

NATIONAL RADIO ASTRONOMY OBSERVATORY  
Socorro, New Mexico

VLBA TECHNICAL REPORT NO. 29

FRONT-END F104 (2.3 Ghz) CARD CAGE CIRCUITRY

Addendum to VLBA TECHNICAL REPORT NO. 10

Gerry Petencin and David Weber  
January 15, 1995



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## 1.0 INTRODUCTION

Technical Report No. 29 is an addendum to VLBA TECHNICAL REPORT NO. 10 (F104, 2.3 GHz, 13 cm). This report augments the RF, thermal and physical descriptions contained in TECHNICAL REPORT NO. 10 (TR 10) by describing the card cage circuitry and its interfaces with the RF amplifiers, vacuum and temperature sensors, vacuum valve, refrigerator, heater calibration, and Monitor and Control system. The temperature and pressure transducer characteristics are also described. Since the Front-End's RF and thermal characteristics are described in TR 10, these topics are not included in this addendum.

An important graphic feature of the Theory of Operation (Section 2.0) is a detailed Front-End block diagram that shows all Front-End interconnect and interface circuitry. Reduced scale copies of the schematic and assembly drawings for the four card types and the associated BOMs are included. The card descriptions include alignment procedures.

Section 3 contains a list of relevant NRAO Technical Reports and memoranda.

Section 4 contains data sheets for special-purpose components used in the card cage circuitry.

Since TR 10 contains many assembly and BOM drawings and the card cage wire list, they are not included in this addendum. These drawings are referenced in the circuitry descriptions as required.

## 2.0 THEORY OF OPERATION

### 2.1 Front-End Block Diagram

Drawing C53204K002, following this text, is the F104 block diagram and provides a functional overview of the F104 circuitry. It shows the card cage, dewar, RF Plate, pressure and temperature transducers, vacuum valve, refrigerator control, and Monitor and Control interface circuitry. The four card types are shown in block form; the card's schematic, assembly and BOM drawings are included for reference in the circuit card descriptions.

I/O connector pins and signals are tabulated in section 2.3. Drawing B53203W002, TR 10 Appendix page II-28 is the card cage assembly drawing and shows the card cage, I/O connectors, card connectors, power resistors, and ground lug. Drawing B53203A004, TR 10 Appendix page II-6, is a similar drawing and shows cable routing and a connector table. J17, the 9-pin "D" connector, provides power and signal connections to the RF Plate mounted on the side of the card cage.



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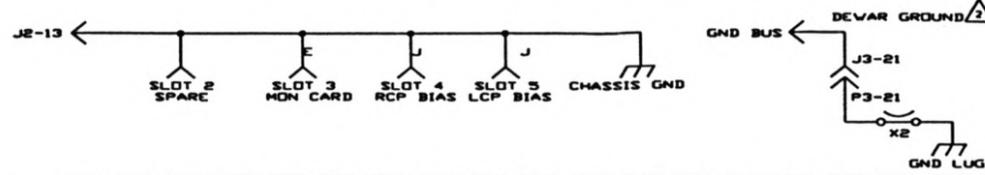
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QUALITY GROUND STRING

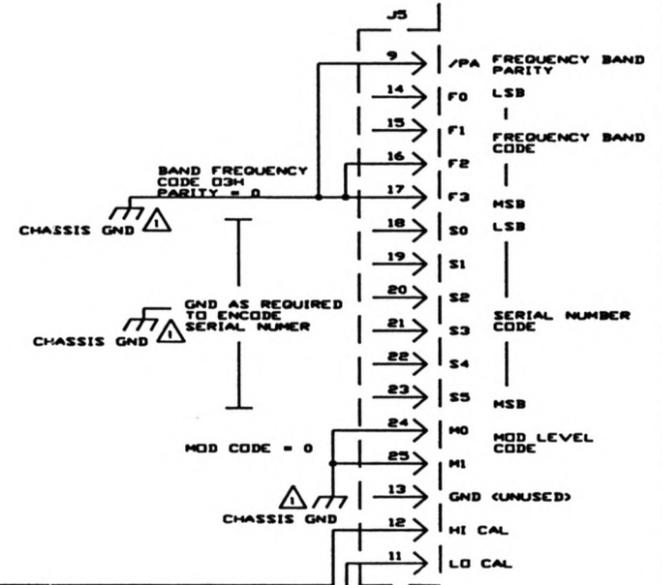
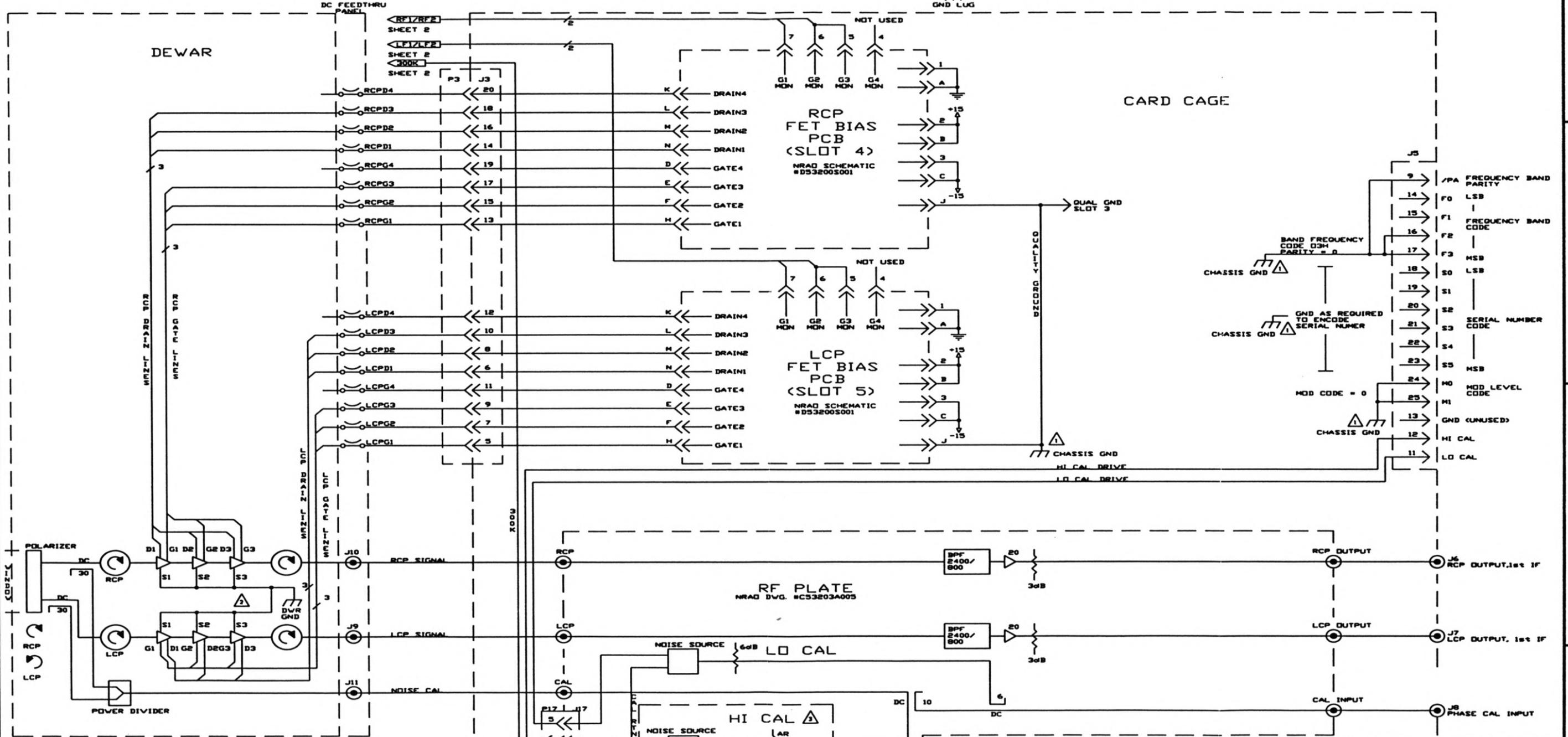
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NOTES:  
 ▲ FOR GROUND LUG LOCATIONS SEE 1.5 GHZ FRONT END CARD CAGE WIRING DIAGRAM (NRAD DVG. #53203V002)  
 ▲ DEWAR GROUND IS THROUGH METAL STRUCTURES  
 ▲ HI CAL CIRCUIT IS OPTIONAL. A FEW VLBA F104'S HAVE HI CAL CIRCUITS



DEWAR

CARD CAGE



ORCAD : 53204K2A

PROPERTY OF NRAD

B53203V002	WIRING DIAG
A53203V001	WIRE LIST
D53203A004	ASSEMBLY
NEXT ASSEMBLY	DVG TYPE

UNLESS OTHERWISE SPECIFIED DIMENSIONS ARE IN INCHES  
 TOLERANCES: ANGLES ±  
 3 PLACE DECIMALS (.XXX) ±  
 2 PLACE DECIMALS (.XX) ±  
 1 PLACE DECIMALS (.X) ±

MATERIAL:  
 FINISH:

F104  
 2.3 GHZ FRONT END

F104  
 2.3 GHZ FRONT END  
 CARD CAGE  
 BLOCK DIAGRAM

SHEET NUMBER 1 OF 2  
 DRAWING NUMBER C53204K002  
 REV. - SCALE -

NATIONAL RADIO ASTRONOMY OBSERVATORY  
 SOCORRO, NEW MEXICO 87801

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APPROVED BY	DATE



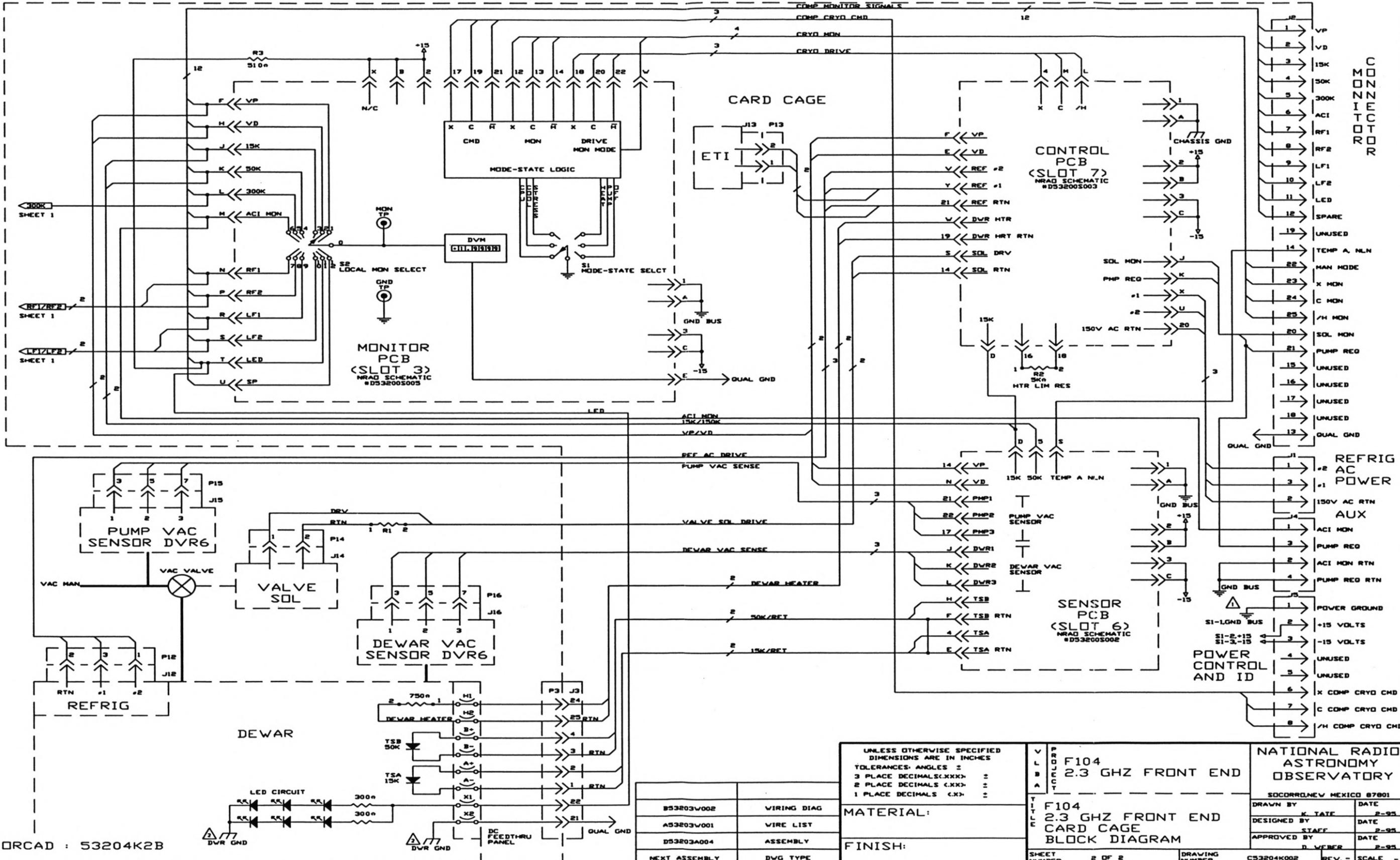
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REV.	DATE	DRAWN BY	APPROV'D BY	DESCRIPTION



ORCAD : 53204K2B

PROPERTY OF NRAO

B53203W002	WIRING DIAG
A53203W001	WIRE LIST
D53203A004	ASSEMBLY
NEXT ASSEMBLY	DWG TYPE

UNLESS OTHERWISE SPECIFIED  
DIMENSIONS ARE IN INCHES  
TOLERANCES: ANGLES ±  
3 PLACE DECIMALS (.XXX) ±  
2 PLACE DECIMALS (.XX) ±  
1 PLACE DECIMALS (.X) ±

MATERIAL:  
FINISH:

V L P  
L B P  
B E L  
A T  
T  
L  
E

F104  
2.3 GHZ FRONT END

F104  
2.3 GHZ FRONT END  
CARD CAGE  
BLOCK DIAGRAM

SHEET NUMBER 2 OF 2  
DRAWING NUMBER C53204K002  
REV. - SCALE -

NATIONAL RADIO  
ASTRONOMY  
OBSERVATORY

SOCORRO, NEW MEXICO 87801

DRAWN BY	K. TATE	DATE	2-95
DESIGNED BY	STAFF	DATE	2-95
APPROVED BY	D. WEBER	DATE	2-95



## 2.2 Front-End Interface Signals and Characteristics

### Card Cage Panel Connectors

#### J2-Monitor

Pin	Name	Function/Type
1	VP	PUMP VAC Mon/analog
2	VD	DEWAR VAC Mon/analog
3	15K	15K TEMP Mon/analog
4	50K	50K TEMP Mon/analog
5	300K	300K TEMP Mon/analog
6	AC1	AC CURRENT Mon/analog
7	RF1	RCP STAGE 1 Mon/analog
8	RF2	OTHER STAGES Mon/analog
9	LF1	LCP STAGE 1 Mon/analog
10	LF2	OTHER STAGES Mon/analog
11	LED	LED VOLTAGE Mon/analog
12	Not Used	
13	QGND	QUALITY GND/analog
14	SENS	TEMP SENSE A Mon/analog
15	Not Used	
16	Not Used	
17	Not Used	
18	Not Used	
19	Not Used	
20	S	SOLENOID MON/TTL
21	P	PUMP REQUEST MON/TTL
22	M	MANUAL MON/TTL
23	X	CONTROL MON/TTL
24	C	MODE MON/TTL
25	H	MONITOR MON/TTL

#### J5-PWR, Control & ID

Pin	Name	Function/Type
1	GND	POWER GROUND
2	+15	+15V/FE Power
3	-15	-15V/FE Power
4	Not Used	
5	Not Used	
6	X	CONTROL BIT/TTL
7	C	CONTROL BIT/TTL
8	H	CONTROL BIT/TTL
9	PA	FE PARITY/TTL
10	Not Used	
11	CAL	+28V DRIVE/CMD
12	HI CAL	+28V DRIVE/CMD
13	GND	Not Used*
14	F0	LSB /TTL
15	F1	FREQUENCY /TTL
16	F2	ID /TTL
17	F3	MSB /TTL
18	S0	LSB /TTL
19	S1	LSB /TTL
20	S2	SERIAL /TTL
21	S3	NUMBER /TTL
22	S4	ID /TTL
23	S5	MSB /TTL
24	M0	MODIFICATION/TTL
25	M1	MSB /TTL

#### J3-Dewar Bias, LED & Temp

Pin	Name	Function/Type
1	TSA Ret (15K)	Ret/analog
2	TSA Sig (15K)	Sig/analog
3	TSB Ret (50K)	Ret/analog
4	TSB Sig (50K)	Sig/analog
5	LCP GATE 1	BIAS/analog
6	LCP DRAIN 1	BIAS/analog
7	LCP GATE 2	BIAS/analog
8	LCP DRAIN 2	BIAS/analog
9	LCP GATE 4	BIAS/analog
10	LCP DRAIN 3	BIAS/analog
11	LCP GATE 4	BIAS/analog
12	LCP DRAIN 4	BIAS/analog
13	RCP GATE 1	BIAS/analog
14	RCP DRAIN 1	BIAS/analog
15	RCP GATE 2	BIAS/analog
16	RCP DRAIN 2	BIAS/analog
17	RCP GATE 3	BIAS/analog
18	RCP DRAIN 3	BIAS/analog
19	RCP GATE 4	BIAS/analog
20	RCP DRAIN 4	BIAS/analog
21	DEWAR GND	Not Used*
22	LED	LED DRIVE/analog
23	Not Used	
24	DEWAR HEATER/150 VAC	
25	DEWAR HEATER RET/AC	

#### J4-Auxiliary

Pin	Name	Function/Type
1	AC+	CURRENT MON/analog
2	AC-	CURRENT MON/analog
3	P	PUMP REQUEST CMD/TTL
4	GND	GROUND PUMP REQ RET/GND
5 through 9		Not Used

#### J1-AC Power Interface

Pin	Name	Function/Type
1	φ1	SHIFTED PHASE/150 VAC
2	φ2	LINE PHASE/150 VAC
3	RETURN	

#### J17-RF Plate

Pin	Name	Function/Type
1	Ground	
2	+15 volts	
3	-15 volts	
4	Ground	
5	Low Cal Control	
6	High Cal Control	
7	Cal Return	
8	300 °K Temp Mon	
9	Not Used	

**Dewar DC Feedthrough** - See Figure 4 in Section 2.10.

**RF I/O Connectors:** J6-RCP RF Out; J7-LCP RF Out; J8-Phase Cal Input

**AC Power Cables:** P12 Refrigerator AC Power J12; P13 AC power to Elapsed Time Indicator J13; P14 AC drive to Solenoid J14. See Wire List A53203W001, Sheet 8, TR 10 Appendix page II-22 and 2.3 GHz FE Block Diagram C53204K002 for connections.

**Vacuum Sensor Cables:** P15 Pump Vacuum Sense to Pump DV-R6 J15; P16 Dewar Vacuum Sense to Dewar DV-R6 J16. See Wire List A53203W001, Sheet 7, TR 10 Appendix page II-21 and 2.3 GHz FE Block Diagram C53204K002 for connections.

\* Although VLBA Front-End manuals typically designate this pin as Ground, it is not wired in F104; see Wire List Sheet 12, TR 10 Appendix page II-26.

### 2.3 Front-End Modes and Cryogenics Control States

The F104 Front-End operates in two Modes: Local (manual) and CPU (remote). The mode is manually selected by S1, the Heat, Pump, Off, Load, Cool, CPU manual selector switch on the card cage Control-Monitor panel. When the switch pointer is in the CPU position, the mode is computer-remote; if the pointer is in any other position, the mode is Local-manual. When the switch is in the Local mode, the control computer cannot override the mode switch setting.

In both modes, there are five Cryogenic States selected by either the manual selector switch in the Local mode or by the control computer in the CPU mode. These five states are: Heat, Pump, Off, Load, and Cool. The table below briefly describes the operations performed by the cryogenic components as a function of the Cryogenic State. The three control discrettes X, C, and  $\bar{H}$  (described in the Monitor Card description) determine the operation of the refrigerator, vacuum valve and pump request drive circuitry in the Control Card (described below).

State	X	C	$\bar{H}$	Cryogenic Functions
OFF	1	0	1	No refrigerator power, heater power or vacuum pumping.
COOL	1	1	1	Normal cooled operation.
STRESS	1	0	0	COOL with a small added heat load to stress-test the cryogenic system.
HEAT	1	1	0	Fast warm-up of the dewar with 35 watts of heat added. PUMP REQ goes high when dewar vacuum is greater than 10 microns.
PUMP	0	1	0	No refrigerator or heater power. PUMP REQ is high. The vacuum solenoid is open when the manifold pressure is less than the dewar pressure.

In the CPU mode, three computer-commanded X, C, and  $\bar{H}$  control discrettes from the F117 (VLBA) or the F14 (VLA) control the cryogenic state.  $\bar{H}$  is the standard terminology for this term and the bar on top does not imply logic negation. The \* suffix denotes a logic negation; thus  $\bar{H}$  is true and  $\bar{H}^*$  is false.

### 2.4 Cryogenic Control Equations

From the table above, it would appear that when the X, C and  $\bar{H}$  control bits are set to the state appropriate for a desired cryogenic state, the cryogenic functions are automatically activated. This implied automatic activation is not the case; the commanded action will happen only if TA (15 °K stage temperature), VD (dewar vacuum), and VP (pump vacuum) parameters are in ranges appropriate for these actions and the relationship between VD and VP is correct. Control logic equations for these cryogenic functions contain discrete terms which are a function of the parameter level and an associated threshold value. If the parameter is within the specified range, the term is true and is an enabling factor in the activation of the function. If a parameter is outside the specified range, it is false and the term inhibits

the activation of the function. With the exception of the OFF state, which is unconditional, all equation terms must be true to activate the selected action. The + symbol denotes an OR function and the • symbol denotes an AND function. Parenthesis brackets delimit an AND term and a \* suffix denotes a logic negation.

When the logic equations are true, they activate the following:

- L — activates a 1/2 W dewar power load to stress-test the refrigerator.
- P — the Pump Request activates the vacuum pump.
- Q — activates a 30 W power load to heat the dewar.
- R — activates refrigerator AC power.
- S — activates the solenoid valve to enable the vacuum pump to reduce dewar pressure.

The equations are:

$$L = C \cdot \bar{H} \cdot (TA < 360 \text{ }^\circ\text{K})$$

$$P = (C + C \cdot \bar{H}) \cdot (VD > 3 \mu\text{m})$$

$$Q = (X + C) \cdot \bar{H} \cdot (TA < 360 \text{ }^\circ\text{K})$$

$$R = (C \cdot \bar{H} + C \cdot \bar{H}) \cdot (VD < 50 \mu\text{m})$$

$$S = (C + C \cdot \bar{H}) \cdot \{ (VD > 5 \mu\text{m}) \cdot (VP < VD) \cdot (TA > 30 \text{ }^\circ\text{K}) + (VD > 50 \mu\text{m}) \cdot (TA > 280 \text{ }^\circ\text{K}) \}$$

These equations are implemented on the Control Card, schematic D53200S003, described below. The X, C and  $\bar{H}$  control discrettes come from the Monitor Card, schematic D53200S005, described below. The TA, VD and VP analog signals come from the Sensor Card, schematic DD53200S002, described below.

## 2.5 Control Card Description

The Control Card (schematic D53200S003) is installed in slot 7 and implements the cryogenic control logic equations described above. During the following discussion, refer to the reduced copy of this drawing following this text. A description of the implementation of these control equations follows a description of the card inputs and outputs.

The card inputs are the TTL level X, C and  $\bar{H}$  control terms from the Monitor Card and the TA, VD and VP analog signals from the Sensor Card. TA is the 15 °K stage dewar temperature, VD is dewar vacuum and VP is the pump vacuum.

The card outputs are P, the pump request discrete, and 150 VAC power to the refrigerator, vacuum solenoid, 760 Ω dewar heater resistor and the 5 kΩ dewar heater limiting resistor. The AC power outputs are switched by relays K1 through K5. During the following discussion refer to Figure 1.3.3 on page 18 in TR 10, which shows the Front-End AC wiring. Note that a PCB track connects the 150 VAC unshifted phase input on pin X (designated 150V A on the schematic) to pins Y, W and S. Also note that a PCB track connects the 150 VAC shifted phase input on pin U (designated 150V C on the schematic) to pin V. The AC circuitry is described in Section 2.11.

See Block Diagram C53204K002 for the Control Card connections. Wire list A53203W001, Appendix page II-30, in TR 10, also describes the Control Card wiring connections.

The control equations are implemented in LS-TTL digital logic. The analog signals are threshold-compared and the comparator outputs are compatible with TTL logic. The comparator threshold levels are described below.

Three LM339N analog comparator outputs change state at three preset levels of TA. The U1-1, U1-2 and U1-14 outputs switch states when  $TA > 30\text{ K}$ ,  $TA > 280\text{ K}$  and  $TA < 360\text{ K}$ , respectively.

Three LM339N analog comparator outputs change state at three preset levels of VD. The U2-1, U2-2 and U2-14 outputs switch states when  $VD > 3\mu\text{m}$ ,  $VD > 5\mu\text{m}$  and  $VD < 50\mu\text{m}$ , respectively. One LM339N comparator, U2-13, compares VD with VP and switches high when  $VP < VD$ .

An analog comparator is a form of operational amplifier whose output makes large level changes for small differences in the two input terminals. Typically, one of the inputs, either the + or - input, is connected to a preset reference level. When the other input slightly exceeds or is slightly less than the reference input, the output makes a large change.

The LM339N comparator output is high when the voltage on the negative (-) input is more negative than the voltage on the positive (+) input. Comparators can be either inverting or non-inverting depending upon the choice of inputs for reference level and input signal. U1-14 is an inverting comparator because the + input is connected to a reference voltage and the negative (-) input is connected to the variable signal. The output swings low if the variable signal is more positive than the reference level. The operation is analogous to an inverting operational amplifier. The non-inverting comparator has the - input connected to the reference level and the variable signal is connected to the + input. The output swings high (positive) when the variable signal is more positive than the reference level. The operation is analogous to a non-inverting operational amplifier. U1-1, U1-2, U2-1, U2-2 and U2-14 are non-inverting comparators. U2-13 is a basic comparator because both inputs are variable levels. An LM339 data sheet is included in Section 4.

