | 14     |
| 2   | 3   | 2 | 90.7     | 13.3    | 15     | 81.9     | 20.7    | 9      |
| 2   | 4   | 1 |          |         |        |          |         |        |
| 2   | 4   | 2 | 111.9    | 11.2    | 15     |          |         |        |
| 3   | 1   | 1 |          |         |        | 2.6      | 1.1     | 13     |
| 3   | 1   | 2 |          |         |        | 3.9      | 0.8     | 15     |
| 3   | 2   | 1 |          |         |        | 86.1     | 29.1    | 10     |
| 3   | 2   | 2 |          |         |        | 116.7    | 12.7    | 13     |
| 3   | 3   | 1 |          |         |        | 31.9     | 11.6    | 15     |
| 3   | 3   | 2 |          |         |        | 49.0     | 9.3     | 14     |
| 4   | 1   | 1 |          |         |        | 3.7      | 0.5     | 15     |
| 4   | 1   | 2 |          |         |        | 3.4      | 1.2     | 15     |
| 4   | 2   | 1 | 21.9     | 2.0     | 15     | 115.6    | 20.2    | 15     |
| 4   | 2   | 2 | 62.9     | 6.7     | 15     | 102.9    | 23.3    | 10     |
| 4   | 3   | 1 | 16.2     | 3.9     | 6      | 43.0     | 8.4     | 15     |
| 4   | 3   | 2 |          |         |        | 36.3     | 10.7    | 15     |
| 4   | 4   | 1 | 17.6     | 2.1     | 10     |          |         |        |
| 4   | 4   | 2 | 50.7     | 3.2     | 15     |          |         |        |
| 5   | 1   | 1 |          |         |        | 4.1      | 1.5     | 15     |
| 5   | 1   | 2 |          |         |        | 3.9      | 1.1     | 15     |
| 5   | 2   | 1 | 26.4     | 3.7     | 14     | 135.3    | 32.4    | 14     |
| 5   | 2   | 2 | 28.4     | 3.7     | 15     | 130.0    | 36.0    | 15     |
| 5   | 3   | 1 | 23.8     | 3.0     | 14     | 74.5     | 21.5    | 14     |
| 5   | 3   | 2 | 24.3     | 2.4     | 15     | 59.0     | 13.6    | 12     |
| 5   | 4   | 1 | 22.6     | 1.1     | 3      |          |         |        |
| 5   | 4   | 2 | 25.0     | 3.1     | 9      |          |         |        |

Table 6: FRING SNR ratios for lower frequency SPWs

|     |     |   |          | TS044B0 |        |          | TS044C0 |        |
|-----|-----|---|----------|---------|--------|----------|---------|--------|
| Ant | SPW | S | Mean SNR | rms SNR | Number | Mean SNR | rms SNR | Number |
| 6   | 1   | 1 | 28.3     | 2.9     | 15     |          |         |        |
| 6   | 1   | 2 |          |         |        | 27.9     | 5.5     | 15     |
| 6   | 2   | 1 | 72.6     | 5.0     | 15     | 103.1    | 30.6    | 15     |
| 6   | 2   | 2 | 84.2     | 7.8     | 15     | 63.5     | 6.6     | 15     |
| 6   | 3   | 1 | 49.6     | 4.1     | 15     | 69.3     | 21.1    | 15     |
| 6   | 3   | 2 | 65.9     | 3.2     | 15     | 48.8     | 6.4     | 15     |
| 6   | 4   | 1 | 49.0     | 4.2     | 15     |          |         |        |
| 6   | 4   | 2 | 71.4     | 2.9     | 15     |          |         |        |
| 7   | 1   | 1 |          |         |        | 2.8      | 0.8     | 15     |
| 7   | 1   | 2 |          |         |        | 1.8      | 0.5     | 14     |
| 7   | 2   | 1 |          |         |        | 87.8     | 23.0    | 15     |
| 7   | 2   | 2 |          |         |        | 59.7     | 16.9    | 15     |
| 8   | 1   | 1 |          |         |        | 2.5      | 0.6     | 15     |
| 8   | 1   | 2 |          |         |        | 3.7      | 0.7     | 15     |
| 8   | 2   | 1 | 98.9     | 7.0     | 15     | 85.9     | 22.4    | 15     |
| 8   | 2   | 2 | 72.4     | 8.0     | 15     | 107.2    | 19.9    | 15     |
| 8   | 3   | 1 | 71.0     | 11.4    | 15     | 40.4     | 10.0    | 15     |
| 8   | 3   | 2 | 55.4     | 6.7     | 13     | 52.3     | 9.3     | 15     |
| 8   | 4   | 1 | 83.0     | 7.2     | 15     |          |         |        |
| 8   | 4   | 2 | 67.6     | 5.3     | 15     |          |         |        |
| 9   | 1   | 1 | 86.5     | 21.1    | 10     | 37.0     | 7.3     | 2      |
| 9   | 1   | 2 |          |         |        | 54.5     | 10.5    | 7      |
| 9   | 2   | 1 | 201.0    | 18.3    | 15     | 104.4    | 26.3    | 2      |
| 9   | 2   | 2 |          |         |        | 135.9    | 20.5    | 8      |
| 9   | 3   | 1 | 131.0    | 13.4    | 15     | 69.3     | 15.9    | 2      |
| 9   | 3   | 2 |          |         |        | 86.3     | 15.0    | 7      |
| 9   | 4   | 1 | 142.3    | 16.6    | 15     |          |         |        |
| 9   | 4   | 2 |          |         |        |          |         |        |
| 10  | 1   | 1 |          |         |        | 3.5      | 0.5     | 15     |
| 10  | 1   | 2 |          |         |        | 2.7      | 0.5     | 10     |
| 10  | 2   | 1 | 41.3     | 12.6    | 15     | 113.0    | 20.3    | 15     |
| 10  | 2   | 2 | 67.9     | 8.2     | 15     | 83.0     | 10.7    | 15     |
| 10  | 3   | 1 | 22.4     | 8.2     | 8      | 31.5     | 7.3     | 14     |
| 10  | 3   | 2 | 30.6     | 6.1     | 14     | 25.8     | 3.6     | 15     |
| 10  | 4   | 1 | 25.7     | 6.2     | 15     |          |         |        |
| 10  | 4   | 2 | 43.9     | 2.9     | 15     |          |         |        |

Table 7: FRING SNR ratios for lower frequency SPWs