The comparator outputs have positive feedbacks so that the comparator's switching thresholds exhibit hysteresis. The hysteresis effect (or signal overdrive requirement) requires that the variable analog signal swing past the level that would cause the output to switch if hysteresis were not a factor. The hysteresis property applies to both positive-going and negative-going levels of the variable signal. Hysteresis is often used in analog comparator circuits to eliminate noise-induced switching when the variable level is near the reference level. Low-level noise is generally present in analog signals and comparator hysteresis prevents noise-induced switching in this situation.

TA scaling is  $10\text{ mV}/^\circ\text{K}$ . The TA comparator reference levels and associated temperatures are: U1-1,  $+0.297\text{ V}$  ( $29.7\text{ }^\circ\text{K}$ ); U1-2,  $+2.816\text{ V}$  ( $282\text{ }^\circ\text{K}$ ); U1-14,  $+3.602\text{ V}$  ( $360\text{ }^\circ\text{K}$ ). The VD comparator reference levels and associated vacuums are: U2-1,  $+0.745\text{ V}$  ( $3\text{ }\mu\text{m}$ ); U2-2,  $+1.334\text{ V}$  ( $5\text{ }\mu\text{m}$ ) and U2-14,  $+4.521\text{ V}$  ( $50\text{ }\mu\text{m}$ ). These vacuum levels are based upon the chart of vacuum monitor voltage versus vacuum on page 15 in TR 10.

The TA comparator hysteresis values are: U1-1,  $50\text{ mV}$  ( $5\text{ }^\circ\text{K}$ ); U1-2,  $50\text{ mV}$  ( $5\text{ }^\circ\text{K}$ ), U1-14,  $10\text{ mV}$  ( $10\text{ }^\circ\text{K}$ ). The VD comparator hysteresis values are: U2-1,  $278\text{ mV}$  ( $\approx 1.8\text{ }\mu\text{m}$ ); U2-2,  $350\text{ mV}$  ( $\approx 3\text{ }\mu\text{m}$ ); U2-14,  $10\text{ mV}$  ( $\approx 0.4\text{ }\mu\text{m}$ ) and U2-13,  $50\text{ mV}$  ( $\approx 2\text{ }\mu\text{m}$ ).

U10, an Analog Devices AD581JH precision voltage reference, provides a  $+10\text{ volt}$  DC reference for the comparator reference voltage dividers. Since the load on the AD581 does not vary and the Front-

Ends operate at about 25 °C, the +10 reference is stable within a few millivolts. An AD581 data sheet is included in Section 4.

Refer to the equations above. Examination of the equations shows that the terms  $C \bullet \bar{H}^*$  and  $C^* \bullet \bar{H}$  are used in four of the five equations. These two terms are formed in OR-gates U6-6 and U6-11 and are combined as required in the equations. Since the X, C, and  $\bar{H}$  control discretely are used in all the equations, the yellow CR6 (X), red CR8 (C) and CR9 ( $\bar{H}$ ) LEDs are provided to make it easier to check the card logic.

The solid-state relays K1, K2, K3 and K4 and their associated LEDs are driven by 75452 dual peripheral drivers. Each driver has a two input AND gate that drives an open-collector, high current sinking capacity output transistor. K1 through K5 are all solid-state relays with an LED input optically coupled to a solid-state AC switch.

L, the 1/2 watt load equation  $L = C^* \bullet \bar{H} \bullet (TA < 360K)$ , causes a 5 k $\Omega$  limiting resistor to be inserted in series with the 760  $\Omega$  dewar heater resistor. The resistor is inserted by closing relay K2; K3 is open in this state. (See the Front-End AC wiring schematic on page 18 in TR 10.) The term T3 ( $TA < 360$  °K) from comparator U1-14 is AND-ed with H in U6-4. This is AND-ed with  $C^*$  in U7-3 (a 75452) and the output is low when all three terms are high-true. The low-true output sinks current from +15 V through the coil of relay K2 and CR4, a yellow LED (5 k $\Omega$ ). The relay's output switch connects the lower end of the 5 K $\Omega$  resistor to AC low.

Q, the dewar heater equation  $Q = (X^* + C^*) \bullet \bar{H} \bullet (TA < 360K)$ , uses the  $T3 \bullet \bar{H}$  product from U6-6. It is AND-ed with  $X^* + C^*$  from U11-1 in gate U8-5 (a 75452). The output is low-true when all three terms are high-true and sinks current from +15 V through the LED of relay K3 and the red LED (HEATER), CR3. K3's output applies 150 VAC to the 760  $\Omega$  dewar heater resistor.

P is the pump request equation  $P = (C + C^* \bullet \bar{H}) \bullet (VD > 3 \mu m)$ . AND gate U6-3 uses the  $C + C^* \bullet \bar{H}$  term from U5-3 (mentioned above) and the V1 term from comparator U2-1 ( $VD > 3 \mu m$ ). The output is high-true if both input terms are high-true. This P (pump request) output goes to the auxiliary connector pin J4-3 to drive an external vacuum pump control circuit. It is also connected to the monitor connector J2-21 to enable the monitor and control system to read the P state. CR7 (PUMP), a yellow LED, sinks current through inverter U3-2 from +5 volts when P is high.

R, the refrigerator power equation  $R = (C \bullet \bar{H}^* + C^* \bullet \bar{H}) \bullet (VD < 50 \mu m)$ , uses the  $(C \bullet \bar{H}^* + C^* \bullet \bar{H})$  term from U5-6 (described above). This term is inverted to low-true by U3-8, which drives a 74LS32 gate U5-8. In this application, the 74LS32 functions as a low-true AND. The U5-8 output is low-true only if both inputs are low. V3,  $VD > 50 \mu m$  is the other U5 input. This term is high when  $VD > 50 \mu m$  and low when  $VD < 50 \mu m$ . Thus the U5-8 output is low when  $(C \bullet \bar{H}^* + C^* \bullet \bar{H}) \bullet (VD < 50 \mu m)$ . U8 is a 75452. The pin 1 input is connected to +5 through a 4.7 K $\Omega$  resistor so that output U8-3 is high when the equation is true. The U8-3 output sinks current from +15 V through K4's LED and a 750  $\Omega$  resistor. When K5 is actuated, it connects the 150 VAC return (or common) to the refrigerator. Note from the block diagram above that card pin X is connected to 150 VAC, Phase 1, the unshifted phase. This line drives a rectifier-divider-filter circuit consisting of CR2 (1N4007), R35 (10k $\Omega$ ), R36 (1k $\Omega$ ) and C9 (100  $\mu F$ ). When the 150 VAC, Phase 1 power is present at the filter input, C9 charges to about 19.3 volts. Note that K4's contacts are connected to the junction of the 10 k $\Omega$  and 1 k $\Omega$  resistors and to the low side of the capacitor so that when K4 is actuated, the filter input is shorted. When the equation is true, K4

is not actuated, its contacts are open, and the capacitor is charged to about 19 volts. This DC voltage drives K5's LED, which closes its output contacts to pass the 150 VAC return (or common) to the refrigerator. Section 4 has data sheets for the 75452 and the relays.

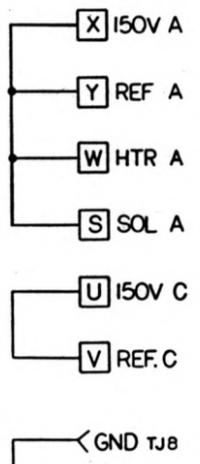
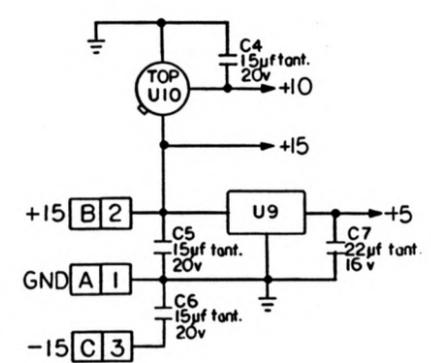
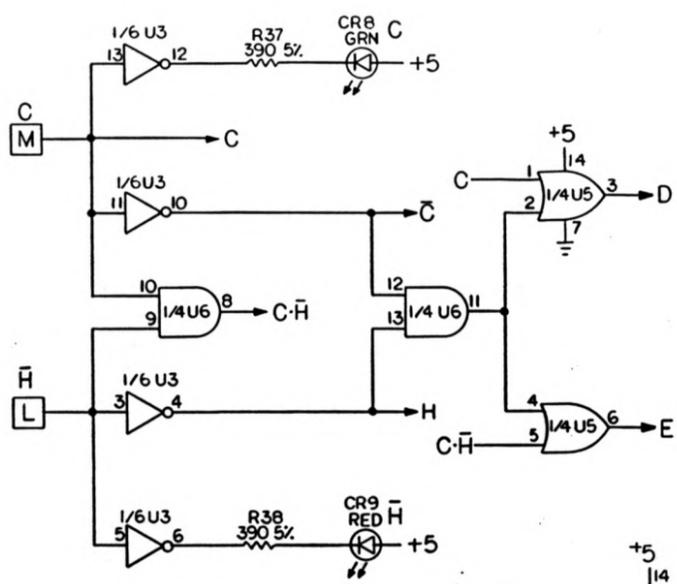
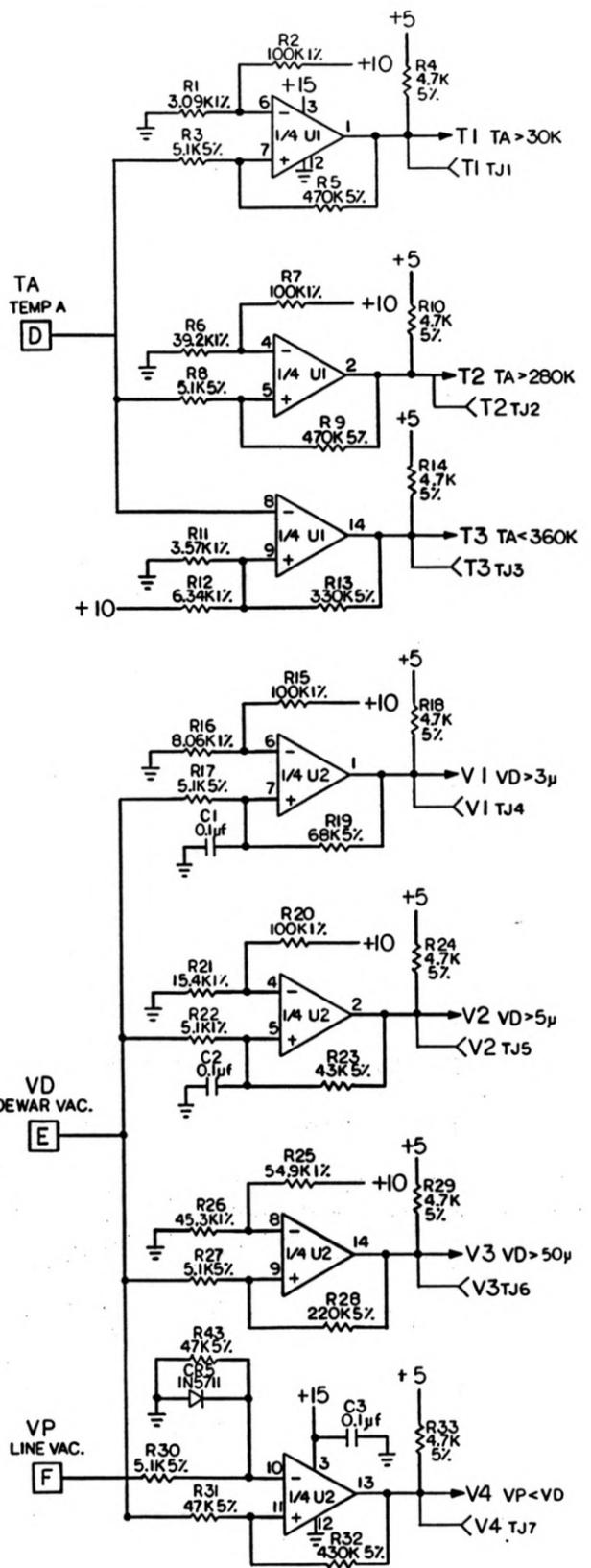
S, the solenoid equation, is the most complicated and is the OR sum of two sets of AND products.  $S = (C+C*\bar{H}) \bullet \{(VD>5\mu m) \bullet (VP<VD) \bullet (TA>30K) + (VD>50\mu m) \bullet (TA>280K)\}$ . The term D ( $C+C*\bar{H}$ ) is common to both products. Consider the first set of products. The first term,  $C+C*\bar{H}$ , is formed by U5-3. The second term, V2 ( $VD>5\mu m$ ), is the output of comparator U2-1. The third term, V4 ( $VP<VD$ ), is the output of comparator U2-13. The fourth term T1, ( $TA>30^\circ K$ ), is the output of comparator U1-1. ( $VD>5\mu m$ ), ( $VP<VD$ ) and ( $TA>30^\circ K$ ) are AND-ed in gate U4-6. The output is ORR-ed in gate U5-11, a 75452 driver, with the second product. The second product is formed in U4-12, which has the inputs V3 ( $VD>50\mu m$ ) and T2 ( $TA>280^\circ K$ ). The U5-11 output drives one input on U7-5. The other input is the D ( $C+C*\bar{H}$ ) term from U5-3. U7-5 sinks current through K1's LED and CR1 (SOL), a yellow LED. The SMON term, a monitor discrete, is formed in gate U4-8 by the output of U5-11 and D. The Solenoid valve is an inductive device and if it does not actuate, the solenoid's AC current demand can be as high as 0.40 amperes. To protect K1 from current-induced voltage surges, an MOV and series RC circuit are connected across K1's output. The MOV clips voltage peaks and the RC circuit provides additional surge protection to K1.

For convenience in maintenance, the card LEDs mentioned above and circuit level test jacks are placed on the card edge for easy access. LED and test jack labels are silkscreened on the card. See the card assembly drawing D53200A004 for the locations.

The card's +5 volt logic power is derived from +15 volt power by U9, a MC7805, 5-volt DC regulator.

### Control Card Alignment

The Control Card does not have any alignment adjustments. There is not a Control Card tester or formal card alignment procedure but the circuit operations can be evaluated using the card's maintenance features, the Monitor Panel DVM and the Monitor Panel State Select switch, S1. The levels of four analog signals, TA ( $15^\circ K$ ), VD, VP and ACI (AC current load), can be measured using the DVM. The states of the comparator outputs (via card test jacks) can be related to these analog signal levels. LEDs on the X, C and  $\bar{H}$  control discretes enable verification of the control inputs from the Monitor Card. LEDs on the outputs of the five equation's logic circuits indicate the state of the equation's logic output. The Monitor Panel's State switch S1 can be set to select any of the five possible manual-mode states. This will cause the X, C and  $\bar{H}$  states to activate the logic equations as described above. In most cases, the card circuitry can be evaluated by selecting a cryogenic state, noting the TA, VD, VP, and ACI analog levels, the associated comparator outputs, and the response of the solenoid, the refrigerator, vacuum pump, dewar heater, and 1/2 watt load to these signal levels and control states.

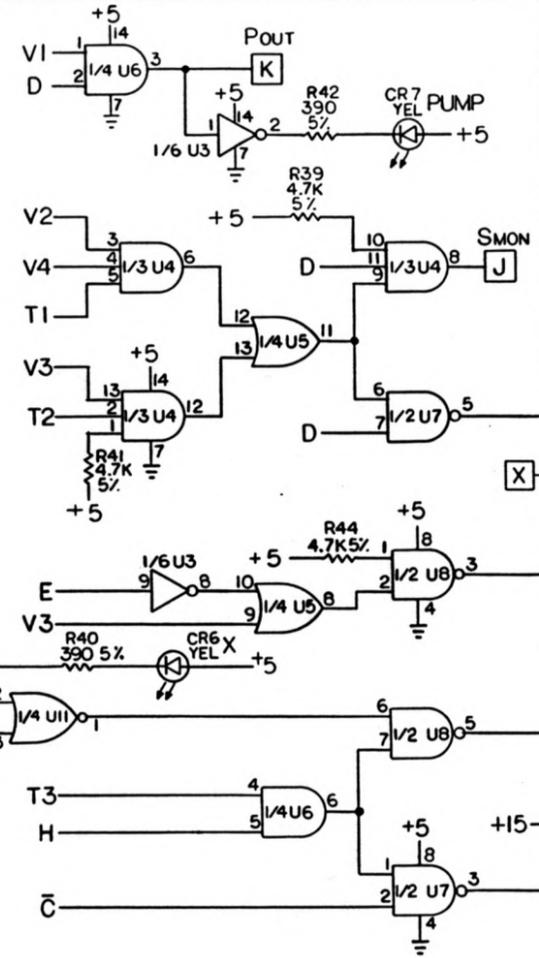


**CONTROL LOGIC\***

- L=1/2 W Load =  $\bar{C} \cdot H \cdot (TA < 360K)$
- P=Pump Request =  $(C + \bar{C} \cdot H) \cdot (VD > 3\mu)$
- Q=Heater 30 W =  $(\bar{X} + \bar{C}) \cdot H \cdot (TA < 360K)$
- R=Refrigerator PWR =  $(C \cdot \bar{H} + \bar{C} \cdot H) \cdot (VD < 50\mu)$
- S=Valve Open (Sol. On) =  $(C + \bar{C} \cdot H) \cdot (VD > 5\mu) \cdot (VP < VD) \cdot (TA > 30K) + (VD > 50\mu) \cdot (TA > 280K)$

**NOTES**

1. U1-U2 - LM339N
2. U3 - 74LS04
3. U4 - 74LS11
4. U5 - 74LS32
5. U6 - 74LS08
6. U7-U8 - 75452
7. U9 - 7805CT
8. U10 - AD581JH
9. ALL CAPS. ARE 50V UNLESS OTHERWISE MARKED.
10. ALL RES. AS FOLLOWS:  
1% 1/8WATT  
5% 1/4WATT
11. K1-K3 - 645-2
12. U11 - 74LS02
13. K4 - 643-1
14. K5 - MP240D4



**CONTROL STATES\***

STATE	CONTROL BIT X	CONTROL BIT C	CONTROL BIT H	OCTAL VALUE	SYSTEM MODE
COOL	1	1	1	7	NORMAL
LOAD	1	0	0	4	1/2 W LOAD
OFF	1	0	1	5	NO COOL, HEAT OR PUMP
PUMP	0	1	0	2	PUMP ONLY
HEAT	1	1	0	6	PUMP AND HEAT (30W)
UNUSED	0	0	0	0	LOAD
UNUSED	0	0	1	1	OFF
UNUSED	0	1	1	3	COOL

\*TTL LOGIC 1=ON =HI LEVEL  
0=OFF=LO LEVEL

REV	DATE	DRAWN BY	APPROV'D BY	DESCRIPTION
D	4-87	W.WINTER		ADDED TO NOTES
C	1-86	G.MOERS		CO-260130-06
B	8/85	G.MOERS		
A	8/84	H.D.H.		CO-840817-20

FRONT ENDS

**CONTROL CARD**

NATIONAL RADIO ASTRONOMY OBSERVATORY  
CHARLOTTEVILLE, VA. 22901

ORDER BY: H.DILL 840710  
DESIGNED BY: S.WEINREB 840622  
APPROVED BY: DATE

SHEET 1 of 1 DRAWING NUMBER: 0532009003 REV D SCALE



8

7

6

5

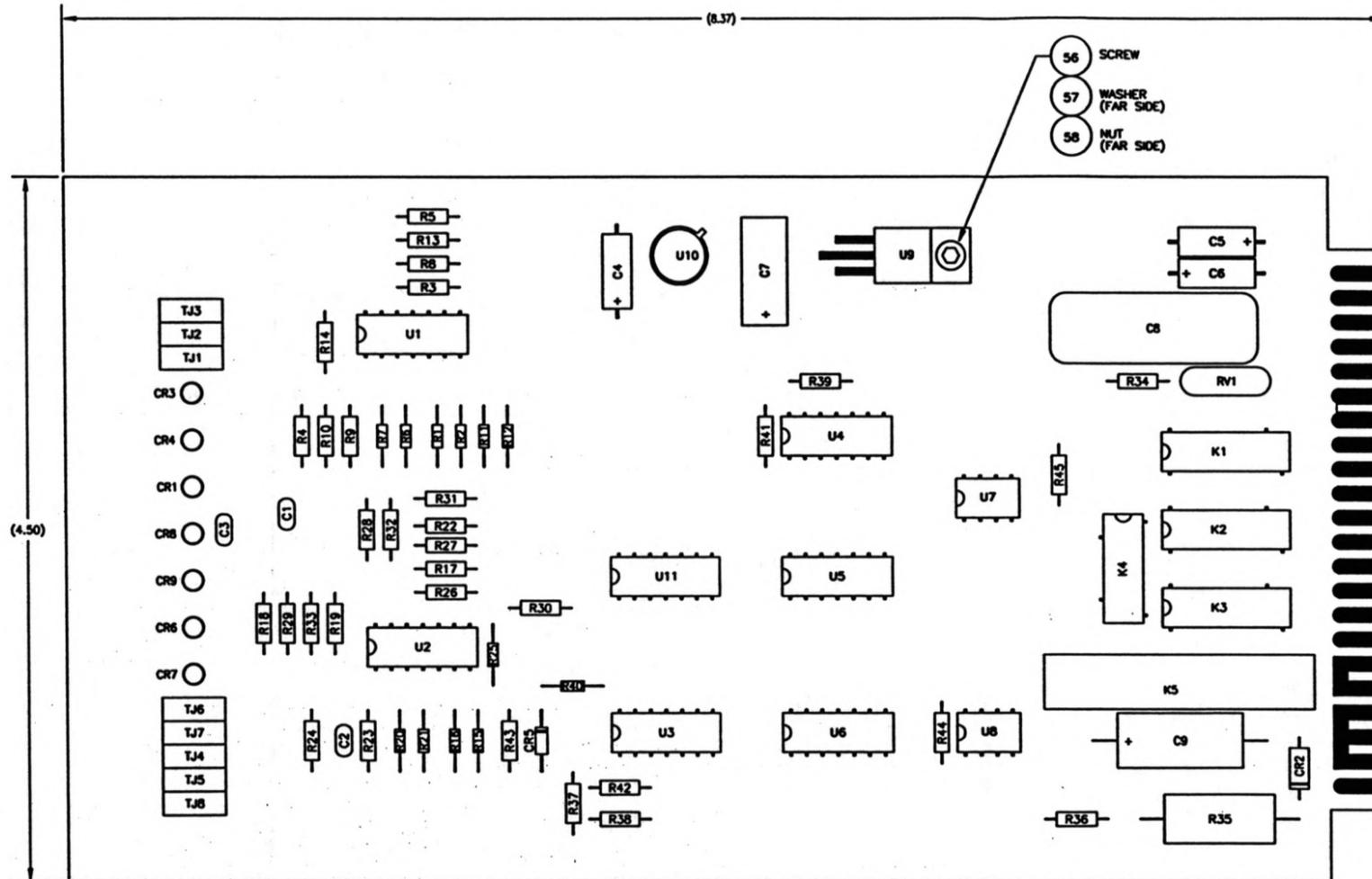
4

3

2

1

REV	DATE	DRAWN BY	APPRVD BY	DESCRIPTION
C	9-94	TATE	PETENCIN	REVISED AND REDRAWN



CIRCUIT BOARD 1

COMPONENT SIDE

58				NUT, HEX, SS, 4-40UNC-2B	1
57				WASHER, LOCK, #4	1
56				SCREW, SOCKET HEAD, SS, 2-40UNC-2A x .75 LONG	1
55	U7-U8	AUGAT	608-CG1	SOCKET, 8-PIN	2
54	U1-U6, U11	AUGAT	614-CG1	SOCKET, 14-PIN	7
53	U11	TEXAS INSTRUMENTS	SN74LS02N	GATE, NOR, QUAD INPUT	1
52	U10	ANALOG DEVICES	AD581JH	REFERENCE, VOLTAGE	1
51	U9	MOTOROLA	MC7805CT	REGULATOR, POSITIVE	1
50	U7, U8	TEXAS INSTRUMENTS	SN75452BP	GATE, NAND	2
49	U6	TEXAS INSTRUMENTS	SN74LS08N	GATE, AND, 2-INPUT	1
48	U5	TEXAS INSTRUMENTS	SN74LS32N	GATE, OR, 2-INPUT	1
47	U4	TEXAS INSTRUMENTS	SN74LS11N	GATE, AND, 3-INPUT	1
46	U3	TEXAS INSTRUMENTS	SN74LS04N	INVERTER, HEX	1
45	U1, U2	MOTOROLA	LM339N	COMPARATOR, QUAD	2
44	TJ8	E.F. JOHNSON	105-0751-001	TEST JACK, BLACK	1
43	TJ6	E.F. JOHNSON	105-0751-001	TEST JACK, WHITE	1
42	TJ5	E.F. JOHNSON	105-0751-001	TEST JACK, RED	1
41	TJ3	E.F. JOHNSON	105-0751-001	TEST JACK, GREEN	1
40	TJ2, TJ4	E.F. JOHNSON	105-0751-001	TEST JACK, YELLOW	2
39	TJ1, TJ7	E.F. JOHNSON	105-0751-001	TEST JACK, BLUE	2
38	RV1	TELEDYNE	970-2	VARISTOR, METAL OXIDE	1
37	R45	ALLEN-BRADLEY	RC07GF751J	RESISTOR, 750, 1/4W, 5%	1
36	R39	ALLEN-BRADLEY	RC07GF391J	RESISTOR, 390, 1/4W, 5%	4
35	R36	ALLEN-BRADLEY	RC07GF102J	RESISTOR, 1K, 1/4W, 5%	1
34	R35	ALLEN-BRADLEY	RC42GF103J	RESISTOR, 10K, 2W, 5%	1
33	R34	ALLEN-BRADLEY	RC07GF470J	RESISTOR, 47, 1/4W, 5%	1
32	R32	ALLEN-BRADLEY	RC07GF434J	RESISTOR, 430K, 1/4W, 5%	1
31	R31, R43	ALLEN-BRADLEY	RC07GF473K	RESISTOR, 47K, 1/4W, 5%	2
30	R28	ALLEN-BRADLEY	RC07GF222R	RESISTOR, 220K, 1/4W, 5%	1
29	R26	DALE	RN55C4532F	RESISTOR, 45.3K, 1/8W, 1%	1
28	R25	DALE	RN55C5492F	RESISTOR, 54.9K, 1/8W, 1%	1
27	R23	ALLEN-BRADLEY	RC07GF433J	RESISTOR, 43K, 1/4W, 5%	1
26	R21	DALE	RN55C1542F	RESISTOR, 15.4K, 1/8W, 1%	1
25	R19	ALLEN-BRADLEY	RC07GF683J	RESISTOR, 68K, 1/4W, 5%	1
24	R16	DALE	RN55C8061F	RESISTOR, 8.06K, 1/8W, 1%	1
23	R13	ALLEN-BRADLEY	RC07GF334J	RESISTOR, 330K, 1/4W, 5%	1
22	R12	DALE	RN55C6341F	RESISTOR, 6.34K, 1/8W, 1%	1
21	R11	DALE	RN55C3571F	RESISTOR, 3.57K, 1/8W, 1%	1
20	R6	DALE	RN55C3922F	RESISTOR, 39.2K, 1/8W, 1%	1
19	R5, R9	ALLEN-BRADLEY	RC07GF474J	RESISTOR, 470K, 1/4W, 5%	2
18	R14, R15, R16, R17, R18	ALLEN-BRADLEY	RC07GF472J	RESISTOR, 4.7K, 1/4W, 5%	10
17	R13, R14, R15, R16, R17, R18	ALLEN-BRADLEY	RC07GF512J	RESISTOR, 5.1K, 1/4W, 5%	6
16	R12, R20	DALE	RN55C1003F	RESISTOR, 100K, 1/8W, 1%	4
15	R1	DALE	RN55C3091F	RESISTOR, 3.09K, 1/8W, 1%	1
14	K5	NTE ELECTRONICS	RSI-ID4-2I	RELAY	1
13	K4	TELEDYNE	643-1	RELAY	1
12	K1-K3	TELEDYNE	645-2	RELAY	3
11	CR8	GENERAL INSTRUMENT	CMD5274C	LED, GREEN	1
10	CR5	HEWLETT PACKARD	1N5711	DIODE, SCHOTTKY	1
9	CR3, CR9	GENERAL INSTRUMENT	CMD5774C	LED, RED	2
8	CR2	MOTOROLA	1N4007	DIODE	1
7	CR1, CR7	GENERAL INSTRUMENT	CMD5374C	LED, YELLOW	4
6	C9	MALLORY	CSR13E107KP	CAPACITOR, TANT, 100uf, 50V	1
5	C8	SPRAGUE	6PS-S47	CAPACITOR, 47uf, 600V	1
4	C7	MALLORY	CSR13E226KP	CAPACITOR, TANT, 22uf, 20V	1
3	C4-C6	MALLORY	CSR13E156KP	CAPACITOR, TANT, 15uf, 20V	3
2	C1-C3	KEMET	C330C104M5U5CA	CAPACITOR, 1uf, 50V	3
1		NRAO	D53200Q003	BOARD, CIRCUIT	1

ITEM NO.	REF. DES.	MANUFACTURER	PART NUMBER	DESCRIPTION	QTY
UNLESS OTHERWISE SPECIFIED DIMENSIONS ARE IN INCHES					
MATERIAL :					
FINISH :					
NEXT ASSEMBLY :					

D53200S003	SCHEMATIC
D53200A003	ARTWORK
D53200P003	DRILL DWG
D53200I008	SILKSCREEN
D53200M004	SOLDER MASK
	DWG. TYPE

COMMON FRONT END		NATIONAL RADIO ASTRONOMY OBSERVATORY	
FRONT END CONTROL PCB ASSEMBLY		SOCORRO, NEW MEXICO 87801	
DESIGNED BY	H. DILL	DATE	9-85
DESIGNED BY	S. WEINREB	DATE	9-85
APPROVED BY	S. WEINREB	DATE	9-85
SHEET NUMBER	1 of 1	DRAWING NUMBER	D53200A004
REV.	C	SCALE	2/1

ACAD : 53200A04



## 2.6 Monitor Card Description

The Monitor Card is installed in Slot 3 and has two functions: mode-state control via S1 (the Monitor Panel Mode-State switch) and its associated logic and local analog monitoring using the Monitor Panel DVM and S2, the Monitor Select Switch. Drawing C53200S005 shows the Monitor Card circuitry. Section 4 contains a data sheet for the DVM, a Texmate PM-45XU 4½ digit panel meter.

The Monitor Panel is attached to the Monitor Card so that the card and panel are a single assembly. Figure 1 shows the Monitor Panel.

See Block Diagram C53204K002 for the Monitor Card connections. Wire list A53203W001, Sheet 4, TR 10 Appendix page II-18, also describes the Monitor Card wiring connections.

S1, the mode-state selector switch, has six positions: HEAT, PUMP, OFF, LOAD, COOL and CPU. When the switch is in the CPU position, the Front-End is controlled by the control computer via F117 (VLBA) or F14 (VLA). In the other five positions, the Front-End cryogenic state is controlled by the setting of S1 as shown in the table in Section 2.3 above.

The Monitor mode-state logic is simple encoding and multiplexing logic. S1, the mode-state switch wiper, is connected to ground. The HEAT, PUMP, OFF, STRESS and COOL contacts are connected to +5 volt pull-up resistors and the inputs of U1, a 74LS148, 8-line to 3-line priority encoder. The sixth position, CPU A0, A1 and A2 outputs are the X, C, and H control discretes, respectively. Since S1 has physical stops and the encoder inputs are low-true, the other three encoder inputs can safely float.

The X, C, and  $\bar{H}$  encoder outputs are connected to the B inputs of U2, a 74LS157 quad 2-input multiplexer. The multiplexer A inputs are the X, C, and  $\bar{H}^*$  cryogenic state command inputs from the CPU (via F14 or F117). The multiplexer outputs drive the X, C, and  $\bar{H}^*$  inputs of the Control Card described in Section 2.5 above. The multiplexer A/B input selection is controlled by S1. When S1 is in the CPU position, the 2 kΩ pull-up resistor to +5 volts causes the multiplexer to select the A inputs; in any of the other five positions, the encoder outputs are selected. The three multiplexer outputs are connected to the Control Card.

The choice of encoder states is rather important. If through some mischance or malfunction the

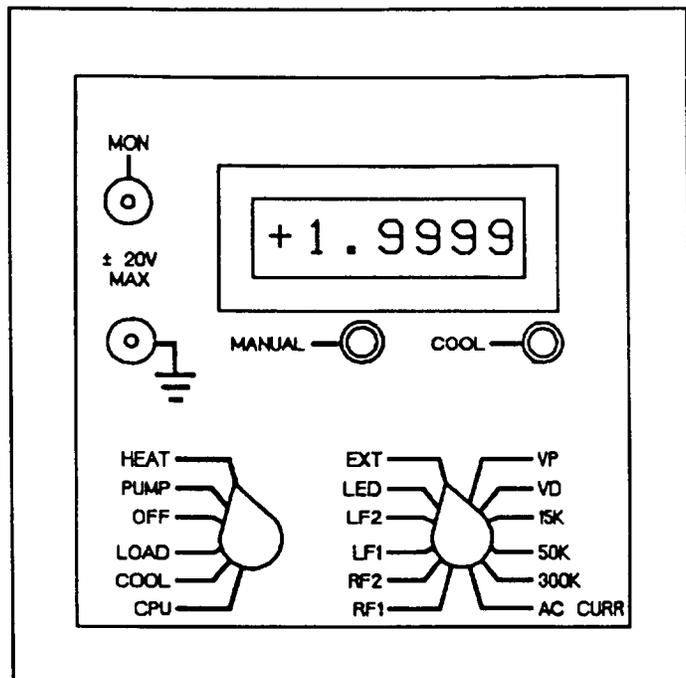


Figure 1 Monitor Panel

C and H\* bits are stuck high or low, the Control Card will assume either the COOL or LOAD states, the desired default cryogenic states.

Three OR gates in U3, a 74LS32, are used as isolating buffers on the X, C, and  $\bar{H}$  lines to J2, the cryogenic state monitor outputs to F117 or F14 via J2. In the event of an inadvertant short on these lines, the buffers protect the X, C, and H inputs to the Control Card.

Gate U4-8 decodes the COOL state to sink current from a Monitor Panel red LED, CR2. When S1 is in the CPU position, gate U4-12 sinks current from a Monitor Panel red LED, CR1. The state of U4-12 is output to F117 and F14 via J2.

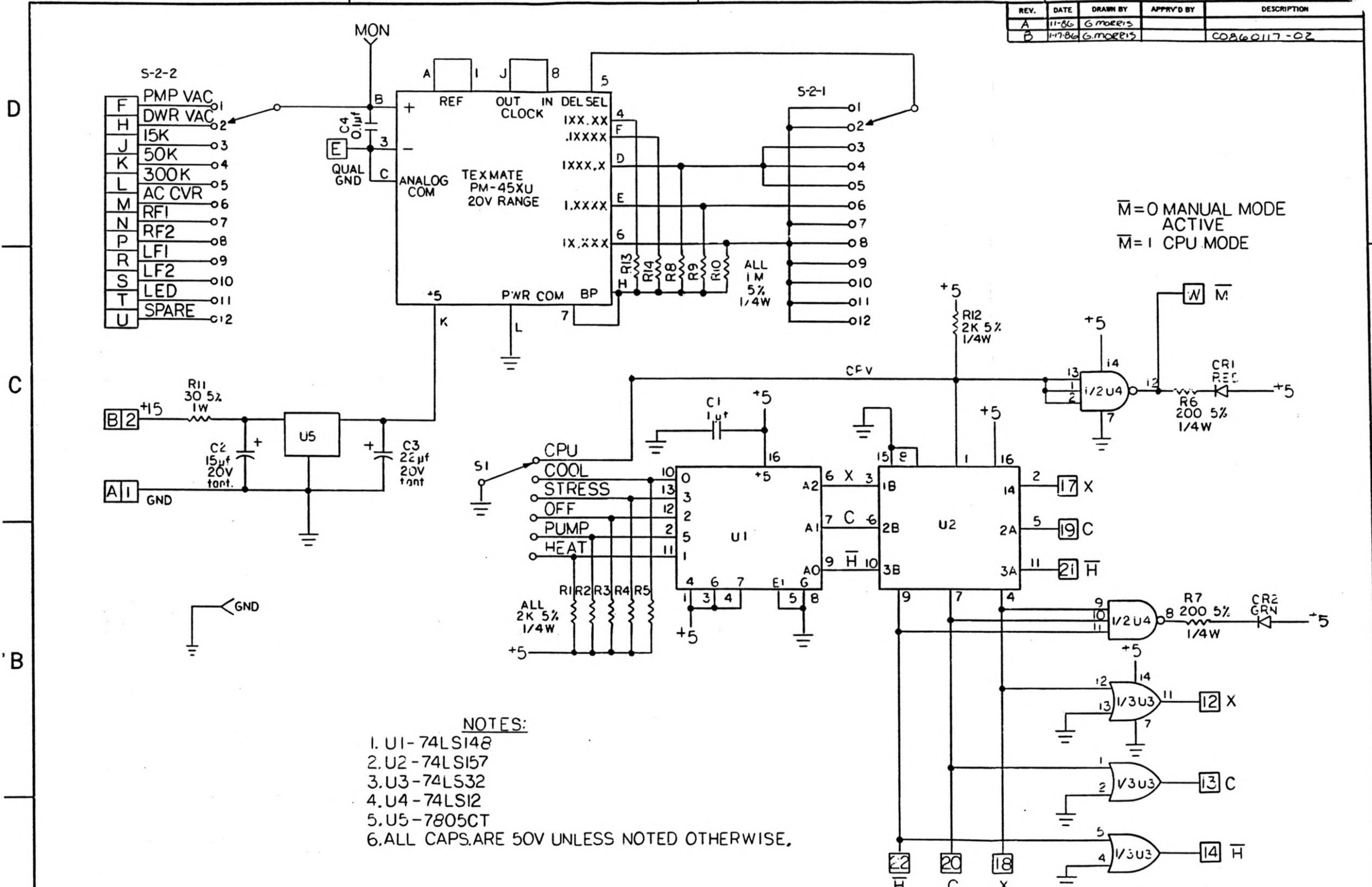
Five volt logic and DVM power is provided by U5, a 7805CT series regulator. Note that the DVM signal ground reference is Quality Ground from J2-13.

The Texmate PM-45-XU has jumper connectors to control its mode and the decimal point is selected by section 1 of the Monitor Select switch, S2. A pair of test jacks on the panel permits an external meter to be connected to the DVM input if there is some question about the DVM values. Since a DVM data sheet is included in Section 4, it is not described here.

Typical values and tolerances for the analog parameters measured by the DVM are described in Section 2.12.

There are no alignment adjustments for the Monitor Card. The card logic is so simple that it can be checked by setting the mode-state switch to the six positions and noting the states of the Monitor Panel LEDs (COOL and MAN) and the Control Card X, C, and  $\bar{H}$  LEDs.

REV.	DATE	DRAWN BY	APPR'D BY	DESCRIPTION
A	11-86	G.MORRIS		
B	1-7-86	G.MORRIS		COB60117-02



$\bar{M}=0$  MANUAL MODE ACTIVE  
 $\bar{M}=1$  CPU MODE

- NOTES:
1. U1-74LS148
  2. U2-74LS157
  3. U3-74LS32
  4. U4-74LS12
  5. U5-7805CT
  6. ALL CAPS. ARE 50V UNLESS NOTED OTHERWISE.

UNLESS OTHERWISE SPECIFIED DIMENSIONS ARE IN INCHES  
 TOLERANCES: ANGLES ±  
 3 PLACE DECIMALS (.XXX): ±  
 2 PLACE DECIMALS (.XX): ±  
 1 PLACE DECIMALS (.X): ±

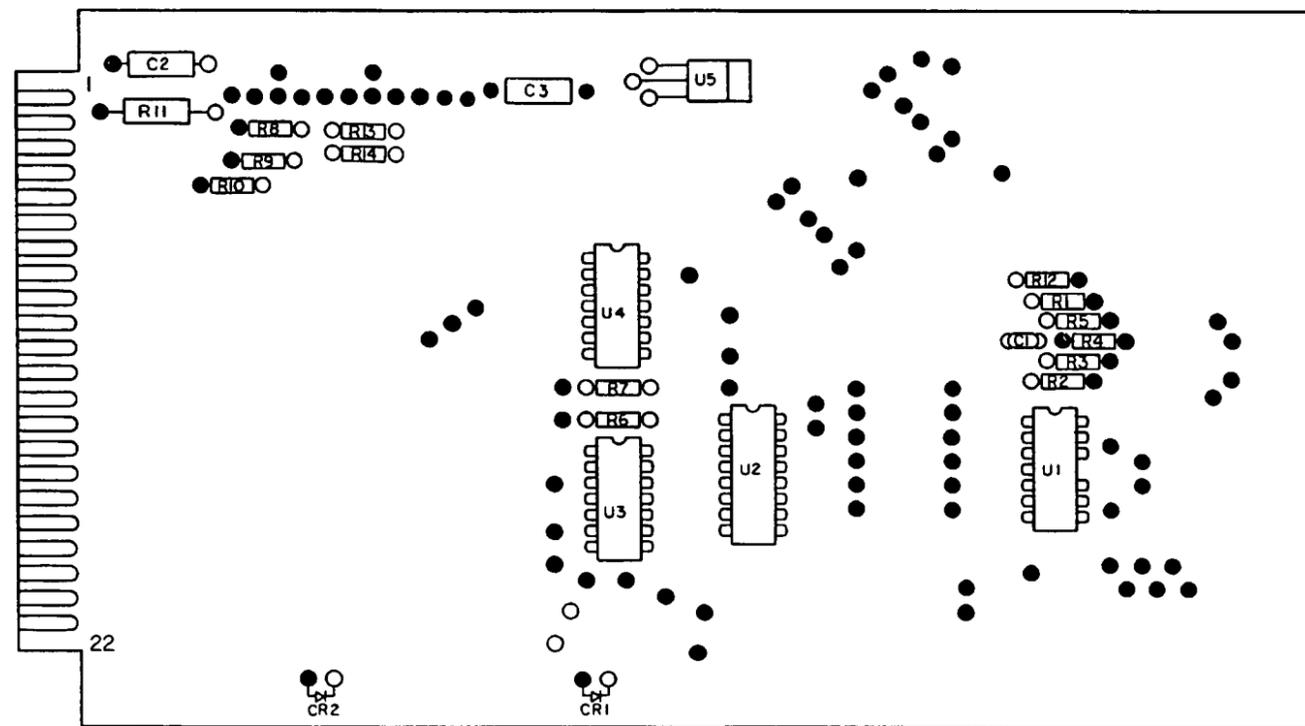
FRONT END		NATIONAL RADIO ASTRONOMY OBSERVATORY	
MONITOR BOARD		DRAWN BY G.MORRIS	DATE 6-30-83
		DESIGNED BY S.WEINREIB	DATE 7-15-83
		APPROVED BY	DATE
SHEET NUMBER	DRAWING NUMBER C53200S0C5	REV. B	SCALE

MATERIAL:	
FINISH:	
NEXT ASSY	USED ON

D  
C  
B  
A



REF. DES.	PART DESCRIPTION	PART NO.	ITEM NO.
C1	CAP 1µf 50V	C330C105M5U5CA	11
C2	CAP 15µf 20V TANT.	CSR13E156KP	12
C3	CAP 22µf 20V TANT.	CSR13E226KP	13
CR1	DIODE RED	MJ5752	24
CR2	DIODE GREEN	MJ64521	25
R1	RES 2K 1/4W 5%	RC07GF202J	26
R2	RES 2K 1/4W 5%	RC07GF202J	27
R3	RES 2K 1/4W 5%	RC07GF202J	28
R4	RES 2K 1/4W 5%	RC07GF202J	29
R5	RES 2K 1/4W 5%	RC07GF202J	30
R6	RES 200 1/2W 5%	RC20GF201J	7
R7	RES 200 1/2W 5%	RC20GF201J	7
R8	RES 1M 1/4W 5%	RC07GF105J	3
R9	RES 1M 1/4W 5%	RC07GF105J	3
R10	RES 1M 1/4W 5%	RC07GF105J	3
R11	RES 30 1W 5%	RC32GF300J	6
R12	RES 2K 1/4W 5%	RC07GF202J	8
U1	IC 74LS148	SN74LS148N	15
U2	IC 74LS157	SN74LS157N	16
U3	IC 74LS32	SN74LS32N	17
U4	IC 74LS12	SN74LS12N	18
U5	VOLTAGE REG 5V	7805CT	14
R3	RES 1M 1/4W 5%	RC07GF105J	3
R4	RES 1M 1/4W 5%	RC07GF105J	3



COMPONENT SIDE

NOTES: HOLES THAT ARE SHADED TO BE PLATED THRU.

DEILL DWG. 053200P004  
SCH. DWG. C53200S005

REV	DATE	DRAWN BY	APPR'D BY	DESCRIPTION
V				FRONT END
A				ASSY-MONITOR CARD

NATIONAL RADIO ASTRONOMY OBSERVATORY	
CHARLOTTEVILLE, VA. 22901	
DRAWN BY	DATE
DESIGNED BY	DATE
APPROVED BY	DATE

A (1/4W) 1/2W ITEM NOS  
REV DATE BY DESCRIPTION

SHEET NUMBER DRAWING NUMBER 053200A006 REV A SCALE 2X



## 2.7 Sensor Card Description

The Sensor Card, slot 6, contains the interface circuitry for two Teledyne-Hastings DV-6R vacuum gauges and two Lake Shore DT-500-KL diode temperature sensors. The vacuum gauges sense dewar vacuum (VD) and the pump or manifold vacuum (VP) and the two diodes sense the 15 °K (TA) and 50 °K (TB) dewar temperature stages.

The conditioned VD, VP, and TA outputs of the Sensor Card are connected to the Control Card, slot 7, for use in controlling the Front-End's cryogenic states. They are also connected to the Monitor Card for local monitor readout on the DVM and to J2 for readout by the Monitor and Control System. A non-linear form of TA is also connected to J2 for Monitor and Control System readout. This signal has a higher sensitivity and potentially greater accuracy because it is not subjected to linearizing corrections. TB is not used by the Control Card but is connected to the Monitor Card for DVM readout and is also connected to J2 for Monitor and Control System readout. See Block Diagram C53204K002 for the Sensor Card connections. Wire list A53203W001, TR 10 Appendix page II-29, also describes the Sensor Card wiring connections. The Sensor Card schematic is D53200S002 and the assembly drawing is D53200A003.

### Teledyne-Hastings DV-R6 Vacuum Guages

The Hastings DV-6R vacuum gauge is a ruggedized, precision vacuum sensing gauge with a specified range of 0 to 1000  $\mu\text{m}$  of Hg (sea-level atmospheric pressure is 760,000  $\mu\text{m}$  of Hg.). The DV-6R is a thermopile consisting of three identical noble-metal alloy thermocouples; see Figure 2 which shows the sensor and its connections to the VD interface amplifier. The + symbol indicates the thermal EMF polarity. The thermocouple alloys are Gold/Platinum and Platinum/Rhodium. All three thermocouples sense the gas pressure and the - (negative thermal EMF polarity) sides of all three are connected to DV-6R pin 8, which is simply a tie-point that is not connected to any external circuitry. The + sides of two thermocouples are connected to pins 3 and 5 and are heated by the AC excitation. The + side of the third thermocouple is connected to pin 7, is not heated by the AC excitation, and is analogous to the reference junction in a conventional thermocouple circuit. The thermal EMF of this third thermocouple is determined by the temperature of the sensed gas, is very small, and its polarity is in opposition to the thermal EMF of the heated thermocouples.

The vacuum-sensing properties of the DV-6R are a function of the sensed air's thermal conductivity, which decreases when the air pressure is decreased. A decreasing thermal conductivity increases the hot junction's temperatures, which increases the thermopile DC output. At a high vacuum, the hot junction temperature is about 300 °C. In the dewar and manifold vacuum-sensing applications, the DV-6R sensitivity is determined by the AC heating power delivered to the thermocouple junction; the Sensor Card VD ZERO and VP ZERO adjustments determine this power level. Hastings does not have an explicit

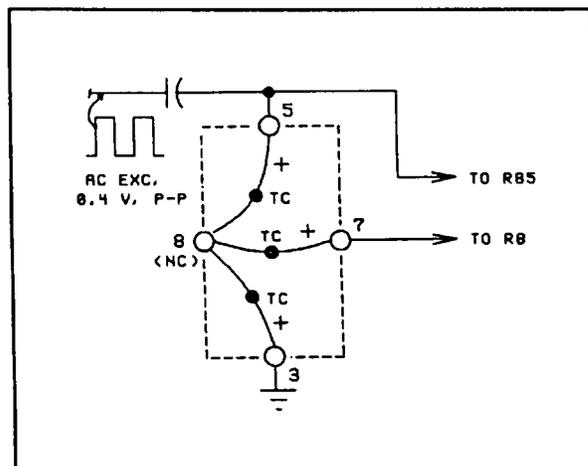


Figure 2 DV-6R Connections

mathematical expression for DC output as a function of the sensed air pressure but the DV-6R's output is roughly a logarithmic function of pressure. Hastings states that the DV-6R accuracy is about  $\pm 2\%$  at a high vacuum ( $\approx 1 \mu\text{m}$ ).

Page 15 (in TR 10) shows a graph of the Sensor Card vacuum interface circuit readout voltage versus dewar pressure. At a vacuum of  $1 \mu\text{m Hg}$ , and with the appropriate AC excitation, the nominal DV-6R sensitivity (output voltage change /vacuum change) is  $-161 \text{ mV}/\mu\text{m}$ ; this is the DV-6R's highest sensitivity. As pressure increases, the sensitivity rapidly decreases. At  $1000 \mu\text{m}$  the interface circuit output is  $+9652 \text{ mV}$  and at sea level atmospheric pressure, the interface circuit output is  $+10,000 \text{ mV}$ . The nominal sensitivity of  $-161 \text{ mV}/\mu\text{m}$  at  $1 \mu\text{m}$  is the value used in Sensor Card alignment.

Hastings' vacuum thermopile interface circuit uses a center-tapped transformer secondary that drives pins 3 and 5 with a 0.38 volt, P-P square wave; this heats the two thermocouples connected back-to-back across pins 3 and 5. The primary is driven by a 5 kHz power oscillator. The thermopile's DC output connections are pin 7 (the + side of the unheated thermocouple) and the transformer center-tap. Relative to pin 7, the heated thermocouple's DC voltages on pins 3 and 5 are identical because the two heated thermocouples are in parallel. Hastings typically connects the DC output to an analog current meter with a  $40 \Omega$  current limiting resistor. The Hastings' interface's meter scale is calibrated for the sensor's working range.

The DV-6R interface circuits are aligned by substituting a Hastings DB-20 reference tube for the DV-6R. The DB-20 simulates the DV-6R at some high vacuum level, typically  $2 \mu\text{m}$ . In a recent lab test, a Hastings DB-20 Reference Tube marked  $2 \mu\text{m}$  was substituted for the DV-6R. The DB-20 DC output measured on pin L of the Sensor Card was  $-287 \text{ mV}$ . Although this was slightly under the expected  $322 \text{ mV}$ , the Sensor Card circuit aligned normally. The vacuum interface alignment procedure is described below. A Hastings DV-6R data sheet is included in Section 4.

The vacuum gauge interface circuitry is shown on the left half of the Sensor Card schematic drawing, D53200S002. Note that there are three connections to the DV-6R.

### Vacuum Gauge Interface Circuitry

The DV-6R vacuum gauges require an AC excitation. An oscillator and two power buffers provide the AC power to drive the thermopiles. The oscillator is U4-8, a TI TL084BCN operational amplifier used in an RC relaxation oscillator circuit. The oscillation results from an alternating sequence of capacitor charge-discharge ramps. One output cycle consists of a capacitor charge period and a capacitor discharge period; therefore the capacitor's voltage waveform is a sawtooth and the oscillator's output is a square wave. The amplifier's negative (-) input is connected to the capacitor-resistor junction. The amplifier's positive (+) input is connected to a center-tapped  $48 \text{ k}\Omega$  resistive voltage divider, connected to the amplifier's output; therefore, the amplifier's + input voltage is always half the output voltage. Capacitor C14 is charged (or discharged) through resistor R81 until a switching threshold is reached; at the threshold, the amplifier's output switches to the opposite polarity. This causes the charging current polarity to reverse so the capacitor begins to discharge (or charge). The TL084's two output levels are the positive and negative saturation limits, about  $+13.5$  and  $-13.5$  volts. The two switching thresholds are the levels at which the voltage difference between the two amplifier inputs is zero. Since the amplifier's + input is connected to the midpoint of the  $48 \text{ k}\Omega$  resistive voltage divider, the switching thresholds are  $+6.25$  and  $-6.25$  volts.

The oscillator period is  $2.2R_8C_{14}$ , which is  $52.8 \mu\text{s}$ , so the frequency is about 18.9 kHz.

The + input connected to the voltage divider experiences positive feedback, which adds hysteresis to the switching thresholds. This prevents spurious noise-induced switching that might otherwise occur when the differential voltage between the inputs is very small. Low level noise is always present in virtually any analog circuit.

The voltage on the TL084 inputs are  $\pm 6.5$  volts above or below ground. This could be a problem in a conventional operational amplifier. The TL084 has JFET-inputs and is capable of operating with a differential input voltage of  $\pm 30$  volts and an input voltage of  $\pm 15$  volts. Section 4 has a data sheet for the TL084.

The oscillator output is clipped to a  $\pm 6.2$  volt square wave by a zener diode clipping circuit. R79, a  $2 \text{ k}\Omega$  resistor, isolates the amplifier from the clipper to prevent clipper overload. A pair of paralleled 1N821, 6.2 volt zener diodes make a precise + and - 6.2 volt square wave that is nearly independent of temperature. The 1N821 has a temperature coefficient of  $0.01 \%/^\circ\text{C}$ . The 1N823, which may be used as an alternate zener, has the same zener voltage but a  $0.005\%/^\circ\text{C}$  temperature coefficient.

Since there are two vacuum sensors, two independent sets of DV-R6 drivers and conditioning amplifiers are required. The driver circuits are power buffers and the conditioning amplifiers are a differential amplifier driving an inverting amplifier. The Hastings catalog does not specify a resistance value for the thermopile but it's reasonable to assume that it is small, probably less than an ohm. This low resistance requires a low impedance, high current drive.

We first consider the VD power buffer, driven by the clipper circuit described above. The power buffer is U8-1, an inverting operational amplifier with Q1, an emitter-follower power transistor in the feedback loop. The transistor provides the low impedance, high current drive required by the DV-6R.

The DV-6R must be driven by an AC signal. Therefore, the buffer amplifier input and output are both AC-coupled. The input is AC-coupled via  $C_1$  ( $0.01 \mu\text{F}$ ). At 18.9 kHz,  $C_1$ 's impedance is about  $800 \Omega$ , small in comparison to  $R_7$  ( $130 \text{ k}\Omega$ ) and  $R_3$  ( $50 \text{ k}\Omega$ ). The amplifier output drive to the DV-6R is AC-coupled via  $C_2$ ,  $10 \mu\text{F}$ .  $C_2$ 's impedance is about  $0.8 \Omega$ , small in comparison to the DV-6R impedance.

Note that Q1's collector is connected to ground; a  $0.3 \text{ mA}$  offset current from +10 volts into U8-2, the summing junction, shifts Q1's emitter Q-point to about -3.0 volts. This avoids clipping the DV-6R drive. Diode CR<sub>5</sub> across the transistor base-emitter junction prevents base-emitter reverse voltage protection.

The amplifier gain is controlled by the ratio of feedback to input resistance. The feedback resistor is  $R_1$ , ( $10 \text{ k}\Omega$ ) and the input resistance is  $R_7$  ( $130 \text{ k}\Omega$ ), and  $R_3$ , (a  $50 \text{ k}\Omega$  pot). The maximum and minimum gains are 0.076 and 0.055, respectively as a function of  $R_3$ 's setting. The clipper output is a 12.4 volt, P-P signal; with these two gain extremes, the corresponding Q1 output is about 0.95 volts P-P, and 0.69 volts, P-P. With  $R_3$  set mid-range, the buffer output is about 0.79 volts P-P. Hastings uses a 0.38 volt drive across pins 5 and 3.

The drive is AC-coupled to the DV-6R pin 5 and the thermopile heating current flows through the two thermocouples to ground via DV-6R pin 3. The  $100 \text{ pF}$  capacitor across the  $10 \text{ k}\Omega$  feedback resistor  $R_9$ , provides some high frequency pre-emphasis.

The DV-6R pin 7 output is amplified by cascaded amplifiers, U5-13 (noninverting) and U6-6 (inverting). The DV-6R thermal EMF output on pins 5 and 7 is a DC output that is connected to the inputs of differential amplifier U6-13. Note from Figure 2 that the two heated thermocouple's thermal EMFs are in opposition, thus pin 5 is actually at DC ground; this was verified in a recent measurement.

The DV-6R's negative polarity, thermal EMF output on pin 7, drives U5-4, the amplifier's noninverting (+) input. Since the noninverting input is driven and the noninverting input is static at DC ground, the amplifier's output signal polarity is the same as the DV-6R pin 7 polarity.

Note that the DV-6R AC excitation is also a normal-mode input to U5-13. The AC level on DV-6R pin 7 is half the AC excitation voltage. The normal-mode component is reduced by resistor  $R_{86}$  so that the AC level on U5-3 is also half the excitation level. The normal-mode component of the AC excitation is also reduced by the two amplifier's low-pass filtering.

U5-13's gain is 50, determined by the  $R_9/R_{85}$  ratio. The 19.8 kHz AC signal on U5-13's inputs is filtered by capacitor  $C_4$  across U5-13's feedback path. This capacitor in conjunction with  $R_{84}$  forms a single-pole, low-pass filter having a -3 dB frequency of about 3 Hz. Inverting amplifier U5-6 has a gain of 10, and capacitor  $C_8$  provides additional AC filtering. U5-6's -3dB frequency is about 32 Hz.

When the pressure is 1  $\mu\text{m}$ , the U5-13's output is - 8.050 volts ( $50 \times -0.161$ ). When the air pressure is high, U5-13's output is very small.

The next amplifier stage, U5-6, is an inverting amplifier with a gain of 10. Note that the + input of U5-6 is biased to about +1 volt by the resistive voltage divider to +10 volts. This also causes the - input to be biased to the same +1 volt level. If the U5-13 output is about zero volts, which is the atmospheric pressure level output of the DV-6R, the U5-6 output is +10 volts. If the U5-13 output is - 8.050 volts, the result of a 1  $\mu\text{m}$  pressure in the DV-6R, the U5-6 output is zero volts.

The VD amplifier output may be measured at TJ-5; TJ7 is analog ground. The amplifier's three outputs (MON OUT, METER, and VD) have isolation resistors  $R_{16}$  (2 k $\Omega$ ),  $R_{17}$  (10 k $\Omega$ ) and  $R_{18}$  (100  $\Omega$ ), respectively. The METER OUT signal could be used to drive an analog meter but is not used in F104. The MON OUT is also not used in F104. The VD output is connected to the Control Card (slot 7), the Monitor Card (slot 3), and to J2-2 for readout by the Monitor and Control System.

The VP power buffer (U8-14 and Q2) is similar to the VD power buffer but provides a slightly lower drive for its DV-6R;  $R_7$  in the series attenuator is 200 k $\Omega$ . The maximum and minimum drives as a function of the  $R_7$  setting are 0.49 and 0.30 volts, P-P respectively. With  $R_{21}$  set mid-range, the AC drive is 0.40 volts, P-P, close to Hastings drive level.

## Vacuum Sensor Interface Circuit Alignment

This alignment procedure was abstracted from VLBA Technical Report No. 1.

The two DV-6R interface circuits are aligned by using a Sensor Card Tester. The tester contains a Hastings DB-20 Reference Tube, which simulates the output of a DV-6R at a specified vacuum level, typically 2 to 3  $\mu\text{m}$ , printed on the side of the Reference Tube. The vacuum interface circuitry in the tester has a VD/VP selector switch to connect the DB-20 to either interface circuit and a ZERO/ATMOS toggle switch for the two adjustments. The DV-6R interface circuits have two alignment adjustments, VP

ZERO (or VD ZERO) and VP ATMOS (or VD ATMOS). The VP ZERO adjustment determines the AC drive level to the buffer circuit and the VP ATMOS adjustment determines the DC offset to the U6-6 (or U5-6) output amplifiers. In aligning the card's two DV-6R interface circuits, the tester's ZERO/ATMOS switch is first set to the ZERO position and the card's VP (or VD) ZERO potentiometer is adjusted to produce an output of 161 mV times the DB-20 reference pressure value. The output can be measured at TJ6 (or TJ5) on the tester on the EXT DVM jack or by the Monitor Panel DVM. Next, the ZERO/ATMOS is set to the ATMOS position and the VP (or VD) ATMOS potentiometer is adjusted to produce an output of +10230 mV (about positive full-scale on a 5 mV/LSB, 12-bit A/D converter). In the ATMOS position, the tester presents an open circuit to the interface circuit in place of the DV-6R; this causes the full-scale output. Section 4 contains a Hastings DB-20 data sheet. A field calibration procedure for the DV-6R vacuum sensors is included in the Appendix, Section 5.

### DT-500 Temperature Sense Diodes, TSA and TSB

The temperatures of the dewar 15 °K and 50 °K stations is sensed by two Lake Shore DT-500-KL diode temperature sensors, TSA and TSB. The 15 °K stage conditioned signal is TA and TB is the 50 °K stage conditioned signal. Section 4 contains a data sheet for a similar Lake Shore diode temperature sensor. The 300 °K temperature is measured by a National Semiconductor LM335 chip and is described in the RF Card description, Section 2.9, below. Figure 3, on the next page, shows a plot of the DT-500 diode voltage vs. temperature. This plot was abstracted from NRAO EDIR Report No. 204, May 1980 by Michael Balister.

The diode's characteristics are determined by the diode equation:  $I_F = I_S (e^{\frac{qV}{kT}} - 1)$ .  $I_F$  is the diode forward current and  $I_S$  is the reverse-bias saturation current. Constants are:  $I_S$ ,  $e$ , the electronic charge, and  $k$ , Boltzman's constant. Variables are  $I_F$ ,  $V$ , the diode voltage, and  $T$ , the diode temperature, °K. If  $I_F$  is maintained at a constant value, there are only two variables,  $V$  and  $T$ . By using a suitable conversion table and holding  $I_F$  at a constant value,  $T$  may be determined by measuring  $V$ . Note from the Lake Shore data sheets that if  $I_F$  is 10  $\mu$ A,  $V$  is 1.345 volts at 13 °K and 0.519 volts at 300 °K.

### Diode Interface Circuitry

Block Diagram C53204K002 shows the TSA and TSB diode wiring connections to the Sensor Card, which has two identical temperature interface circuits. The diode anodes are connected to analog ground (pins E and F) and the cathodes are connected to the current sources and temperature sense interface circuit inputs (pins 4 and H). The TA and TB diode interface circuits are shown in the right half of Schematic diagram D53200S002.

Implementation of a two-segment linearization circuit is suggested by the character of the DT-500 thermal response curve shown in Figure 3. The Sensor Card's diode interface circuitry is an adaptation of the design described in EDIR No. 204. <sup>1</sup>

Consider the TA circuit. Transistor Q3 and associated components are the 10  $\mu$ A current sources for TSA. The base of Q3 is held at -8.8 volts by zenar diode CR<sub>1</sub> ( $V_Z = 6.2$  volts). Q3's collector current is determined by  $V_{CE}$  and the resistance between the emitter and -15 volts. Potentiometer R<sub>39</sub> adjusts the

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<sup>1</sup> Page 37, VLBA TECHNICAL REPORT NO. 1, August 29, 1984

diode current to the 10  $\mu$ A value.

Noninverting, unity-gain voltage followers U1-1 and U2-1 isolate the diode's current source circuitry from the linearization circuitry. Since they simply buffer the diode's voltage, the amplifier's outputs are a nonlinear function of temperature. The TSA signal is connected to its linearization circuitry and to J2-14 for readout by the Monitor and Control System. R<sub>87</sub>, a 1 k $\Omega$  resistor, isolates the TA amplifier from the test point terminal TP1 and the nonlinear TA output on pin S. The nonlinear form of TA is not used by the Control Card and is not available to the Monitor Card DVM. The nonlinear TSB signal is only used by the TB linearization circuitry.

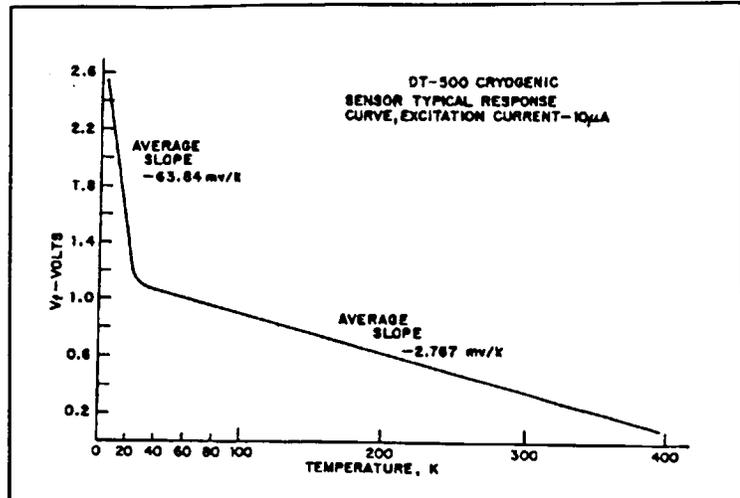


Figure 3 DT-500 Sensor Temperature Response

Note from the Lake Shore data sheets in Section 4 that at 13  $^{\circ}$ K, the nonlinear TA signal has a sensitivity (slope) of 21.9 mV/ $^{\circ}$ K. The sensitivity decreases to 15.9 mV/ $^{\circ}$ K at 24  $^{\circ}$ K. In this 11 degree region, the nonlinear TSA signal is more sensitive than the linearized TA and TB signals, which have a sensitivity of 10 mV/ $^{\circ}$ K. In addition, in this region the nonlinear TA is more accurate than the linearized TA because the linearized signals are segmented approximations to the diode curve.

The TA and TB linearization circuitry approximates the diode's V versus T curve with two straight-line segment approximations, only one of which is operative at any given time. When the sensed temperature changes from one segment's range to the other segment's range, it crosses a segment transition temperature which causes the other segment's output signal to be selected for output. The segment amplifier's gains and offsets are adjusted for the best fit for its portion of the diode's V-T curve. The segment transition temperature is 27  $^{\circ}$ K. The linearized TA and TB signals can be adjusted to be in exact agreement with the diode V-T curves at 13, 18, 50 and 300  $^{\circ}$ K. Since TSB monitors the 50  $^{\circ}$ K stage, the lower temperature segment is never operative.

The linearization implementation consists of two independent segment gain paths with gain and offset adjustments appropriate for the segment, a segment signal level comparator, and a segment selector switch driven by the comparator.

The TA and TB linearization circuits are identical.

In each circuit both paths are driven by the input, unity-gain voltage follower, U1-1 or U2-1. The circuitry consists of two parallel-path independent, inverting operational amplifiers with different gains, an analog comparator that compares the two amplifier's outputs, an analog switch driven by the comparator that selects the most appropriate amplifier for output, and an inverting output amplifier.

Note from the schematic that one TA path is a HI GAIN path used for the higher temperature segment and the other path is the LO GAIN path used for the lower temperature segment. From the

paragraph above describing the nonlinear TA signal, note that in the 13 to 24°K range, the diode's sensitivity is greater than 10 mV/°K so the lower segment amplifier's gain must be less than 1. Also note that for temperatures greater than 25 degrees, the upper segment amplifier's gain must be greater than 1. 20 kΩ gain control potentiometers R<sub>43</sub> and R<sub>44</sub> control the gain of the two TA amplifiers U1-7 and U1-8. For extreme settings of these two potentiometers, the resultant gains are: 4.02 and 3.29, HI GAIN and 0.21 and 0.16, LO GAIN.

Both amplifiers use an offset current from an Analog Devices, AD581JH precision +10.000 reference voltage source. This chip was described in the Control Card description, Section 2.5. Potentiometers R<sub>40</sub> and R<sub>47</sub>, 100 kΩ, and 50 kΩ, respectively, are the offset current adjustments.

Comparator U3-1, a National Semiconductor LM393AN, compares the levels of the high and low gain amplifiers. If the HI GAIN level on the negative input (-) is more positive than the LO GAIN positive input (+), the output is low. In the converse case, the output is high. The comparator output is an open-collector transistor; a 22 kΩ pull-up resistor to +15 makes the output levels 0 and +15 volts. The LM393 features a very low input offset, typically 1 mV, important in this application.

U4 is an Analog Devices AD7512DIKN, dual-channel analog switch that selects either the HI GAIN signal or the LO GAIN signal as a function of the address (select control) input, pin 4. If pin 4 is high, the HI GAIN amplifier input on pin 9 is connected to the output, pin 10; if low, the LO GAIN signal on pin 11 is connected to the output. R<sub>74</sub> provides isolation from the comparator for the control input and diode CR4 protects it in the event of a negative control input. The AD7512 features a low "ON" resistance, 75 Ω, and low leakage currents. Section 4 contains an AD7512DI data sheet.

Unity-gain, inverting amplifier U1-14 provides output buffering for the TA output on card pin D. R<sub>56</sub>, a 100 Ω resistor, provides short-circuit protection for this output. The EXT MON output on pin 6 is not used in F104.

0.47 μF Capacitors across the operational amplifiers provide low-frequency filtering of the temperature signals.

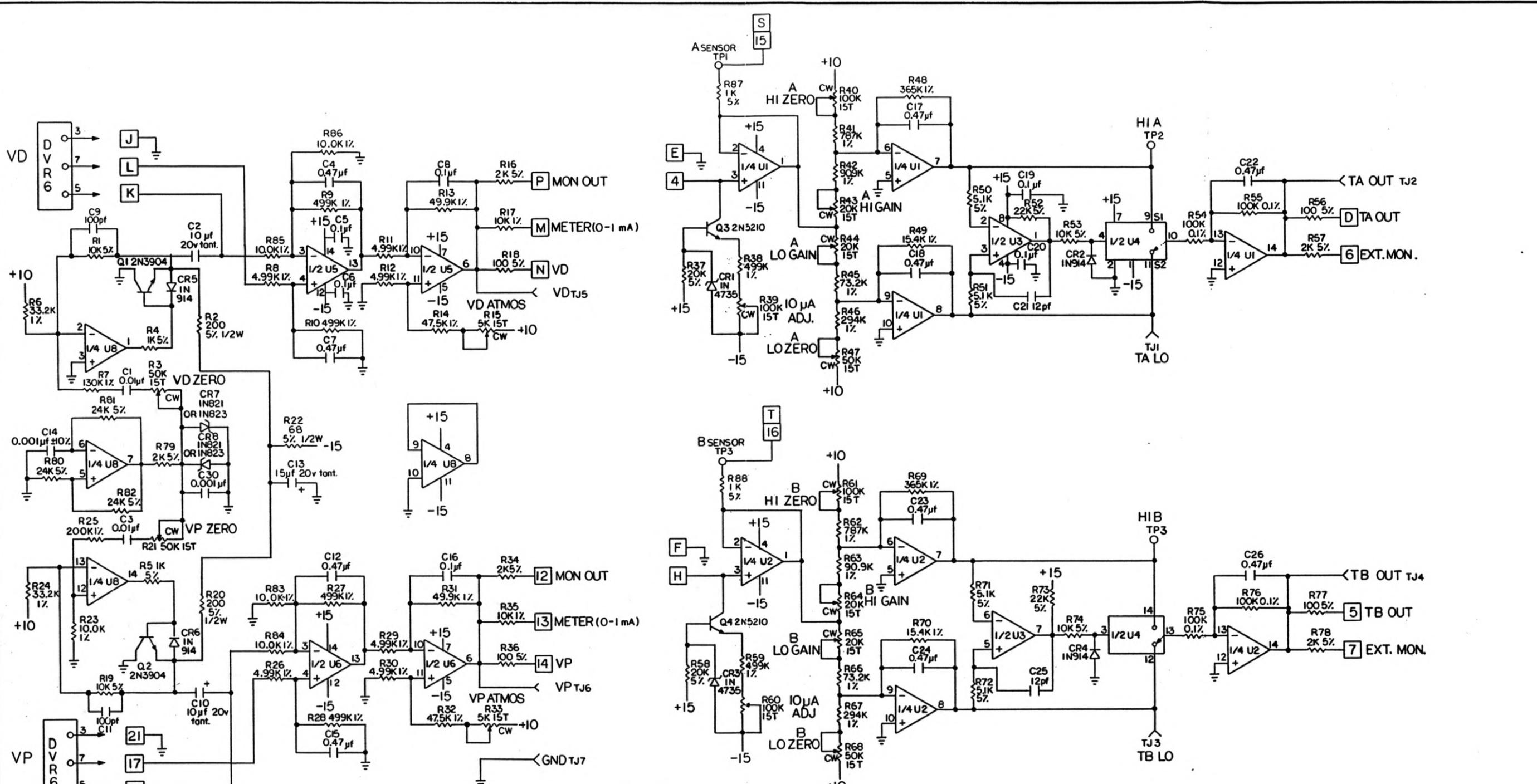
TJ1 and TJ3 enable measurement of the LO GAIN amplifier outputs and TJ2 and TJ4 enable measurement of the TA and TB outputs, respectively. TP2 and TP3 terminals enable measurement of the HI GAIN amplifier's outputs.

The Sensor Card Tester uses potentiometers and a buffer amplifier simulates the diode temperature sensors. Using this tester, the TA and TB interface circuits are aligned as follows:

1. Set the DVM switch to TA.
2. Set the Mode switch to A-10 μA and adjust the A-10 μA potentiometer for a reading of 1000 on the DVM.
3. Set the MODE switch to TA/TB and the TEMP switch to SHORT and adjust the TA HI GAIN potentiometer for 4350 mV on the DVM. Adjust the TA LO GAIN potentiometer for 445 mV, on the A LO GAIN test terminal, read by an external DVM.
4. Set the TEMP switch at 50 and adjust the TA HI GAIN potentiometer for 500 mV on the tester DVM.
5. Set the TEMP switch at 300 and readjust the TA HI GAIN potentiometer for a reading of 3000 mV on the tester DVM. Repeat steps 4 and 5 until 500 mV and 3000 mV readings are

obtained.

6. Set the TEMP switch at 13 and adjust the TA LO GAIN potentiometer for 130 mV on the tester DVM.
7. Set the TEMP switch at 18 and readjust the TA LO GAIN potentiometer for 180 mV on the tester DVM. Repeat steps 6 and 7 until 130 mV and 180 mV readings are obtained.
8. Repeat steps 1 through 7 for the TB circuit.

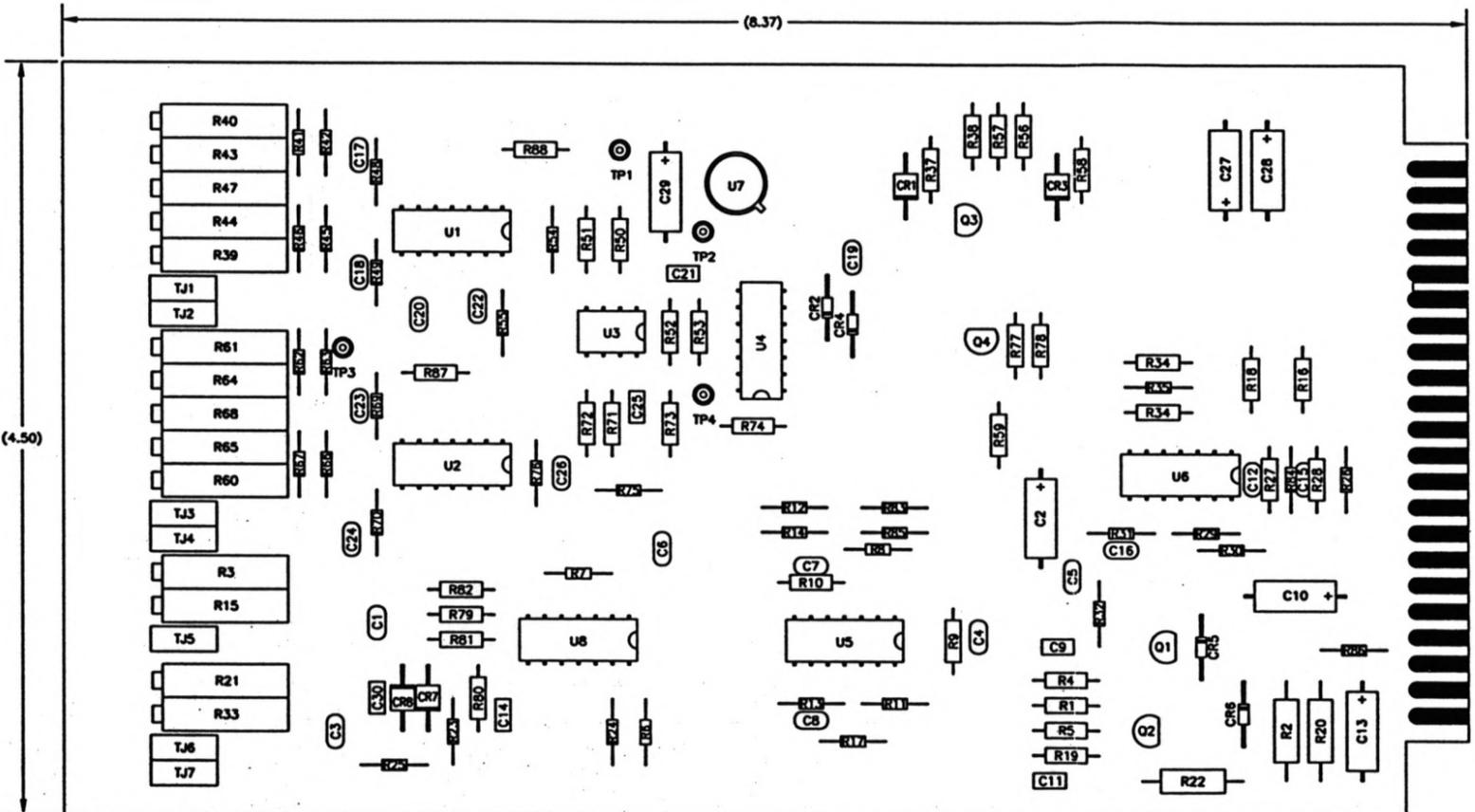


- NOTES**
1. U1,U2,U8-TL084BCN
  2. U3-LM393AN
  3. U4-AD752DIKN
  4. U5-U6-OPIOCY
  5. U7-AD581JH
  6. ALL CAPS. ARE 50V UNLESS NOTED OTHERWISE.
  7. ALL RES. AS FOLLOWS UNLESS NOTED OTHERWISE.  
1% 1/8 WATT  
5% 1/4 WATT

C	11-84	G. MOERIS		CO-860130-07
B	11-85	G. MOERIS		
A	8/84	H. DILL		CO-840817-20
REV	DATE	DRAWN BY	APPR'D BY	DESCRIPTION
V				FRONT ENDS
SENSOR CARD				NATIONAL RADIO ASTRONOMY OBSERVATORY CHARLOTTESVILLE, VA. 22901
DRAWN BY H. DILL		DATE 8/07/84	REV. C	
DESIGNED BY S. WEINREB		DATE 8/06/84	SCALE	
APPROVED BY		DATE		
SHEET 1 of 1		DRAWING NUMBER 053200S002	REV. C	



REV	DATE	DRAWN BY	APPRVD BY	DESCRIPTION
B	1-87	WIREMAN		ADD TEMP SENSOR HOLES
C	2-87	MORRIS		CHG ORDER 870218-5
D	8-94	TATE	PETENCIN	REVISED AND REDRAWN



COMPONENT SIDE

57	U3	AUGAT	608-CG1	SOCKET, 8-PIN	1
56	U1, U2	AUGAT	614-CG1	SOCKET, 14-PIN	7
55	U7	ADI	AD581JH	IC, 14-PIN	1
54	U5, U6	PMI	OP10CY	IC, 14-PIN	2
53	U4	ADI	AD7512DIKN	IC, 14-PIN	1
52	U3	MOTOROLA	LM393N	IC, 8-PIN	1
51	U1, U2, U3	TI	TL084CN	IC, 14-PIN	3
50	TF-TP4	KEYSTONE	1562-2	TURRET, TEST POINT	4
49	TJ7			TEST JACK, BLACK	1
48	TJ6			TEST JACK, GREEN	1
47	TJ5			TEST JACK, GRAY	1
46	TJ3			TEST JACK, ORANGE	1
45	TJ2			TEST JACK, RED	1
44	TJ1, TJ3			TEST JACK, WHITE	2
43	R80-R82	ALLEN-BRADLEY	RC07GF243J	RESISTOR, 24K, 1/4W, 5%	3
42	R51, R52	DALE	RN55C1003F	RESISTOR, 100K, 1/8W, 1%	4
41	R52, R73	ALLEN-BRADLEY	RC07GF223J	RESISTOR, 22K, 1/4W, 5%	2
40	R53, R74	ALLEN-BRADLEY	RC07GH512J	RESISTOR, 5.1K, 1/4W, 5%	4
39	R49, R70	DALE	RN55C1542F	RESISTOR, 15.4K, 1/8W, 2%	2
38	R48, R69	DALE	RN55C3653F	RESISTOR, 356K, 1/8W, 1%	2
37	R46, R67	DALE	RN55C2943F	RESISTOR, 294K, 1/8W, 1%	2
36	R45, R66	DALE	RN55C7322F	RESISTOR, 73.2, 1/8W, 1%	2
35	R43, R44	CEMET	3006P 20K	TRIM POT, 20K, 15T	4
34	R42, R63	DALE	RN55C9092F	RESISTOR, 90.9K, 1/8W, 1%	2
33	R41, R62	DALE	RN55C7873F	RESISTOR, 787K, 1/8W, 1%	2
32	R39, R40	CEMET	3006P 100K	TRIM POT, 100K, 15T	4
31	R37, R58	ALLEN-BRADLEY	RC07GF203K	RESISTOR, 20K, 1/4W, 5%	2
30	R25	DALE	RN55C2003F	RESISTOR, 200K, 1/8W, 1%	1
29	R22	ALLEN-BRADLEY	RC20GF680J	RESISTOR, 68, 1/2, 5%	1
28	R18, R36	ALLEN-BRADLEY	RC07GF101J	RESISTOR, 100, 1/4W, 5%	4
27	R17, R35, R36	DALE	RN55C1002F	RESISTOR, 10K, 1/8W, 1%	7
26	R16, R34, R37	ALLEN-BRADLEY	RC07GF202J	RESISTOR, 2K, 1/4W, 5%	5
25	R15, R33	CEMET	3006P 5K	TRIM POT, 5K, 15T	2
24	R14, R32	DALE	RN55C4752F	RESISTOR, 47.5K, 1/8W, 1%	2
23	R13, R31	DALE	RN55C4992F	RESISTOR, 49.9K, 1/8W, 1%	2
22	R12, R30	DALE	RN60D4993F	RESISTOR, 499K, 1/4W, 1%	6
21	R11, R29, R30	DALE	RN55C4991F	RESISTOR, 4.99K, 1/8W, 1%	6
20	R7	DALE	RN55C1303F	RESISTOR, 130K, 1/8W, 1%	1
19	R6, R24	DALE	RN55C3322F	RESISTOR, 3.3K, 1/8W, 1%	2
18	R5, R23	ALLEN-BRADLEY	RC07GF102J	RESISTOR, 1K, 1/4W, 5%	4
17	R4, R22	CEMET	3006P 50K	TRIM POT, 50K, 15T	4
16	R2, R20	ALLEN-BRADLEY	RC20GF201J	RESISTOR, 200, 1/2W, 5%	2
15	R19, R18	ALLEN-BRADLEY	RC07GF103J	RESISTOR, 10K, 1/4W, 5%	4
14	Q3, Q4	MOTOROLA	2N5210	TRANSISTOR, NPN	2
13	Q1, Q2	MOTOROLA	2N3904	TRANSISTOR, NPN	2
12	CR7, CR8	AMD	1N821	DIODE	2
11	CR2, CR6	AMD	1N914	DIODE	4
10	CR1, CR3	MOTOROLA	1N4735	DIODE	2
9	C21, C25	KEMET	CK05BX120K	CAPACITOR, 12pf, 50V	2
8	C14, C30	KEMET	CK05BX102K	CAPACITOR, .001uf, 50V	2
7	C13, C27-C29	MALLORY	CSR13E156KP	CAPACITOR, TANT., 15uf, 20V	4
6	C9, C11	KEMET	CK05BX101K	CAPACITOR, 100pf, 50V	2
5	C5, C8, C20	KEMET	C330C104M5U5CA	CAPACITOR, .1uf, 50V	6
4	C16, C18, C22	KEMET	C330C474M5U5CA	CAPACITOR, .47uf, 50V	10
3	C2, C10	MALLORY	CSR13E106KP	CAPACITOR, TANT., 10uf, 20V	2
2	C1, C3	KEMET	C330C103M5U5CA	CAPACITOR, .01uf, 50V	2
1		NRAO	D532000002	BOARD, CIRCUIT	1

ITEM NO.	REF.	DES.	MANUFACTURER	PART NUMBER	DESCRIPTION	QTY
UNLESS OTHERWISE SPECIFIED DIMENSIONS ARE IN INCHES						
MATERIAL :						
FINISH :						
NEXT ASSEMBLY DWG. TYPE						
COMMON FRONT END			NATIONAL RADIO ASTRONOMY OBSERVATORY SOCORRO, NEW MEXICO 87801			
FRONT END SENSOR PCB ASSEMBLY			DRAWN BY H. DILL DATE 9-85			
			DESIGNED BY S. WENREB DATE 9-85			
			APPROVED BY S. WENREB DATE 9-85			
SHEET NUMBER 1 of 1		DRAWING NUMBER D53200A003		REV. D		SCALE 2/1

ACAD : 53200A03

D53200S002	SCHEMATIC
D53200A002	ARTWORK
D53200P002	DRILL DWG
D53200I013	SILKSCREEN
D53200I007	SOLDER MASK
NEXT ASSEMBLY	DWG. TYPE



## 2.8 Bias Card Description

The dewar RCP and LCP amplifiers each use three HEMT (high electron mobility transistor) GASFET amplifiers. The amplifier's RF gain and noise performance can be optimized by providing each HEMT stage an empirically-determined, optimum pair of DC drain voltage and DC drain current values. The amplifier stages are AC-coupled; therefore, each stage can have a distinct DC drain voltage and current. The FET Bias Card performs two functions: 1) it provides the optimal HEMT drain voltages and 2) it controls the gate voltages to maintain the optimal drain currents.

During the test phase of F104 fabrication, optimum VD and ID values at both 15 °K and 300 °K temperatures are determined. These values and the resultant VG are recorded on an amplifier data sheet for future reference. Sheet 4, Appendix I, TR 10, is a copy of the F104, dewar S/N 01 data sheet. These data sheets are maintained in the AOC Front-End Laboratory file and the VG values are entered into the VLA and VLBA Data Checker programs for fault monitoring. In order to permit replacement of FET Bias Cards without adjustment, all new or spare cards are adjusted to produce a VD of +3 volts and an ID of 1 mA; these values should enable the HEMT to function until the optimum settings are determined.

Each FET Bias Card contains four identical sets of bias control circuits. Since the F104 uses three HEMTs in each channel, two FET Bias Cards are used, one card for each channel. The RCP bias card is installed in slot 4 and the LCP bias card is installed in slot 5. Each card has an unused bias circuit that is wired to the dewar DC Feedthrough panel for potential future use. The spare bias circuit is thus immediately available in the event that a future dewar amplifier requires a fourth HEMT stage. Dewar ground is the return for these sixteen signals. Block Diagram C53204K002 shows the Bias Card-Dewar wiring connections and D53200S001 is the Bias Card Schematic. D53200A002 is the Bias Card assembly drawing.

Each bias circuit has a HEMT drain voltage (VD) and drain current (ID), adjustment potentiometer accessible on the edge of the card. HEMT sources are connected to dewar ground.

All four VD voltages can be measured on card-edge test jacks but cannot be measured by the DVM or the Monitor and Control System.

All four drain currents (ID) can be measured as voltages on card-edge test jacks. The ID voltage scaling factor is 1 mA/100 mV. The drain currents cannot be measured by the DVM or by the Monitor and Control System.

All four gate voltages (VG) can be measured on card-edge test jacks. The first stage VG can also be measured by the Monitor Card DVM (with the selector switch S2 in the LF1 and RF1 positions) and by the Monitor and Control System via J2-7 (RF1 signal) and J2-9 (LF1 signal). Second and third stage VG voltages cannot be individually measured by the DVM or Monitor and Control System but a composite form of these two VG signals can be measured. Note that the block diagram shows that the stage 2 and 3 VG monitor signals on pins 5 and 6 are connected together and to the DVM selector switch S2. This connection sums the two signals and the composite signal level is intermediate between the VG2 and VG3 levels. The DVM measures the composite VG signals in selector switch positions LF2 and RF2. These two composite VG signals are also connected to J2-8 (RF2) and J2-10 (LF2) for readout by the Monitor and Control System. Since the composite VG readout level is the sum of the stage 2 and stage 3 VG levels, its level will differ from the actual VG2 and VG3 levels and its level will be approximately

intermediate between the two. It is important to remember this VG monitoring configuration when comparing the amplifier S/N data sheet VG2 and VG3 values (e.g., TR 10, Appendix I, Sheet 4 example values) with the composite VG values read out as RF2 and LF2.

The normal range of VG is between 0 and -1 volts and is a function of temperature with a typical change of 100 to 300 mV from 300 °K to 15 °K. At 15 °K the VG value should be within  $\pm 20$  mV of the data sheet value. An open in the drain circuit will force the measured VG to the VG bias amplifier's positive limit, about +13.5 volts. In this condition, the forward gate current is limited to about 7 mA by a series resistor. A short in the drain or gate circuit (perhaps the result of insulation cold-flow on a dewar wire) will force the measured VG to the amplifier's negative limit, about -13.5 volts. In this condition, the actual HEMT gate voltage is limited to about -5 volts by the 1N821 protection diode.

Consider the first FET bias stage in the upper left quarter of D53200S001. Mentally picture the associated HEMT stage with the source connected to DC (dewar) ground, the gate connected to pin H (VG), and the drain connected to pin N (VD). Also assume that both the gate RF input and drain RF output are AC-coupled.

The bias circuit consists of a set of four interconnected operational amplifiers U1 (a TL084BCN quad operational amplifier) and a transistor Q1 (2N2219). The circuit description can be simplified if it is considered to consist of three sub-circuits: a VD driver circuit (U1-1, Q1 and U1-14), an ID sense circuit (U1-8), and a VG driver circuit (U1-7). The VD driver and ID sense circuit are described first because the VG driver circuit is a control loop that is dependent upon the outputs of the VD driver and ID sense circuits.

The bias circuit's first function is to set the VD voltage; this is the function of the VD driver, which consists of U1-1 and transistor Q1 (2N2219). This circuit is a voltage follower (noninverting operational amplifier with a gain of 1) with a Q1 emitter follower included in the feedback loop. Potentiometer  $R_{14}$  is the VD set point adjustment and provides a DC bias to U1-2, the + input. Since Q1 is inside the follower loop, U1's output is Q1's  $V_{BE}$  drop above the VD1 set point so the VD level is that set on  $R_{14}$ . Diode CR1 is a protective diode across Q1's emitter-base junction. The diode protects Q1 in the event that the U1-14 output ever swings negative (perhaps due to an accidental short while probing the board with a DVM, etc.). CR2 has a zener voltage of 6.8 volts to protect the HEMT drain in the event of some malfunction or open in the operational amplifier circuit. U1-14 is a voltage follower used to isolate the drain from the VD1 test jack, TJ13. It also drives the ID sense circuit.  $R_1$ , the 2 k $\Omega$  series resistor between U1-14 and the VD1 test jack, protects U1-14 in the event that TJ13 is inadvertently shorted to ground. Finally,  $C_2$ , a 1.0  $\mu$ F capacitor filters the driver circuit's DC bias value to keep the output noise free.

The ID sense circuit consists of U1-14, a voltage follower and U1-8, a differential amplifier. HEMT drain current flows from the +15 volt power source through Q1, through  $R_8$  (200  $\Omega$ ), out pin N to the HEMT drain, and through the HEMT to dewar ground. ID is sensed as a voltage drop across  $R_8$  and amplified by differential amplifier U1-8, which has a gain of 0.5. U1-8 is a differential amplifier because VD1 is a common-mode voltage on both U1-8's inputs. U1-8's output is scaled at 100 mV per mA of ID current. 2 k $\Omega$  resistor  $R_2$  isolates U1-8's output from TJ12 in the event of an inadvertant short to ground.

The second function of the FET bias circuit is to control VG so that ID is a constant, preset value; this is done by the VG drive circuit that closes the loop on ID. The VG driver consists of U1-7 with two

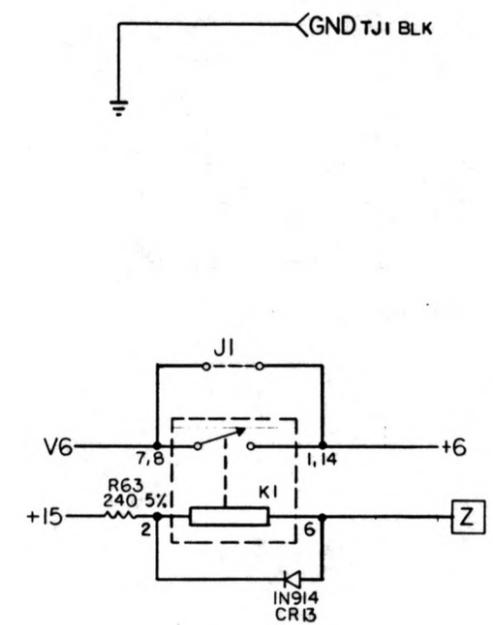
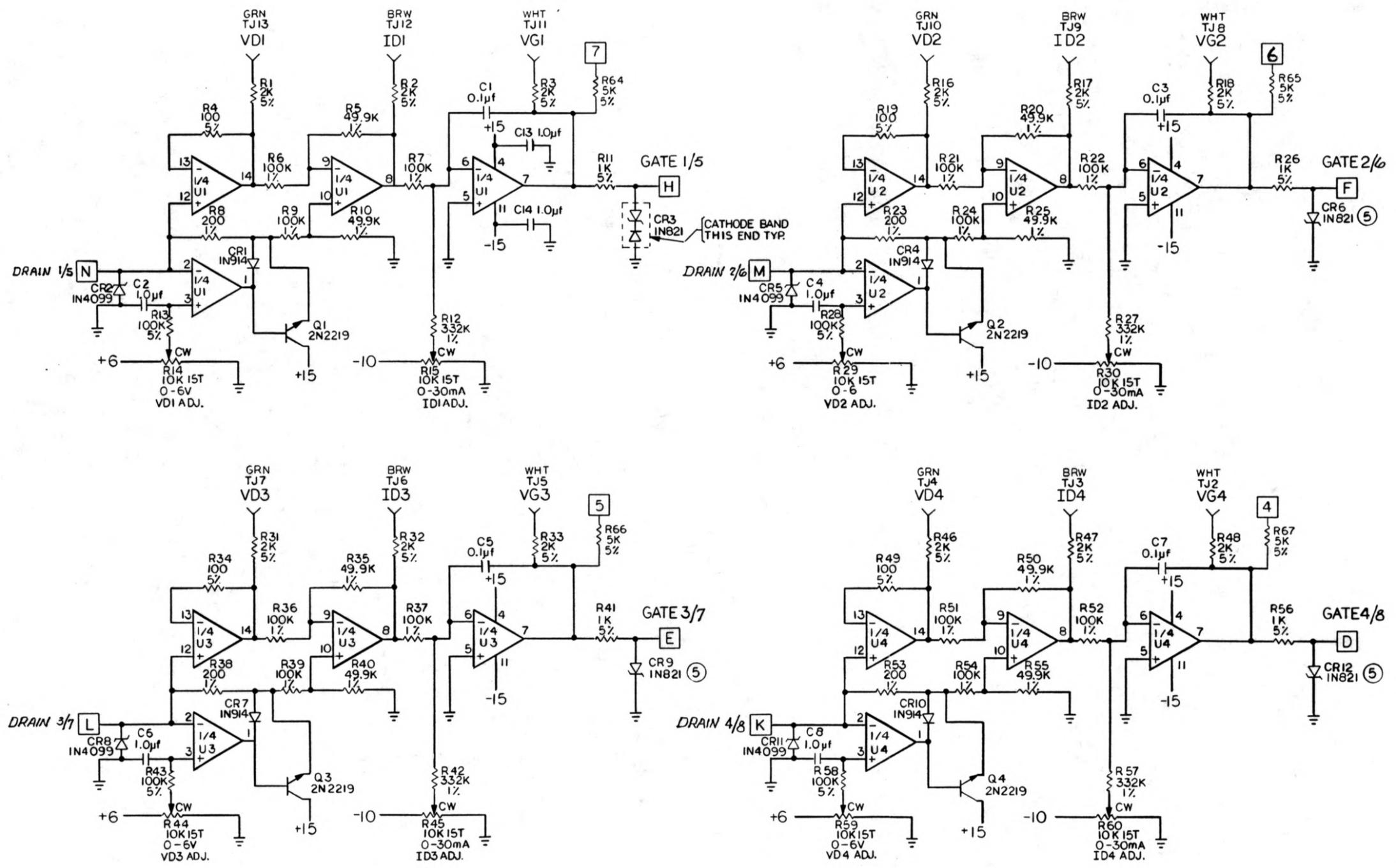
summing junction (U1-6) inputs: 1) a positive ID current input from U1-8 and 2) a negative offset current flowing to R<sub>15</sub>, the ID1 adjustment potentiometer. U1-8's output is a positive voltage that is an analog of ID and is scaled at 100 mV/mA. A current proportional to this voltage is input to the U1-7 summing junction (the - input) via R<sub>7</sub>, 100 k $\Omega$ . When the loop is closed, the ID current into U1-6 is equal to the offset current through R<sub>12</sub>, and the op-amp's output U1-7 is proportional to the offset current through R<sub>12</sub>. Although it's not obvious, the HEMT's drain-source impedance is a factor in the feedback path.

Two DC reference voltages are used by the bias circuits: -10 volts and +6 volts, derived from a pair of AD581JH +10 volt precision reference voltage sources. Four 10 k $\Omega$  VD adjustment pots are connected in parallel and to resistor R<sub>6</sub>, 1.5 k $\Omega$ , which drops four volts to produce the +6 volts for the VD adjustment potentiometers. Data sheets for the AD581JH and TL084BCN are included in Section 4.

The 6 volt relay circuit on the right side of the schematic diagram is not used.

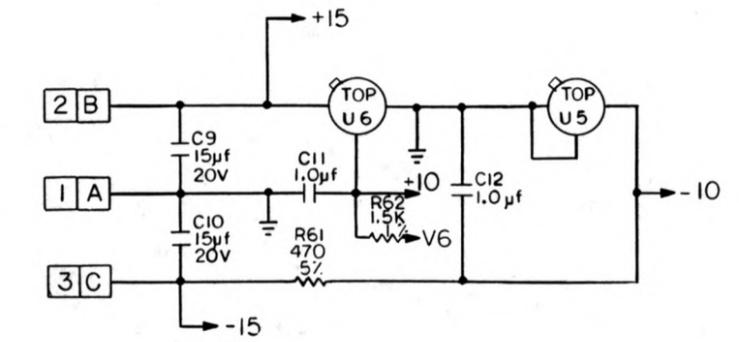
The FET Bias Card is tested on a Bias Card Tester that contains + and - 15 volt power supplies and four FETs with characteristics similar to cooled GASFETs. The card is plugged into the tester and a DVM is plugged into the card's ground (TJ1), VD, ID and VG test jacks. The four sets of VD and ID potentiometers are adjusted to produce a VD of +3 volts, an ID of 1 mA, and VG is measured to verify that it is about -400 mV with these VD and ID values.





REPRESENTS AMPLIFIER STAGES 1 THRU 4  
 DRAIN X/Y REPRESENTS AMPLIFIER STAGES 5 THRU 8

NOTE: 2<sup>ND</sup> BIAS CARD MAY BE REQUIRED FOR AMPLIFIERS HAVING MORE THAN 4 STAGES.

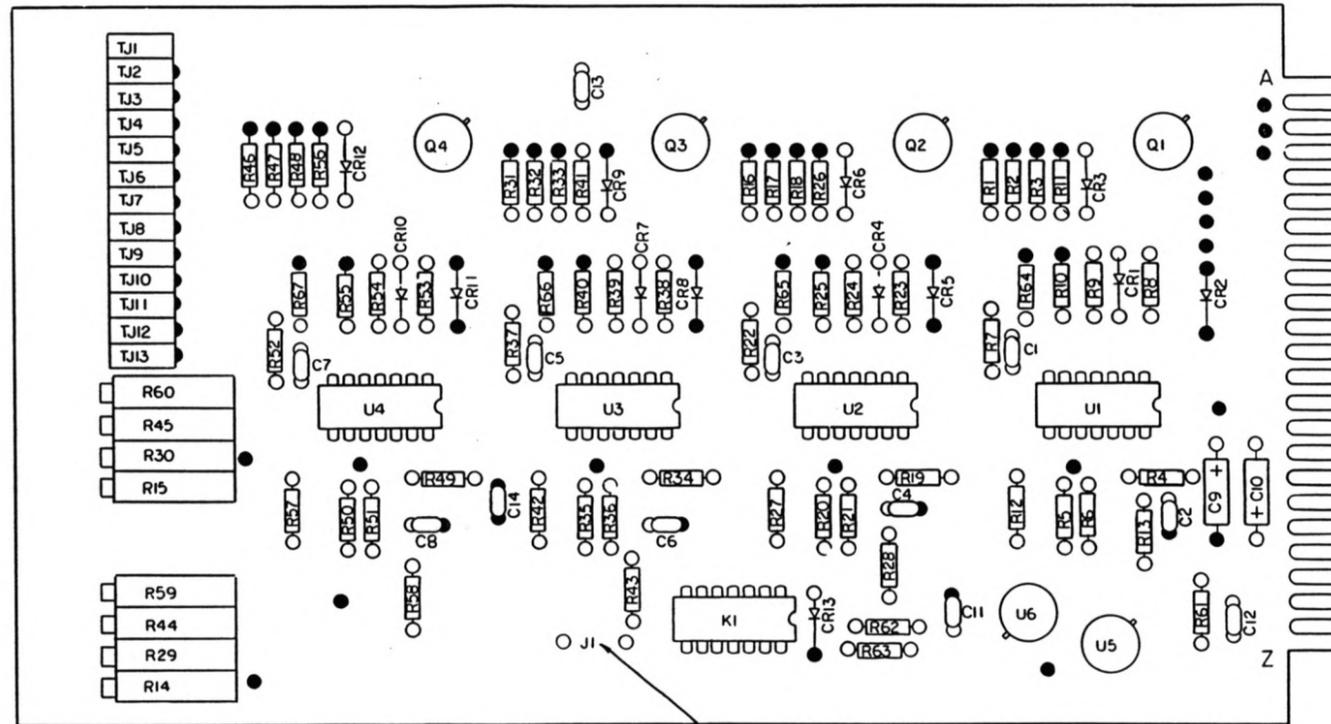


- NOTES
- ① U1-4 TL084BCN
  - ② U5-6 AD581JH
  - ③ ALL CAPS. ARE 50V UNLESS OTHERWISE MARKED.
  - ④ ALL RES. AS FOLLOWS:  
 5% 1/4 WATT  
 1% 1/8 WATT
  - ⑤ SEE CR3 FOR INTERNAL SCHEMATIC.
  - ⑥ KI-MAGNECRAFT W17DIP-14

C	7/87	G. MOERS		CO870218-4
B	8/85	G. MOERS		
A	8/81	H. DILL		CO-810816-21
REV.	DATE	DRAWN BY	APPR'D BY	DESCRIPTION
V				FRONT ENDS
B				NATIONAL RADIO ASTRONOMY OBSERVATORY
A				CHARLOTTESVILLE, VA. 22901
				FET BIAS CARD
				4-STAGE
				DESIGNED BY H. DILL DATE 8-10-70
				DESIGNED BY S. W. HARRIS DATE 8-10-82
				APPROVED BY DATE
				SHEET NUMBER 1 OF DRAWING NUMBER D532005001 REV. D SCALE



REF. DES.	PART DESCRIPTION	PART NUMBER	ITEM#
C 1	CAP. 0.1uf 50v	C330C104M5USCA	5
C 2	CAP. 1.0uf 50v	C330C105M5USCA	6
C 3	CAP. 0.1uf 50v	C330C104M5USCA	5
C 4	CAP. 1.0uf 50v	C330C105M5USCA	6
C 5	CAP. 0.1uf 50v	C330C104M5USCA	5
C 6	CAP. 1.0uf 50v	C330C105M5USCA	6
C 7	CAP. 0.1uf 50v	C330C104M5USCA	5
C 8	CAP. 1.0uf 50v	C330C105M5USCA	6
C 9	CAP. 15uf 20v tant.	CSR13E156KF	7
C 10	CAP. 15uf 20v tant.	CSR13E156KF	7
C 11	CAP. 1.0uf 50v	C330C105M5USCA	6
C 12	CAP. 1.0uf 50v	C330C105M5USCA	6
C 13	CAP. 1.0uf 50v	C330C105M5USCA	6
C 14	CAP. 1.0uf 50v	C330C105M5USCA	6
CR 1	DIODE 1N914	1N914	8
CR 2	DIODE 1N4099	1N4099	9
CR 3	DIODE 1N821	1N821	10
CR 4	DIODE 1N914	1N914	8
CR 5	DIODE 1N4099	1N4099	9
CR 6	DIODE 1N821	1N821	10
CR 7	DIODE 1N914	1N914	8
CR 8	DIODE 1N4099	1N4099	9
CR 9	DIODE 1N821	1N821	10
CR 10	DIODE 1N914	1N914	8
CR 11	DIODE 1N4099	1N4099	9
CR 12	DIODE 1N821	1N821	10
CR 13	DIODE 1N914	1N914	8
K 1	SPST REED RELAY	W171DIP-14	30
Q 1	TRAN. 2N2219	2N2219	24
Q 2	TRAN. 2N2219	2N2219	24
Q 3	TRAN. 2N2219	2N2219	24
Q 4	TRAN. 2N2219	2N2219	24
R 1	RES. 2K 1/4W 5%	RC07GF202J	18
R 2	RES. 2K 1/4W 5%	RC07GF202J	18
R 3	RES. 2K 1/4W 5%	RC07GF202J	18
R 4	RES. 100 1/4W 5%	RC07GF101J	13
R 5	RES. 49.9K 1/8W 1%	RN55C4992F	19
R 6	RES. 100K 1/8W 1%	RN55C1003F	20
R 7	RES. 100K 1/8W 1%	RN55C1003F	20
R 8	RES. 200 1/8W 1%	RN55C2000F	14
R 9	RES. 100K 1/8W 1%	RN55C1003F	20
R 10	RES. 49.9K 1/8W 1%	RN55C4992F	19
R 11	RES. 1K 1/4W 5%	RC07GF102J	15
R 12	RES. 33K 1/8W 1%	RN55C3323F	22
R 13	RES. 100K 1/4W 5%	RC07GF104J	21
R 14	TRIM POT 10K 15T	CERMET 3006P 10K	23
R 15	TRIM POT 10K 15T	CERMET 3006P 10K	23
R 16	RES. 2K 1/4W 5%	RC07GF202J	18
R 17	RES. 2K 1/4W 5%	RC07GF202J	18
R 18	RES. 2K 1/4W 5%	RC07GF202J	18
R 19	RES. 100 1/4W 5%	RC07GF101J	13
R 20	RES. 49.9K 1/8W 1%	RN55C4992F	19
R 21	RES. 100K 1/8W 1%	RN55C1003F	20
R 22	RES. 100K 1/8W 1%	RN55C1003F	20
R 23	RES. 200 1/8W 1%	RN55C2000F	14
R 24	RES. 100K 1/8W 1%	RN55C1003F	20
R 25	RES. 49.9K 1/8W 1%	RN55C4992F	19
R 26	RES. 1K 1/4W 5%	RC07GF102J	15
R 27	RES. 332K 1/8W 1%	RN55C3323F	22
R 28	RES. 100K 1/4W 5%	RC07GF104J	21
R 29	TRIM POT 10K 15T	CERMET 3006P 10K	23
R 30	TRIM POT 10K 15T	CERMET 3006P 10K	23
R 31	RES. 2K 1/4W 5%	RC07GF202J	18
R 32	RES. 2K 1/4W 5%	RC07GF202J	18
R 33	RES. 2K 1/4W 5%	RC07GF202J	18
R 34	RES. 100 1/4W 5%	RC07GF101J	13
R 35	RES. 49.9K 1/8W 1%	RN55C4992F	19
R 36	RES. 100K 1/8W 1%	RN55C1003F	20
R 37	RES. 100K 1/8W 1%	RN55C1003F	20
R 38	RES. 200 1/8W 1%	RN55C2000F	14
R 39	RES. 100K 1/8W 1%	RN55C1003F	20
R 40	RES. 49.9K 1/8W 1%	RN55C4992F	19
R 41	RES. 1K 1/4W 5%	RC07GF102J	15
R 42	RES. 332K 1/8W 1%	RN55C3323F	22
R 43	RES. 100K 1/4W 5%	RC07GF104J	21
R 44	TRIM POT 10K 15T	CERMET 3006P 10K	23
R 45	TRIM POT 10K 15T	CERMET 3006P 10K	23
R 46	RES. 2K 1/4W 5%	RC07GF202J	18
R 47	RES. 2K 1/4W 5%	RC07GF202J	18
R 48	RES. 2K 1/4W 5%	RC07GF202J	18
R 49	RES. 100 1/4W 5%	RC07GF101J	13
R 50	RES. 49.9K 1/8W 1%	RN55C4992F	19
R 51	RES. 100K 1/8W 1%	RN55C1003F	20
R 52	RES. 100K 1/8W 1%	RN55C1003F	20
R 53	RES. 200 1/8W 1%	RN55C2000F	14
R 54	RES. 100K 1/8W 1%	RN55C1003F	20
R 55	RES. 49.9K 1/8W 1%	RN55C4992F	19
R 56	RES. 1K 1/4W 5%	RC07GF102J	15
R 57	RES. 332K 1/8W 1%	RN55C3323F	22
R 58	RES. 100K 1/4W 5%	RC07GF104J	21
R 59	TRIM POT 10K 15T	CERMET 3006P 10K	23
R 60	TRIM POT 10K 15T	CERMET 3006P 10K	23
R 61	RES. 470 1/4W 5%	RC07GF471J	16
R 62	RES. 1.5K 1/8W 1%	RN55C1501F	17
R 63	RES. 240 1/4W 5%	RC07GF41J	31
R 64	RES. 5K 1/4W 5%	RC07GF502J	32
R 65	RES. 5K 1/4W 5%	RC07GF502J	32
R 66	RES. 5K 1/4W 5%	RC07GF502J	32
R 67	RES. 5K 1/4W 5%	RC07GF502J	32
TJ 1	TEST JACK BLACK	105-0753-001	25
TJ 2	TEST JACK WHITE	105-0751-001	28
TJ 3	TEST JACK BROWN	105-0758-001	27
TJ 4	TEST JACK GREEN	105-0754-001	26
TJ 5	TEST JACK WHITE	105-0751-001	28
TJ 6	TEST JACK BROWN	105-0758-001	27
TJ 7	TEST JACK GREEN	105-0754-001	26
TJ 8	TEST JACK WHITE	105-0751-001	28
TJ 9	TEST JACK BROWN	105-0758-001	27
TJ 10	TEST JACK GREEN	105-0754-001	26
TJ 11	TEST JACK WHITE	105-0751-001	28
TJ 12	TEST JACK BROWN	105-0758-001	27
TJ 13	TEST JACK GREEN	105-0754-001	26
U 1	IC TL084BCN	TL084BCN	11
U 2	IC TL084BCN	TL084BCN	11
U 3	IC TL084BCN	TL084BCN	11
U 4	IC TL084BCN	TL084BCN	11
U 5	IC AD581JH	AD581JH	12
U 6	IC AD581JH	AD581JH	12



COMPONENT SIDE

#22 BUS WIRE

- NOTES:  
 1. HOLES THAT ARE SHADED TO BE PLATED THRU  
 2. ALL DIP IC PACKAGES USE SOCKETS- ITEM 29 (ICN-143-53-X). U1-U4. A BEAD  
 3. ALL COMPONENT VALUES SHOULD BE VISIBLE IF POSSIBLE.

- ① Bom A53Z00B00Z  
 ② SCH. D53Z005001  
 ③ C53Z009001  
 ④ DRILL DWG. D53Z00P001

B	REV	DATE	GM	APPR'D BY	DESCRIPTION
					C0870219-7
FRONT END					
ASSY - BIAS CARD					
NATIONAL RADIO ASTRONOMY OBSERVATORY CHARLOTTESVILLE, VA. 22904					
DRAWN BY: G. MORRIS DATE: 09-68					
DESIGNED BY: S. WENJER DATE:					
APPROVED BY: DATE:					
DRAWING NUMBER: D53Z00A00Z REV: B SCALE: 2X					



## 2.9 RF Plate Description

The RF Plate is installed on the side of the card cage and performs the amplification, calibration and 300 °K temperature measurement functions shown on the F104 Block Diagram C53204K001, TR 10 page 2. These are: amplification of the LCP and RCP signals from the cooled amplifiers in the dewar, the generation of low and high noise calibration signals, injection of a phase calibration signal, and measurement of the RF Plate temperature.

The RF Plate Assembly drawing is C53203A005 and is shown on TR 10, Appendix page II-9. The associated BOM is A53204B005 and Appendix page II-10 lists the RF Plate components. There is not an RF Card Block diagram. P17, connected to the card cage J17, provides DC power and low frequency connections to the RF Plate. The RF Plate is physically identical to the 1.5 GHz RF Plate but uses different components.

The F104 Block Diagram 53204K001 and RF Plate Assembly drawing shows a High Calibration noise source as an optional F104 feature. Although it may not be installed in all F104s, provisions have been made for its installation.

Block Diagram C53204K002 shows the RF Plate functions in the context of this addendum's description. Since the emphasis of this addendum is on the theory of operation of the card cage circuitry, the RF Plate functions are not described here. Refer to TR 10 Page 33, for a description of the RF Plate's noise calibration circuitry. The room temperature post amplifiers have noise figures less than 3.5 dB and 17 to 20 dB of gain. These amplifiers are described in specification A53204N001 (not part of this manual). The specifications on TR 10 pages 5 through 8 encompass the RF Plate's performance.

The RF Plate has a National Semiconductor LM335Z Precision Temperature Sensor to measure the the plate's temperature. The sensor output is designated 300 °K and connected to the Monitor Card for measurement by the DVM and to the Monitor and Control System via J2-5. The LM335 operates as a two-terminal zenar and has a breakdown voltage directly proportional to absolute temperature with a scaling of +10 mV/°K. Section 4 contains a LM335Z data sheet.

## 2.10 Dewar DC Interface Description

The DC Feedthrough is the interface for the connection of DC power and HEMT bias lines to the dewar RF amplifiers, AC power to the heater, and signal lines to temperature sensing diodes, and the LED circuitry. Wire list A53203W001 does not include the wiring between the card cage J3 and the DC Feedthrough. This wiring is shown on C53204K002, the 2.3 GHz FE Block Diagram.

The B53206A012 dewar DC Feedthrough is a hermetically-sealed interface panel that uses RFI feedthrough terminals soldered into a brass plate attached to the dewar inspection cover. Feedthrough terminal designations are shown on the artwork of a printed circuit board installed on the outside of the feedthrough. These designations are those used in C53204K002. Figure 4 on the next page shows the PC board terminal designations.

Sixteen HEMT drain (VD) and gate (VG) bias lines pass through the DC Feedthrough and are connected to the dewar amplifiers via two small 7-pin, Micro-Tech connectors. Since the emphasis of this report is on the card cage circuitry, for simplicity, these connectors are not shown on the block diagram. The HEMT source lines are connected to dewar ground.

The 15 °K stage temperature sensor diode (TSA) is connected to terminals A+ and A-. The diode anode is connected to A+ and the cathode to A-. Similarly, the 50 °K stage temperature sensor diode (TSB) anode and cathode are connected to terminals B+ and B-.

As shown on C53204K002, the dewar LEDs circuit consists of two series strings, each consisting of three LEDs and a 300 Ω limiting resistor. The bottom of the strings are connected to dewar ground, J3-21, and the tops are connected to terminal X1. Outside the dewar, X1 is connected to P3-22. J3-22 is connected to pin T on the Monitor Card, the LED monitor input for the DVM. A 510 Ω limiting resistor is connected between pin T and Pin X. Pin X is not connected to any Monitor Card circuitry and simply serves as a convenient mounting terminal for the resistor. Pin X is jumpered to Pin 2 and B, the +15 volt bus. This resistor is shown on the Card Cage Assembly Drawing, D53203A004, TR 10 Appendix page II-6. The typical F104 LED monitor voltage is +5.0 volts but it can range between +4.5 to +5.5 volts. If one of the LED strings opens, the LED monitor voltage is +11 volts and if both open, the monitor readout is +15 volts. This value can be read on the DVM but will be full-scale in the Monitor and Control system readout because it exceeds the working range of the Standard Interface Board's A/D converter in F117.

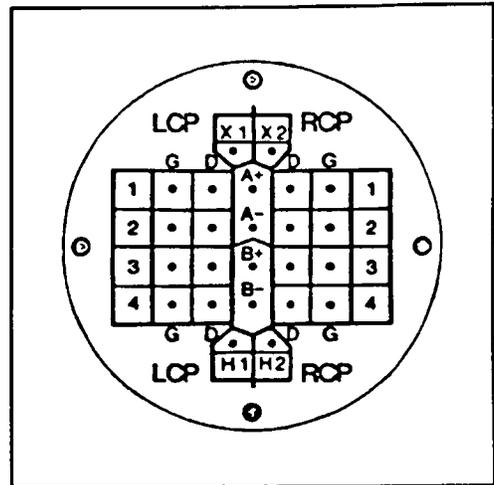


Figure 4 Dewar DC Feedthrough Label

The dewar ground line is also connected to the dewar metal structure.

The dewar heater AC power is connected to terminals H1 and H2. Inside the dewar, these terminals are connected to two 750 Ω, 75 watt, 240 volt heaters.

## 2.11 AC Circuitry Description

The dewar's cryogenic functions are powered by two-phase, 150 volts AC power. Figure 1.3-3 on page 18, in TR 10 shows the Front-End's AC wiring. Page 16 lists the cryogenic function's AC loads. Because the F104 AC power is peculiar to the refrigerator's requirements, it does not have an internal DC power supply for the card cage circuitry. DC + and - 15 volt power is provided by the control interface via J5. This DC power is described in Section 2.15.

Note that the 150 volt, two-phase power is supplied by a Model P112 power supply, which is described in 2.9, page 35, in TR 10. Figure 2.9-1, page 38, shows the power supply schematic. An important P112 power supply output is the AC current monitor, which is a DC signal scaled at 10 amperes/volt. This is input to the Front-End on J4-1 (signal) and J4-2 (return) and the signal polarity is positive. This signal, designated ACI, is connected to the Monitor Panel for DVM measurement and to J2-6 for readout by the Monitor and Control System.

On page 18, note the vacuum solenoid current limiting resistor R<sub>1</sub>, 300 Ω, 20 watts, which is installed on the card cage connector mounting plate. This resistor is pictured in the card cage assembly drawing, D53203A004, TR 10 Appendix page II-6. If the vacuum solenoid is actuated for a long time,

the plate will become quite hot from the resistor's power dissipation. Also note that a stuck vacuum solenoid will draw 0.40 amperes. The dewar heater limiter resistor R<sub>2</sub> 5 kΩ, 10 watts, is also installed on the card cage connector mounting plate; it too is pictured on the card cage assembly drawing.

The cryogenic control equations were described in Section 2.4 and Section 2.5, (Control Card) described the implementation of the control equations. Note that the R, S, H and X contacts shown on the Front-End Wiring schematic (Figure 1.3-3, page 18) are the Control Card relay contacts.

The dewar heater is two 750 Ω, 75 watt, 240 volt Hotwatt heater installed on the 15 °K stage. Heater current is 0.40 amperes and dissipation is 60 watts. Note from the Front-End AC wiring schematic on page 18 that the heater has an internal thermostat that opens at a high temperature level. This feature prevents overheating in the event of a Control Card failure.

## 2.12 DVM Readout Values and Tolerances

The table below shows the DVM analog selector switch position Label, Function, Scaling, Normal Value and acceptable Tolerance Range.

DVM S2 Label	Function	1 volt =	Normal Value	Tolerance Range
VP	Pump Vacuum <sup>1</sup>	-----	+10.000 <sup>2</sup>	+9.950 to +10.000
VD	Dewar Vacuum <sup>1</sup>	-----	0.000	-0.200 to +0.200
15K	15 °K Stage	100 °K	+0.150	+0.100 to +0.200
50K	50 °K Stage	100 °K	+0.550	+0.400 to +0.700
300K	300 °K Station	100 °K	+2.900	+2.000 to +3.000
AC CURR	AC Current <sup>3</sup>	10 Amps	-----	-----
RF1	RCP Gate 1	1 Volt	-0.60 <sup>4</sup>	-1.00 to +1.00
RF2	RCP Gates 2+3 <sup>5</sup>	1 Volt	-0.60 <sup>4</sup>	-1.00 to +1.00
LF1	LCP Gate 1	1 Volt	-0.60 <sup>4</sup>	-1.00 to +1.00
LF2	LCP Gates 2+3 <sup>5</sup>	1 Volt	-0.60 <sup>4</sup>	-1.00 to +1.00
LED	LED Voltage	1 Volt	+5.0 <sup>6</sup>	+4.500 to +5.500
EXT	Spare Mon	1 Volt	-----	N/A

### Notes:

1 Nonlinear vacuum readout scale, see page 15 in TR 10.

2 Readout when pump manifold is at sea level atmospheric pressure.

3 AC current depends upon cryogenic state, see page 16 in TR 10.

4 Typical value. Large changes indicate a dewar amplifier problem.

5 Approximate sum of Stage 2 and 3 Gate voltages.

6 If one LED string opens, the LED readout voltage is about +11 volts; if both strings open, the LED readout is +15 volts.

### 2.13 Monitor and Control System Readout Values

The Telescope Operator Front-End Cryogenic and Electronics displays show F104 status; Figures 5 and 6 are similar to these displays. Figure 5 shows the calibration mode, monitored calibration current and voltage, and the three HEMT gate bias voltages. Figure 6 shows the commanded cryogenics mode, monitored mode, state, discrettes, and selected analog monitor values.

```
FRONT END ELECTRONICS 13CM
CAL MODE LOW SWITCHING
CAL I 7.03 V 27.813 HEMT 5.05
7.5 V 7.505 GRD -0.005
LF FET#1 -0.195 RT FET#1 -0.220
LF FET#2 -0.693 RT FET#2 -1.211
```

Figure 5 VLBA F104 Electronics Screen

```
FRONT END CRYOGENICS 13CM
CMD COOL MANUAL STATE COOL
PUMP REQ OFF AC 1 0.81
VALVE CLOSED 15K 14.6
PUMP VAC 9846 50K 59.6
DEWAR VAC 1 300K 293
```

Figure 6 VLBA F104 Cryogenics Screen

The VLBA control interface is F117. It controls F104, reads F104 discrettes, and converts F104 analog signals to digital values for input to the Antenna control computer via the Monitor and Control bus.

The first VLBA screen shows that the calibration level is LOW and is SWITCHING. F117 measures some additional Front-End analog parameters: (CAL I) cal current, cal voltage, the F117 +7.5 volt reference (7.5V), and F117 ground reference (GRD). The example values show a calibration current of 7.03 mA and a cal voltage of 27.813 volts. The HEMT 5.05 voltage is the LED measurement described in Section 2.10. The FET voltages are the Bias Card HEMT gate voltages described in Section 2.8.

The second VLBA screen shows that the Front-End is commanded to the COOL state, is in the MANUAL mode, and the X, C and H monitor discrettes show the COOL state. The PUMP REQ(uest) is OFF and the (vacuum) VALVE is CLOSED. The 150 volt AC current load is 0.81 amperes. PUMP (VP) VAC is 9846 because the vacuum manifold is at the antenna's atmospheric pressure (see the vacuum vs. monitor voltage curve on page 15). DEWAR VAC(uum) is 1  $\mu$ m. Note that this value has been converted from the voltage readout value to the corresponding vacuum level. The 15K (TA), 50K (TB), and 300K temperatures are shown degrees Kelvin. The SENS temperature (non-linear form of TA) is not shown.

If F104 is installed on the VLA, the control interface would probably be F14.

## 2.14 Band, Serial Number, and Modification Level Encoding

F104 has provisions to identify its serial number, frequency band and modification level as hard-wired binary codes on the J5 connector. These codes are implemented by connecting the appropriate J5 pins to ground lugs near the connector. Grounded pins are 0's and floating pins are 1's. The control interfaces (such as F14, VLA or F117, VLBA) have pull-up resistors to +5 volts for input to TTL logic. Drawing C53204K002 shows the code bit assignments on J5.

The F104 band code is  $3_H$  and the associated parity bit is a 0. Page 14 in TR 10 describes the band, serial number and modification level encoding.

## 2.15 Front-End DC power and Quality Ground

The F104 card cage DC power is + and - 15 volts from J5, provided by the associated control interface, F117. The -15 volt power demand is 100 mA and the +15 volt power demand is 500 mA. The +15 volt current demand is dependent upon F104's cryogenic state. The Control and Monitor card's LS-TTL logic is powered by on-card +5 volt regulators from +15 volt inputs.

Bus-bars running through the card cage PC board connectors (including spare card slots 1 and 2) provide +15 and -15 and power from J5-2 (+15) and J5-3 (-15), respectively. Unlike other VLBA-style Front-Ends, the F104 does not have protective 1N5355A 18 volt zenar diodes installed in the card cage +15 and -15 volt bus bars. The Ground bus bar is connected to chassis ground at slot 7, the Control Card. DC power distribution is shown in C53204K002.

Quality Ground is an analog ground reference that does not carry power currents. This reference is supplied to the Monitor Panel DVM and to the control interface via J2-13. The Quality Ground is connected to chassis ground near slot 5, the LCP FET Bias Card. The Quality Ground string is shown on C53204K002.

Dewar ground on J3-21 is connected to the Ground Bus and also to the dewar internal metal structure. This is the return path for the HEMT sources and the LED strings.

Note that Table II, TR 10, page 12 shows that J5-13 is a ground pin. This pin is floating as shown on the card cage wire list A53203W001, sheet 12, Appendix page II-26.

## 2.16 Wire List Problems

Wire List A53203W001, Sheet 8, TR 10 Appendix page II-22 has an error in the Pin S TO column. It has P14-S; it should be P14-1. On Sheet 12, Appendix page II-26, the TO column shows Gnd Bus for pin 14. It should be N.C. because it is the F0 encoding pin and the F104 Band Code is  $03_H$ ; this pin should float for this code.



### 3.0 RELEVANT NRAO DRAWINGS

Title:	Number:	Notes:
2.3 GHz FE Block Diagram C53204K002		
System Block Diagram	C53204K001	
Front-End Assembly	D53204A001	TR 10, Page 10
Front-End BOM	A53204B001	TR 10, Appendix page II-1
Card Cage Assembly*	D53203A004	TR 10, Appendix page II-6
Card Cage BOM*	A53203B004	TR 10, Appendix page II-7
Card Cage Wire List*	A53203W001	TR 10, Appendix page II-15
RF Plate Assembly*	C53203A005	TR 10, Appendix page II-9
RF Card BOM	A53204B005	TR 10, Appendix page II-10
Sensor Card Schematic	D53200S002	
Sensor Card Assembly	D53200A003	
Sensor Card BOM		No BOM, parts are on the assembly drawing.
Control Card Schematic	D53200S002	
Control Card Assembly	D53200A004	
Control Card BOM	A53200B004	
Monitor Card Schematic	C53200S005	
Monitor Card Assembly	D53200A006	
Monitor Card BOM	A53200B006	
FET Bias Card Schematic	D53200S001	
FET Bias Card Assembly	D53200S002	
FET Bias Card BOM	A53200B002	

\* These components are similar to those used in F103, the 1.5 GHz Front-End.



## 4.0 COMPONENT DATA SHEETS

Data sheets for:

Lake Shore Cryotronics DT-500  
Hastings DV-6R  
Hastings DB-20  
Texas Instruments TL084  
Texmate PM-45XU  
Analog Devices AD581JH  
National Semiconductor LM339N  
Texas Instruments 75452  
Teledyne 643-1  
Teledyne 645-2  
National Semiconductor LM393AN  
Analog Devices AD7512DIKN  
National Semiconductor LM335Z  
Precision Monolithics OP-10CY



Standard Curve 10: Measurement Current = 10  $\mu$ A  $\pm$ 0.05%

T (K)	Voltage	dV/dT (mV/K)	T (K)	Voltage	dV/dT (mV/K)	T (K)	Voltage	dV/dT (mV/K)
1.40	1.69812	-13.1	16.0	1.28527	-18.6	95.0	0.98564	-2.02
1.60	1.69521	-15.9	16.5	1.27607	-18.2	100.0	0.97550	-2.04
1.80	1.69177	-18.4	17.0	1.26702	-18.0	110.0	0.95487	-2.08
2.00	1.68786	-20.7	17.5	1.25810	-17.7	120.0	0.93383	-2.12
2.20	1.68352	-22.7	18.0	1.24928	-17.6	130.0	0.91243	-2.16
2.40	1.67880	-24.4	18.5	1.24053	-17.4	140.0	0.89072	-2.19
2.60	1.67376	-25.9	19.0	1.23184	-17.4	150.0	0.86873	-2.21
2.80	1.66845	-27.1	19.5	1.22314	-17.4	160.0	0.84650	-2.24
3.00	1.66292	-28.1	20.0	1.21440	-17.6	170.0	0.82404	-2.26
3.20	1.65721	-29.0	21.0	1.19645	-18.5	180.0	0.80138	-2.28
3.40	1.65134	-29.8	22.0	1.17705	-20.6	190.0	0.77855	-2.29
3.60	1.64529	-30.7	23.0	1.15558	-21.7	200.0	0.75554	-2.31
3.80	1.63905	-31.6	24.0	1.13598	-15.9	210.0	0.73238	-2.32
4.00	1.63263	-32.7	25.0	1.12463	-7.72	220.0	0.70908	-2.34
4.20	1.62602	-33.6	26.0	1.11896	-4.34	230.0	0.68564	-2.35
4.40	1.61920	-34.6	27.0	1.11517	-3.34	240.0	0.66208	-2.36
4.60	1.61220	-35.4	28.0	1.11212	-2.82	250.0	0.63841	-2.37
4.80	1.60506	-36.0	29.0	1.10945	-2.53	260.0	0.61465	-2.38
5.00	1.59782	-36.5	30.0	1.10702	-2.34	270.0	0.59080	-2.39
5.50	1.57928	-37.6	32.0	1.10263	-2.08	280.0	0.56690	-2.39
6.00	1.56027	-38.4	34.0	1.09864	-1.92	290.0	0.54294	-2.40
6.50	1.54097	-38.7	36.0	1.09490	-1.83	300.0	0.51892	-2.40
7.00	1.52166	-38.4	38.0	1.09131	-1.77	310.0	0.49484	-2.41
7.50	1.50272	-37.3	40.0	1.08781	-1.74	320.0	0.47069	-2.42
8.00	1.48443	-35.8	42.0	1.08436	-1.72	330.0	0.44647	-2.42
8.50	1.46700	-34.0	44.0	1.08093	-1.72	340.0	0.42221	-2.43
9.00	1.45048	-32.1	46.0	1.07748	-1.73	350.0	0.39783	-2.44
9.50	1.43488	-30.3	48.0	1.07402	-1.74	360.0	0.37337	-2.45
10.0	1.42013	-28.7	50.0	1.07053	-1.75	370.0	0.34881	-2.46
10.5	1.40615	-27.2	52.0	1.06700	-1.77	380.0	0.32416	-2.47
11.0	1.39287	-25.9	54.0	1.06346	-1.78	390.0	0.29941	-2.48
11.5	1.38021	-24.8	56.0	1.05988	-1.79	400.0	0.27456	-2.49
12.0	1.36809	-23.7	58.0	1.05629	-1.80	410.0	0.24963	-2.50
12.5	1.35647	-22.8	60.0	1.05267	-1.81	420.0	0.22463	-2.50
13.0	1.34530	-21.9	65.0	1.04353	-1.84	430.0	0.19961	-2.50
13.5	1.33453	-21.2	70.0	1.03425	-1.87	440.0	0.17464	-2.49
14.0	1.32412	-20.5	75.0	1.02482	-1.91	450.0	0.14985	-2.46
14.5	1.31403	-19.9	80.0	1.01525	-1.93	460.0	0.12547	-2.41
15.0	1.30422	-19.4	85.0	1.00552	-1.96	470.0	0.10191	-2.30
15.5	1.29464	-18.9	90.0	0.99565	-1.99	475.0	0.09062	-2.22

Shaded portion highlights truncated portion of Standard Curve 10 corresponding to the reduced temperature range of DT-471 diode sensors.  
The 1.4 K to 325 K portion of Curve 10 is applicable to the DT-450 miniature silicon diode sensor.

DT-500-DRC (B) Voltage - Temperature Characteristic

T <sub>i</sub> , Kelvin	Sensor Voltage	T <sub>i</sub> , Kelvin	Sensor Voltage	T <sub>i</sub> , Kelvin	Sensor Voltage
1.0	--	19.0	1.5944	160.0	0.75680
1.5	2.6647	20.0	1.5159	165.0	0.74276
1.6	2.6622	21.0	1.4389	170.0	0.72868
1.7	2.6593	22.0	1.3575	175.0	0.71457
1.8	2.6562	23.0	1.2895	180.0	0.70041
1.9	2.6528	24.0	1.2378	185.0	0.68622
2.0	2.6491	25.0	1.1955	190.0	0.67201
2.2	2.6410	26.0	1.1645	195.0	0.65777
2.4	2.6321	27.0	1.1434	200.0	0.64353
2.6	2.6223	28.0	1.1293	205.0	0.62928
2.8	2.6117	29.0	1.1192	210.0	0.61504
3.0	2.6005	30.0	1.1115	215.0	0.60084
3.2	2.5886	32.0	1.1003	220.0	0.58672
3.4	2.5762	34.0	1.0923	225.0	0.57268
3.6	2.5633	36.0	1.0859	230.0	0.55880
3.8	2.5499	38.0	1.0804	235.0	0.54508
4.0	2.5361	40.0	1.0752	240.0	0.53152
4.2	2.5220	45.0	1.0632	245.0	0.51810
4.4	2.5075	50.0	1.0515	250.0	0.50479
4.6	2.4928	55.0	1.0397	255.0	0.49151
4.8	2.4780	60.0	1.0276	260.0	0.47818
5.0	2.4631	65.0	1.0151	265.0	0.46483
5.5	2.4254	70.0	1.0024	270.0	0.45137
6.0	2.3877	75.0	0.98933	275.0	0.43773
6.5	2.3505	80.0	0.97610	280.0	0.42388
7.0	2.3142	85.0	0.96277	285.0	0.40988
7.5	2.2790	90.0	0.94939	290.0	0.39574
8.0	2.2452	95.0	0.93591	295.0	0.38155
8.5	2.2127	100.0	0.92238	300.0	0.36729
9.0	2.1818	105.0	0.90881	305.0	0.35294
9.5	2.1524	110.0	0.89520	310.0	0.33843
10.0	2.1246	115.0	0.88156	315.0	0.32375
11.0	2.0731	120.0	0.86788	320.0	0.30893
12.0	2.0236	125.0	0.85412	325.0	0.29407
13.0	1.9730	130.0	0.84035	330.0	0.27919
14.0	1.9186	135.0	0.82652	335.0	0.26432
15.0	1.8561	140.0	0.81265	340.0	0.24943
16.0	1.7942	145.0	0.79873	345.0	0.23458
17.0	1.7325	150.0	0.78478	350.0	0.21974
18.0	1.6651	155.0	0.77081	355.0	0.20500
				360.0	0.19037
				365.0	0.17596
				370.0	0.16192
				375.0	0.14846
				380.0	0.13597



Lake Shore Cryotronics, Inc.  
64 East Walnut Street • Westerville, Ohio 43081-2399  
Fax: (614) 891-1392 • Tel: (614) 891-2243

# HASTINGS VACUUM GAUGE TUBES

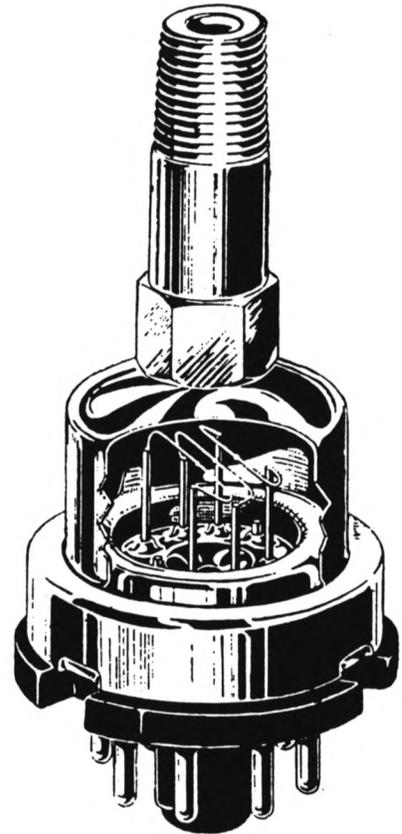
For Economy and Reliability in Vacuum Measurement

- **Corrosion-Resistant**
- **Non-Contaminating**
- **Stable Calibration**
- **Rugged Under Demanding Conditions**



Standard Metal Type

 **TELEDYNE**  
**BROWN ENGINEERING**  
Hastings Instruments



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## Design Features

Hastings Vacuum Gauge Tubes are precision sensing devices designed to provide maximum accuracy in the measurement and control of vacuum. Fully compensated for both temperature and rate of temperature change, the tubes are renowned worldwide for their dependability, and boast a history of success that has endured for over 40 years.

Hastings Gauge Tubes use the rugged but sensitive, time-tested Hastings thermopile sensor. Short, firmly connected thermocouples have no suspended weld to an external heater.

The unique Model DV-760 uses a piezo-resistive strain gauge on a silicon chip. The chip includes a sealed vacuum reference, a resistive bridge circuit, and a temperature compensation network.

Hastings Gauge Tubes are color-coded for matching to the appropriate vacuum gauge or controller.

## CHARACTERISTICS OF HASTINGS VACUUM GAUGE TUBES

	DV-4D	DV-5M	DV-6M	DV-8	DV-23	DV-24	DV-760
Metal Tube	DV-4D	DV-5M	DV-6M	DV-8	DV-23	DV-24	DV-760
"R" Series	DV-4R	—	DV-6R	—	—	—	—
Stainless/Ceramic	DV-34	—	DV-36	—	—	—	—
Pyrex	DV-16D	DV-18	DV-20	DV-31	DV-43	DV-44	—
Metal w/VCR Connection	DV-4D-VCR	DV-5M-VCR	DV-6M-VCR	—	DV-23-VCR	—	—
Metal w/KF-16 Connection	DV-4D-KF-16	—	DV-6M-KF-16	—	DV-23-KF-16	DV-24-KF-16	—
Best Sensitivity Range	0.2 - 5 torr 0.1 - 5 mbar	2 - 20 mtorr 0.002 - .05 mbar	10 - 200 mtorr .01 - .2 mbar	0.1 - 10 mtorr —	5 mtorr - 1 torr .01 - 2 mbar	.1 - 5 torr .1 - 5 mbar	1 - 800 torr 1 - 1100 mbar
Usable Range	0.1 - 20 torr 0.1 - 20 mbar	0.2 - 100 mtorr 0.001 - .1 mbar	1 - 1000 mtorr .01 - 1 mbar	0.1 - 10 mtorr —	5 mtorr - 5 torr .01 - 5 mbar	.1 - 20 torr .1 - 10 mbar	1 - 800 torr 1 - 1100 mbar
Internal Volume of Gauge Tube	1/20 <sup>3</sup> 0.8cc	1/2 <sup>3</sup> 8.2cc	1/2 <sup>3</sup> 8.2cc	1/2 <sup>3</sup> 8.2cc	1/2 <sup>3</sup> 8.2cc	1/2 <sup>3</sup> 8.2cc	1/20 <sup>3</sup> 0.8cc
Thermopile Temperature In a High Vacuum At Atmosphere	250°C 30°C	48°C 1.5°C	300°C 6°C	120°C 10°C	400°C 10°C	400°C 35°C	N/A N/A
A-C Amperes Through Tube	0.029	0.03	0.021	0.053	.04/.04	.03/.04	N/A
A-C Volts Across Tube	0.32	0.20	0.38	0.32	.20/.20	.19/.19	N/A
Watts Required by Tube	0.009	0.006	0.006	0.017	.016	.11	.018
Output at High Vacuum mv D-C	10	2	10	2	13	13	—
Internal Resistance - ohms	11	6	18	6	5/6	6.5/7.5	—
Response Time Zero to ATM - seconds ATM to Zero - seconds	0.04 0.16	0.8 25	0.06 2.9	0.8 25	0.07 3.0	0.05 .2	.002 .002
A-C Connection Pin #	3-5	3-5	3-5	3-5	2-4, 6-8	2-4, 6-8	—
D-C Connection Pin #	7	7	7	7	—	—	—
Color of Base Metal Tube	Purple	Red	Yellow	Green	Orange	White	Lt. Blue

The above information includes nominal values only. Not to be used for design purposes or acceptance tests.

### PRESSURE AND TEMPERATURE DATA

Tube Type	Max. Pressure	Max. Temperature
Metal: DV-4D, DV-4D-VCR, DV-4D-KF-16	150 psig	100°C
All other metal (except Model DV-760)	50 psig	100°C
"R" Series	250 psig	150°C
Stainless/Ceramic	600 psig	300°C
Pyrex	15 psig	400°C
Model DV-760	15 psig	40°C

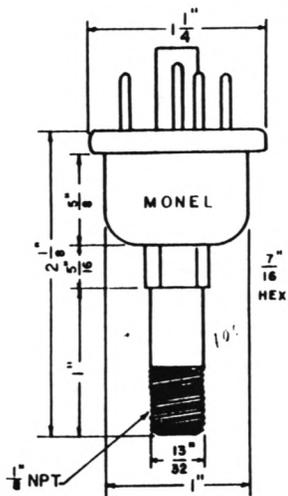
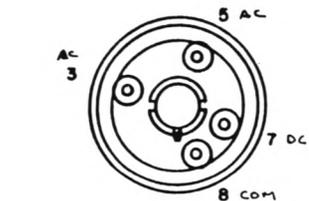
The gauge tubes can be expected to withstand the listed pressure and temperature without rupture but they are not warranted as safe under these conditions. For critical conditions or special testing, contact factory.



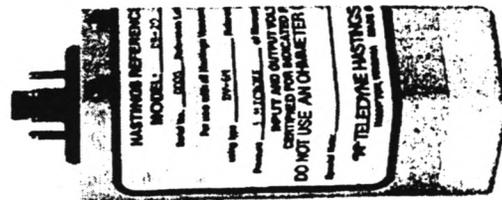
# HASTINGS REFERENCE TUBE

A Quick Calibration Device for  
Hastings Vacuum Gauges

- Instant Calibration Check
- Recalibration of Hastings Gauges
- Adjusts Gauge for Any Length Cable
- Stable, Accurate, Rugged, and Reliable



DV-4 R  
DV-6 R



Reference Tube

**TELEDYNE  
BROWN ENGINEERING**  
Hastings Instruments

## General

The Hastings Reference Tube is an evacuated, sealed vacuum gauge tube accurately calibrated to precisely simulate a gauge tube at a given operating pressure. It is electrically equivalent to the metal and glass gauge tubes used with Hastings Instruments. It permits quick and easy recalibration of Hastings Vacuum Gauge Indicators by merely plugging the instrument into the reference and adjusting the calibration "current set" potentiometer until the instrument reads the exact pressure noted on the reference. Hastings Reference Tubes are available equivalent to most Hastings Gauge Tubes.

## Application

Hastings Vacuum Gauge Indicators, Controllers, or Recorders can be checked or recalibrated in seconds by merely plugging the gauge tube cable into the reference tube. If calibration adjustment is necessary, the "Current Set" potentiometer is adjusted until the instrument indicates the pressure marked on the reference tube. The customer now knows his instrument is correctly calibrated.

Whenever cable lengths between gauge tube and instrument are changed, some error may be introduced, requiring that the instrument be readjusted to compensate for any losses involved. By plugging the Reference Tube into the new cable and readjusting the instrument for a correct reading, this "error" is eliminated.

## Selection

Choose the reference tube that is equivalent to the glass or metal Hastings Gauge Tube you are now using. The Reference Tube will be matched and sealed at a pressure falling on the lower portion of the scale and calibrated accurately at this exact pressure. For example, if an instrument uses a DV-6M Gauge Tube, a DB-20 Reference Tube is ordered. The customer receives a tube marked, possibly, 10 microns. This is the exact pressure to which the indicator should be adjusted when plugged into the reference tube.

## Selection Chart

Equivalent Gauge Tube and Range			Reference Tube	
Metal	Glass	Range	Model No.	Stock No.
* DV-3M		0-1000 $\mu$ Hg		
DV-4D		0-20mm Hg	DB-16D	55-100
* DV-5M		0-100 $\mu$ Hg	* DB-18	55-103
DV-6M	DV-20	0-1000 $\mu$ Hg	DB-20	55-104
DV-8M		0.01-10 $\mu$ Hg	DB-31	55-105
DV-23		0-5000 $\mu$ Hg	DB-33	55-106
DV-24		0-50 Torr	DB-44	55-107
DV-310		0-1000 mTorr and 0-1400 mbar	DB-300	55-252

\*State reference letter of your Gauge Tube type for matching purposes.

## Construction

Hastings Reference Tubes employ the same Hastings noble metal thermopile used in all Hastings Vacuum Gauge Tubes. The thermopile is sealed in a glass capsule that has been evacuated, baked, outgassed, sealed, and then aged to ensure stability over long periods of time. The sealed capsule is then housed in a protective metal shell to provide a rugged, trouble-free assembly.

## Calibration

Considerable care and time are required in the manufacture to obtain the high degree of precision and stability required for the reference tube.

The thermopile is matched to the reference letter of the customer's tubes and maintains its calibration over long periods of time. However, for applications requiring the highest possible degree of accuracy, a periodic return of the reference tube to the factory for a check and recalibration may be desirable. An annual or semiannual check assures the customer of an accurate and reliable reference at all times.

## IMPORTANT NOTE:

These reference tubes are designed specifically for use with instruments employing Hastings circuitry and are NOT interchangeable with instruments using other circuitry. Connection to another manufacturer's instrument may result in burnout.

*Hastings Instruments reserves the right to change or modify the design of its equipment without any obligation to provide notification of change or intent to change.*

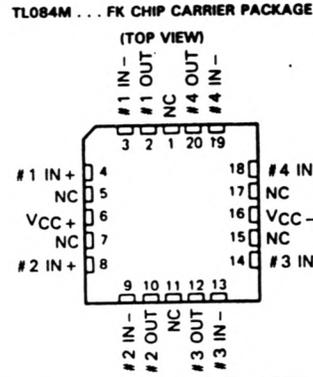
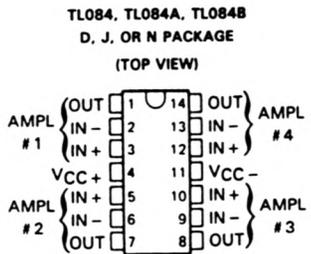
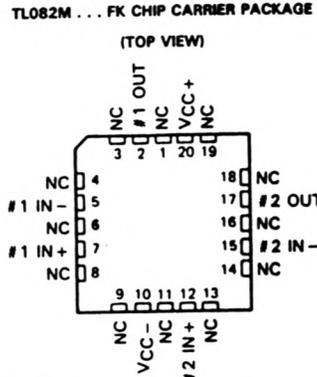
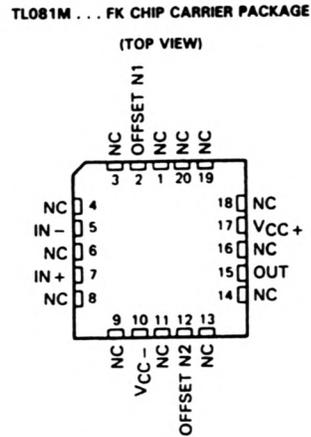
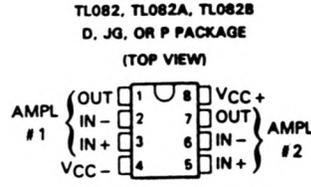
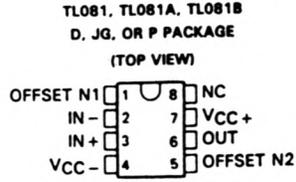
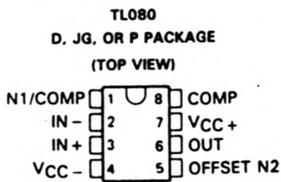
**TELEDYNE  
BROWN ENGINEERING**  
Hastings Instruments

P.O. Box 1436 • Hampton, VA 23661

**TL080, TL081, TL082, TL084, TL081A, TL082A, TL084A  
TL081B, TL082B, TL084B  
JFET-INPUT OPERATIONAL AMPLIFIERS**  
D2297, FEBRUARY 1977—REVISED OCTOBER 1990

**24 DEVICES COVER MILITARY, INDUSTRIAL AND COMMERCIAL TEMPERATURE RANGES**

- Low-Power Consumption
- Wide Common-Mode and Differential Voltage Ranges
- Low Input Bias and Offset Currents
- Output Short-Circuit Protection
- Low Total Harmonic Distortion . . . 0.003% Typ
- High Input Impedance . . . JFET-Input Stage
- Internal Frequency Compensation (Except TL080, TL080A)
- Latch-Up-Free Operation
- High Slew Rate . . . 13 V/ $\mu$ s Typ
- Common-Mode Input Voltage Range Includes  $V_{CC+}$



NC—No internal connection



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No products conform to MIL-STD-883C, Class B, all parameters are tested unless otherwise noted. Do not order products, production processing does not necessarily include testing of all parameters.

2-387

**TL080, TL081, TL082, TL084, TL081A, TL082A, TL084A  
TL081B, TL082B, TL084B  
JFET-INPUT OPERATIONAL AMPLIFIERS**

**absolute maximum ratings over operating free-air temperature range (unless otherwise noted)**

	TL08_C TL08_AC TL08_BC	TL08_I	TL08_M	UNIT
Supply voltage, $V_{CC+}$ (see Note 1)	18	18	18	V
Supply voltage, $V_{CC-}$ (see Note 1)	-18	-18	-18	V
Differential input voltage (see Note 2)	$\pm 30$	$\pm 30$	$\pm 30$	V
Input voltage (see Notes 1 and 3)	$\pm 15$	$\pm 15$	$\pm 15$	V
Duration of output short circuit (see Note 4)	unlimited	unlimited	unlimited	
Continuous total dissipation	See Dissipation Rating Table			
Operating free-air temperature range	0 to 70	-40 to 85	-55 to 125	$^{\circ}$ C
Storage temperature range	-65 to 160	-65 to 160	-65 to 160	$^{\circ}$ C
Case temperature for 60 seconds	FK package			260
Lead temperature 1.6 mm (1/16 inch) from case for 60 seconds	J or JG package			300
Lead temperature 1.6 mm (1/16 inch) from case for 10 seconds	D, N, or P package			260

- NOTES: 1. All voltage values, except differential voltages, are with respect to the midpoint between  $V_{CC+}$  and  $V_{CC-}$ .  
2. Differential voltages are at the noninverting input terminal with respect to the inverting input terminal.  
3. The magnitude of the input voltage must never exceed the magnitude of the supply voltage or 15 V, whichever is less.  
4. The output may be shorted to ground or to either supply. Temperature and/or supply voltages must be limited to ensure that the dissipation rating is not exceeded.

**electrical characteristics,  $V_{CC\pm} = \pm 15$  V (unless otherwise noted)**

PARAMETER	TEST CONDITIONS <sup>†</sup>	MIN	TYP	MAX	MIN	TYP	MAX	UNIT
$V_{IO}$ Input offset voltage	$V_O = 0$ , $R_S = 50 \Omega$		3	6	3	9		mV
Temperature coefficient of input offset voltage	$V_O = 0$ , $R_S = 50 \Omega$ , $T_A = -55^{\circ}\text{C to } 125^{\circ}\text{C}$		18		18			$\mu\text{V}/^{\circ}\text{C}$
$I_{IO}$ Input offset current <sup>‡</sup>	$V_O = 0$		5	100	5	100		pA
$I_{IB}$ Input bias current <sup>‡</sup>	$V_O = 0$		30	200	30	200		pA
$V_{ICR}$ Common-mode input voltage range	$T_A = 25^{\circ}\text{C}$	$\pm 11$	to	15	$\pm 11$	to	15	V
$V_{OM}$ Maximum peak output voltage swing	$T_A = 25^{\circ}\text{C}$ , $R_L = 10 \text{ k}\Omega$	$\pm 12$	$\pm 13.5$		$\pm 12$	$\pm 13.5$		V
	$T_A = -55^{\circ}\text{C to } 125^{\circ}\text{C}$ , $R_L \geq 10 \text{ k}\Omega$	$\pm 12$			$\pm 12$			
	$T_A = 25^{\circ}\text{C}$ , $R_L \geq 2 \text{ k}\Omega$	$\pm 10$	$\pm 12$		$\pm 10$	$\pm 12$		
$A_{VD}$ Large-signal differential voltage amplification	$V_O = \pm 10 \text{ V}$ , $T_A = 25^{\circ}\text{C}$ , $R_L \geq 2 \text{ k}\Omega$	25	200		25	200		V/mV
	$V_O = \pm 10 \text{ V}$ , $T_A = -55^{\circ}\text{C to } 125^{\circ}\text{C}$ , $R_L \geq 2 \text{ k}\Omega$	15			15			
$B_1$ Unity-gain bandwidth	$T_A = 25^{\circ}\text{C}$		3		3			MHz
$r_i$ Input resistance	$T_A = 25^{\circ}\text{C}$		$10^{12}$		$10^{12}$			$\Omega$
CMRR Common-mode rejection ratio	$V_{IC} = V_{ICR \text{ min}}$ , $R_S = 50 \Omega$ , $V_O = 0$ , $T_A = 25^{\circ}\text{C}$	80	86		80	86		dB
$k_{SVR}$ Supply voltage rejection ratio ( $\Delta V_{CC\pm}/\Delta V_{IO}$ )	$V_{CC} = \pm 15 \text{ V to } \pm 9 \text{ V}$ , $R_S = 50 \Omega$ , $V_O = 0$ , $T_A = 25^{\circ}\text{C}$	80	86		80	86		dB
$I_{CC}$ Supply current (per amplifier)	No load, $T_A = 25^{\circ}\text{C}$ , $V_O = 0$	1.4	2.8		1.4	2.8		mA
$V_{O1}/V_{O2}$ Crosstalk attenuation	$A_{VD} = 100$ , $T_A = 25^{\circ}\text{C}$		120			120		dB

<sup>†</sup> All characteristics are measured under open-loop conditions with zero common-mode input voltage unless otherwise specified.  
<sup>‡</sup> Input bias currents of a FET-input operational amplifier are normal junction reverse currents, which are temperature sensitive as shown in Figure 18. Pulse techniques must be used that will maintain the junction temperatures as close to the ambient temperature as is possible.

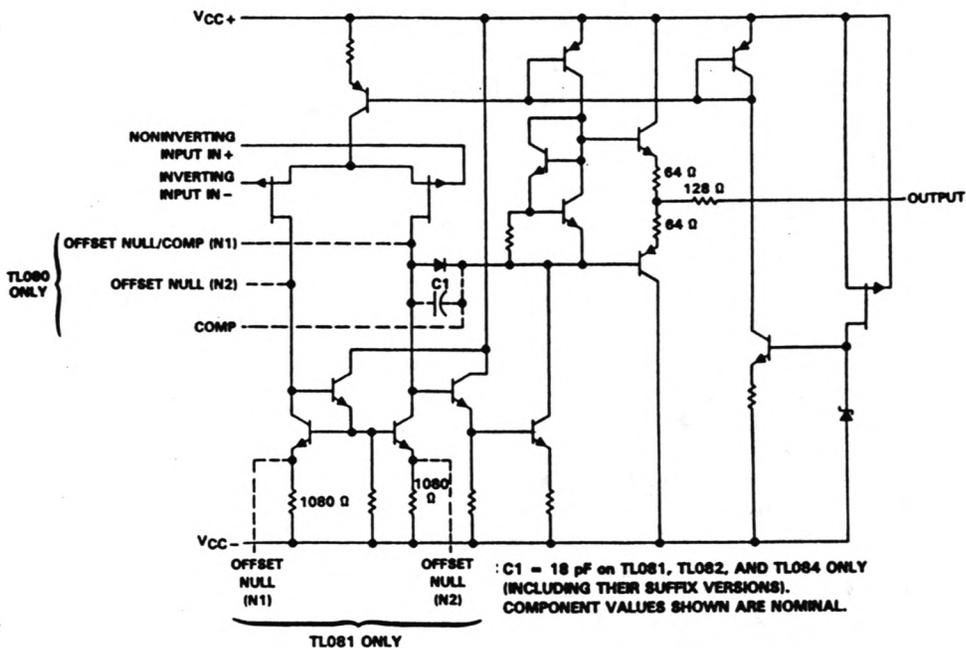
TL080, TL081, TL082, TL084, TL081A, TL082A, TL084A  
TL081B, TL082B, TL084B  
JFET-INPUT OPERATIONAL AMPLIFIERS

operating characteristics,  $V_{CC\pm} = \pm 15\text{ V}$ ,  $T_A = 25^\circ\text{C}$  (unless otherwise noted)

PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
SR	Slew rate at unity gain $V_i = 10\text{ V}$ , $R_L = 2\text{ k}\Omega$ , $C_L = 100\text{ pF}$ . See Figure 1	8*	13		V/ $\mu\text{s}$
$t_r$	Rise time $V_i = 20\text{ mV}$ , $R_L = 2\text{ k}\Omega$ , $C_L = 100\text{ pF}$ . See Figure 1		0.05		$\mu\text{s}$
	Overshoot factor		20%		
$V_n$	Equivalent input noise voltage $R_S = 100\ \Omega$ , $f = 1\text{ kHz}$ $f = 10\text{ Hz}$ to $10\text{ kHz}$		18		nV/ $\sqrt{\text{Hz}}$
$I_n$	Equivalent input noise current $R_S = 100\ \Omega$ , $f = 1\text{ kHz}$		0.01		pA/ $\sqrt{\text{Hz}}$
THD	Total harmonic distortion $V_O(\text{rms}) = 10\text{ V}$ , $R_S \leq 1\text{ k}\Omega$ , $R_L \geq 2\text{ k}\Omega$ , $f = 1\text{ kHz}$		0.003%		

\*On products compliant to MIL-STD-883, Class B, this parameter is not production tested.

schematic (each amplifier)

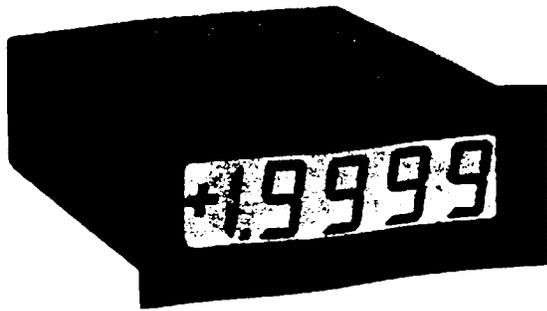


electrical characteristics,  $V_{CC\pm} = \pm 15\text{ V}$  (unless otherwise noted)

PARAMETER	TEST CONDITIONS†	TL080C TL081C TL082C TL084C			TL081AC TL082AC TL084AC			TL081BC TL082BC TL084BC			TL081B TL082B TL084B			UNIT
		MIN	TYP	MAX										
$V_{IO}$	Input offset voltage Temperature $V_O = 0$ , $R_S = 50\ \Omega$	$T_A = 25^\circ\text{C}$ 3	$T_A = 25^\circ\text{C}$ 15	$T_A = \text{full range}$ 20	$T_A = 25^\circ\text{C}$ 3	$T_A = 25^\circ\text{C}$ 15	$T_A = \text{full range}$ 7.5	$T_A = 25^\circ\text{C}$ 3	$T_A = 25^\circ\text{C}$ 15	$T_A = \text{full range}$ 5	$T_A = 25^\circ\text{C}$ 3	$T_A = 25^\circ\text{C}$ 15	$T_A = \text{full range}$ 9	mV
$e_{VIO}$	coefficient of input offset voltage $V_O = 0$ , $R_S = 50\ \Omega$	$T_A = 25^\circ\text{C}$ 18	$T_A = 25^\circ\text{C}$ 18	$T_A = \text{full range}$ 18	$T_A = 25^\circ\text{C}$ 18	$T_A = 25^\circ\text{C}$ 18	$T_A = \text{full range}$ 18	$T_A = 25^\circ\text{C}$ 18	$T_A = 25^\circ\text{C}$ 18	$T_A = \text{full range}$ 18	$T_A = 25^\circ\text{C}$ 18	$T_A = 25^\circ\text{C}$ 18	$T_A = \text{full range}$ 18	$\mu\text{V}/^\circ\text{C}$
$I_{IO}$	Input offset current† $V_O = 0$	$T_A = 25^\circ\text{C}$ 5	$T_A = 25^\circ\text{C}$ 200	$T_A = \text{full range}$ 2	$T_A = 25^\circ\text{C}$ 5	$T_A = 25^\circ\text{C}$ 100	$T_A = \text{full range}$ 2	$T_A = 25^\circ\text{C}$ 5	$T_A = 25^\circ\text{C}$ 100	$T_A = \text{full range}$ 2	$T_A = 25^\circ\text{C}$ 5	$T_A = 25^\circ\text{C}$ 100	$T_A = \text{full range}$ 2	pA
$I_{IB}$	Input bias current† $V_O = 0$	$T_A = 25^\circ\text{C}$ 30	$T_A = 25^\circ\text{C}$ 400	$T_A = \text{full range}$ 10	$T_A = 25^\circ\text{C}$ 30	$T_A = 25^\circ\text{C}$ 200	$T_A = \text{full range}$ 7	$T_A = 25^\circ\text{C}$ 30	$T_A = 25^\circ\text{C}$ 200	$T_A = \text{full range}$ 7	$T_A = 25^\circ\text{C}$ 30	$T_A = 25^\circ\text{C}$ 200	$T_A = \text{full range}$ 7	pA
$V_{ICR}$	Common-mode input voltage range $T_A = 25^\circ\text{C}$	$T_A = 25^\circ\text{C}$ $\pm 11$ to 15	V											
$V_{OM}$	Maximum peak output voltage swing $T_A = 25^\circ\text{C}$	$T_A = 25^\circ\text{C}$ $\pm 12$ $\pm 13.5$	V											
$A_{VD}$	Large-signal differential voltage amplification $V_O = \pm 10\text{ V}$ , $R_L \geq 2\text{ k}\Omega$ , $T_A = 25^\circ\text{C}$	$T_A = 25^\circ\text{C}$ 25	$T_A = 25^\circ\text{C}$ 200	$T_A = 25^\circ\text{C}$ $\pm 10$ $\pm 12$	$T_A = 25^\circ\text{C}$ 25	$T_A = 25^\circ\text{C}$ 200	$T_A = 25^\circ\text{C}$ $\pm 10$ $\pm 12$	$T_A = 25^\circ\text{C}$ 25	$T_A = 25^\circ\text{C}$ 200	$T_A = 25^\circ\text{C}$ $\pm 10$ $\pm 12$	$T_A = 25^\circ\text{C}$ 25	$T_A = 25^\circ\text{C}$ 200	$T_A = 25^\circ\text{C}$ $\pm 10$ $\pm 12$	V/mV
$B_1$	Unity-gain bandwidth $T_A = 25^\circ\text{C}$	$T_A = 25^\circ\text{C}$ 3	$T_A = 25^\circ\text{C}$ 1012	$T_A = 25^\circ\text{C}$ 3	$T_A = 25^\circ\text{C}$ 3	$T_A = 25^\circ\text{C}$ 1012	$T_A = 25^\circ\text{C}$ 3	$T_A = 25^\circ\text{C}$ 3	$T_A = 25^\circ\text{C}$ 1012	$T_A = 25^\circ\text{C}$ 3	$T_A = 25^\circ\text{C}$ 1012	$T_A = 25^\circ\text{C}$ 3	$T_A = 25^\circ\text{C}$ 1012	MHz
CMRR	Common-mode rejection ratio $V_{IC} = V_{ICR}(\text{min})$ , $V_O = 0$ , $R_S = 50\ \Omega$ , $T_A = 25^\circ\text{C}$	$T_A = 25^\circ\text{C}$ 70	$T_A = 25^\circ\text{C}$ 86	$T_A = 25^\circ\text{C}$ 70	$T_A = 25^\circ\text{C}$ 70	$T_A = 25^\circ\text{C}$ 86	$T_A = 25^\circ\text{C}$ 70	$T_A = 25^\circ\text{C}$ 70	$T_A = 25^\circ\text{C}$ 86	$T_A = 25^\circ\text{C}$ 70	$T_A = 25^\circ\text{C}$ 86	$T_A = 25^\circ\text{C}$ 70	$T_A = 25^\circ\text{C}$ 86	dB
$k_{SVR}$	Supply voltage rejection ratio ( $\Delta V_{CC} \pm \Delta V_{IO}$ ) $V_{CC} = \pm 15\text{ V}$ to $\pm 8\text{ V}$ , $V_O = 0$ , $R_S = 50\ \Omega$ , $T_A = 25^\circ\text{C}$	$T_A = 25^\circ\text{C}$ 70	$T_A = 25^\circ\text{C}$ 86	$T_A = 25^\circ\text{C}$ 70	$T_A = 25^\circ\text{C}$ 70	$T_A = 25^\circ\text{C}$ 86	$T_A = 25^\circ\text{C}$ 70	$T_A = 25^\circ\text{C}$ 70	$T_A = 25^\circ\text{C}$ 86	$T_A = 25^\circ\text{C}$ 70	$T_A = 25^\circ\text{C}$ 86	$T_A = 25^\circ\text{C}$ 70	$T_A = 25^\circ\text{C}$ 86	dB
I <sub>CC</sub>	Supply current (per amplifier) No load, $T_A = 25^\circ\text{C}$	$V_O = 0$ , $T_A = 25^\circ\text{C}$ 1.4	$V_O = 0$ , $T_A = 25^\circ\text{C}$ 2.8	$V_O = 0$ , $T_A = 25^\circ\text{C}$ 1.4	$V_O = 0$ , $T_A = 25^\circ\text{C}$ 1.4	$V_O = 0$ , $T_A = 25^\circ\text{C}$ 2.8	$V_O = 0$ , $T_A = 25^\circ\text{C}$ 1.4	$V_O = 0$ , $T_A = 25^\circ\text{C}$ 2.8	$V_O = 0$ , $T_A = 25^\circ\text{C}$ 1.4	$V_O = 0$ , $T_A = 25^\circ\text{C}$ 2.8	$V_O = 0$ , $T_A = 25^\circ\text{C}$ 1.4	$V_O = 0$ , $T_A = 25^\circ\text{C}$ 2.8	$V_O = 0$ , $T_A = 25^\circ\text{C}$ 1.4	mA
$V_{O1/02}$	Quiescent attenuation $V_{O1/02} = 100$ , $T_A = 25^\circ\text{C}$	$T_A = 25^\circ\text{C}$ 120	dB											

† All characteristics are measured under open-loop conditions with zero common-mode input voltage unless otherwise specified. Full range for  $T_A$  is  $0^\circ\text{C}$  to  $70^\circ\text{C}$  for TL080, TL081, TL082, TL084, TL081A, TL082A, TL084A, TL081B, TL082B, TL084B, and  $-40^\circ\text{C}$  to  $85^\circ\text{C}$  for TL081C, TL082C, TL084C, TL081AC, TL082AC, TL084AC, TL081BC, TL082BC, TL084BC, TL081B, TL082B, TL084B. Pulse techniques must be used that will maintain the junction temperatures as close to the ambient temperature as is possible.

# TEXMATE



## PM-45X & PM-45XU 4 1/2 DIGIT PANEL METERS

**ACCURACY LCD METERS WITH 10 $\mu$ V RESOLUTION, TRUE DIFFERENTIAL INPUTS, ULTRA LOW POWER <25mW AT +5VDC, AND STANDARD MUX-BCD OR OPTIONAL PARALLEL BCD OUTPUTS**

### DESCRIPTION

The PM-45X and PM-45XU are truly unique and extremely versatile instruments. Believed to be the world's smallest and most energy efficient 4 1/2 Digit LCD Panel Meters, they nevertheless offer more high performance features than most larger and more expensive DPM's.

Both meters incorporate a crystal controlled 100KHz clock that provides an exceptionally high normal mode rejection of 120dB at multiples to 50/60Hz. Bipolar differential and single-ended DC voltages from  $\pm 199.99$ mV to  $\pm 1200.0$ V full scale can be measured and scaled in almost any known engineering unit. Provision has been made for signal offsetting and the capability of attenuating both high and low signal inputs. Resolution is 10 $\mu$ V over  $\pm 19999$  counts, and errors due to zero drift are virtually eliminated by autozeroing. Other modes of operation, selectable by the user, include an ohmmeter mode, current meter mode and ratiometric mode.

Multiplexed BCD data is available internally from a row of auxiliary solder pads. Both meters may be ordered with an internally mounted Tri-state Buffered Parallel BCD Output Board. This option, which is described in detail on a separate data sheet, can also be purchased for field retrofit.

The PM-45X features an ultra stable temperature compensated reference with selected low TC components. The PM-45XU is a derated economy priced model that provides all the features of the PM-45X but utilizes a standard reference, and components with less stringent specifications.

The true differential input capabilities and high 86dB common mode rejection ratio, combined with their low signal measurement range and high noise immunity, make these meters ideal for measuring various balanced transducers and bridge inputs. When measuring bridge circuits, long term drift of the excitation voltage can be compensated by using the ratiometric voltmeter mode of operation.

The proprietary high contrast, long life liquid crystal display provides excellent readability under high and low ambient light conditions. Since the meters normally draw only a small constant current (<25mW), operation from almost any DC power supply is simplified. If the supply has a stability of only 10%, a voltage dropping resistor in series with the meter is often sufficient. (See Application notes.)

### SPECIFICATIONS

<b>Input Configuration:</b>	True differential and single-ended
<b>Full Scale Ranges:</b>	$\pm 199.99$ mVDC $\pm 1.9999$ VDC (standard) $\pm 19.999$ VDC $\pm 199.99$ VDC $\pm 1200.0$ VDC (max. Input Signal; higher voltages can be measured if voltage dividing resistors are located externally)
<b>Input Impedance:</b>	Exceeds 1000M $\Omega$ on 200mV and 2V ranges 10M $\Omega$ on all other ranges
<b>Input Protection:</b>	$\pm 170$ VDC or 120VAC on 200mV and 2V ranges. $\pm 1200$ VDC or 850VAC on all other ranges
<b>Normal Mode Rejection:</b>	120dB at multiples of 50/60Hz
<b>Common Mode Rejection:</b>	86dB at DC; greater than 120dB at multiples of 50/60Hz
<b>Common Mode Voltage:</b>	-2.8V to +2.8V (standard) $\pm 2.8$ V or more if differential dividers are used (see Typical Application Circuits and Connection Instructions)
<b>Accuracy:</b>	PM-45X $\pm (0.01\%$ of reading + 1 digit) $\pm (0.015\%$ of reading + 2 digits) for 200mV range. PM-45XU $\pm (0.015\%$ of reading + 2 digits). $\pm (0.02\%$ of reading + 3 digits) for 200mV range
<b>Maximum Resolution:</b>	10 $\mu$ V over $\pm 19999$ counts in 200mV range. 100 $\mu$ V over $\pm 19999$ counts in 2V range
<b>Temperature Coefficient:</b>	PM-45X: 5PPM/ $^{\circ}$ C ratiometric, 20PPM/ $^{\circ}$ C using internal adjustable T.C. Reference. PM-45XU: 5PPM/ $^{\circ}$ C ratiometric, 50PPM/ $^{\circ}$ C using internal reference
<b>Zero Stability:</b>	Autozeroed $\pm 10\mu$ V at all ranges; $\pm 1\mu$ V/ $^{\circ}$ C Typical
<b>Conversion Rate:</b>	2.5 readings per second
<b>Clock Frequency:</b>	100KHz system clock derived from 200KHz quartz crystal controlled oscillator of 0.05% accuracy
<b>Display:</b>	0.48" LCD
<b>Polarity:</b>	Automatic; displays both "+" and "-" signs; polarity symbols may be blanked (see page 6)
<b>Overload Indication:</b>	When input exceeds full scale on any range being used, the most significant "1" digit and "+" or "-" symbol is displayed with all other digits blank
<b>Power Requirements:</b>	Low ripple +4.5V to +5.5VDC at 3mA to 5mA
<b>Warmup Time:</b>	10 seconds to specified accuracy
<b>Operating Temperature:</b>	0 $^{\circ}$ C to +60 $^{\circ}$ C

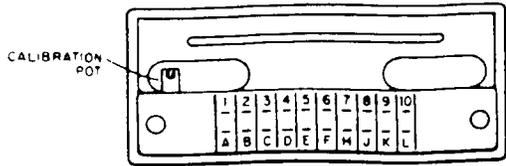
### ORDERING INFORMATION

	Order Part No.	Order Part No.
<b>Standard High Accuracy 4 1/2 Digit Panel Meter (2V Range)</b>	PM-45X	
<b>Standard Utility Version 4 1/2 Digit Panel Meter (2V Range)</b>	PM-45XU	
<b>PM-45X W/Tri-State Parallel BCD Output</b>	PM-45XBCD	
<b>PM-45XU W/Tri-State Parallel BCD Output</b>	PM-45XUBCD	
<b>Retrofit Tri-State Parallel BCD Board for PM-45X/PM-45XU</b>	PM-45XBCDO	
<b>Accessories: Edge Connector (20 pin solder tabs)</b>	CN-L10	
<b>Options: Factory Installed 200mV Range</b>	VG-200MVFI	
<b>Factory Installed 20V Range</b>	VFA-0020V	
<b>Factory Installed 200V Range</b>	VFA-0200V	
<b>Factory Installed 1200V Range</b>	VFA-1200V	
<b>Factory Installed Special Scaling (Specify input signal, the span, and digital reading required, e.g. 1 to 5V input to display 0 to 10,000; 4 to 20mA input to display 0 to 15,000; 0 to 50mA input to display -1,000 to +8,000 )</b>	VS 4 5	
<b>Range Change Kits: (matched resistors for user installation)</b>		
200mV Range		VG-200MV
20V Range		VKA-0020V
200V Range		VKA-0200V
1200V Range		VKA-1200V
<b>Optional Cases* (see back page for details)</b>		
<b>End Mount Case (twin meter mounting)</b>		EM-CASECLR
<b>Center Mount Case (multiple array mounting)</b>		CM-CASECLR
<b>Slim Bezel Case (supplied as standard)</b>		SL-CASECLR

\*Meters purchased prior to August 1989 require cases with a polarizer bonded to the rear side of the lens. To order these cases, use the following part numbers EM-CASELCD, CM-CASELCD, SL-CASELCD.

# CONNECTOR PINOUTS

The Texmate Model PM-45X/PM-45XU is interconnected by means of a standard PC board edge connector having two rows of 10 pins, spaced on 0.156" centers. The optional parallel BCD Output is interconnected by a standard PC board edge connector having two rows of 13 pins spaced on 0.1" centers. (A standard 26 pin, PCB to Ribbon Cable Connector is recommended.) Connectors are available from Texmate, or from almost any connector manufacturer.

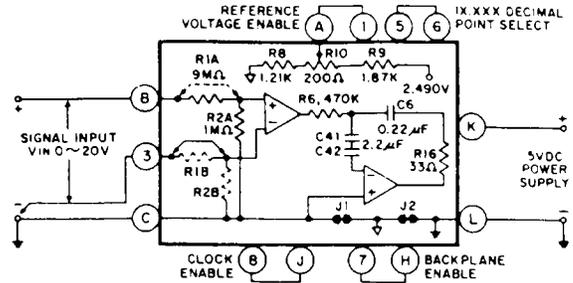


REAR VIEW OF METER CASE

- |                              |                                   |
|------------------------------|-----------------------------------|
| A — Reference Output         | 1 — Reference Input               |
| B — Signal High Input        | 2 — Offset Voltage Output         |
| C — Analog Common            | 3 — Signal Low Input              |
| D — Decimal Select (1XXX.X)  | 4 — Decimal Select (1XX.XX)       |
| E — Decimal Select (1.XXX.X) | 5 — Decimal Select Common         |
| F — Decimal Select (1.XXXX)  | 6 — Decimal Select (1X.XXX)       |
| H — Back Plane Output        | 7 — Back Plane Input/Display Test |
| J — Clock Output             | 8 — Clock Input                   |
| K — +5VDC System Power Input | 9 — Busy Output                   |
| L — Power Ground Input       | 10 — Run/Hold                     |

**CAUTION:** This meter employs high impedance CMOS inputs. Although internal protection has been provided for several hundred volt overloads, the meter will be destroyed if subjected to the high kilovolts of static discharge that can be produced in low humidity environments. Always handle the meter with ground protection.

# FUNCTIONAL DIAGRAM



## SINGLE-ENDED METER — >2V RANGES WITH VOLTAGE DIVIDER

1) High single ended voltages, up to 1200V max. can be measured and/or scaled by installing the appropriate voltage dividing resistors in R1A and R2A positions. Matched dividing resistors for the 20V (1/10), 200V (1/100), and 1200V (1/1000) ranges are available from Texmate. 2) Connect Pin 3 to the nearest end of the signal source ground to avoid possible errors caused by ground loop currents.

# PIN DESCRIPTIONS

**Pin A — Reference Output:** Internal precision voltage reference. Standard output is 1.0000V, adjustable  $\pm 5\%$  by R10 potentiometer. Usable voltages from 0.05V to 2.49V for special high impedance scaling can be obtained by changing the value of internal dividing resistors R8 and R9. The primary reference voltage of the PM-45X is trimmed by potentiometer R20 to obtain the optimum compensated temperature coefficient. This temperature compensation network is omitted on the PM-45XU utility meter. Please read CALIBRATION PROCEDURE (Page 7).

**Pin B — Signal High Input:** Pin B is the signal high input for all input signal ranges. When attenuation is not required the resistor position R1A must be shorted by a jumper. Dividing resistors may be mounted internally in R1A and R2A positions to attenuate voltages up to 1200V max. Matched dividing resistors for the 20V (1/10), 200V (1/100) and 1200V (1/1000) ranges are available from Texmate. Shunt resistors for current measurements up to 200mA may also be internally mounted in the R2A position. The current loop is then applied to Pin B and returned through Analog Common Pin C.

**Pin C — Analog Common:** Pin C is signal return common for differential inputs, ratiometric inputs, or external reference inputs. For single-ended inputs, Signal Low Input Pin 3 must be connected to Analog Common Pin C. To minimize any errors caused by ground loop currents it is recommended that this connection be made as close as possible to the input signal source ground. (See Typical Application Circuits and Connection Instructions, Pages 4-6.)

**Pins D, E, F, 4 and 6 — Decimal Select:** Decimal points may be displayed as required by connecting the appropriate pin to Decimal Select Common Pin 5. Any number of decimal points can be turned on at the same time. An open circuit will turn off the decimal points. However, static current pickup and/or PCB leakage of more than 100nA can cause decimal points to turn on undesirably. Therefore, it is recommended that the unused decimal points be connected to Back Plane Output Pin H either directly or by a resistor of less than 5M $\Omega$  to insure an off condition. **CAUTION:** Any DC component introduced to the display drive circuitry can, in time, cause permanent damage. PLEASE READ PAGES 7 AND 8 FOR A DETAILED EXPLANATION OF LCD OPERATION.

**Pin H — Back Plane Output:** Liquid crystal displays are operated from an AC signal. Back Plane Output Pin H provides a square wave signal of 60~160HZ that must be connected by the user to back plane input Pin 7 for normal operation. Pin 7 is internally connected to the LCD back plane which is the common base of the LCD capacitance structure. Those segments that are driven 180° out-of-phase with the back plane will turn on. Those segments that are driven in-phase with the back plane will turn off. PLEASE READ PAGES 7 AND 8 FOR A DETAILED EXPLANATION OF LCD OPERATION.

**Pin J — Clock Output:** A quartz crystal controlled oscillator provides a stable clock signal output of 100KHz.

**Pin K — +5VDC System Power Input:** The meter requires a low ripple DC power supply of 4.5V to 5.5VDC at 3mA to 5mA. The low power consumption of only 25mW enables the meter to be easily operated from various power sources with simple voltage regulating circuitry. The positive terminal of the power supply should be connected to Pin K.

**Pin L — Power Ground Input:** Negative terminal of the +5VDC power supply should be connected to Pin L. All digital signals, Display Test, and Run/Hold should be returned to this ground point. Pin L is internally connected to Analog Common Pin C.

**Pin 1 — Reference Input:** Reference voltage input for A to D converter. Normally supplied from Pin A. An external reference source referred to Pin C may be used instead. Pin 1 may be used as an input for ratiometric measurements. Minimum usable voltage is .05VDC, with a maximum voltage of 4.0V. For ratiometric operation; Displayed Reading = 10000 X (Signal Input Voltage  $\div$  Reference Input Voltage). The maximum signal input

voltage is  $\pm 4V$ . Higher voltages must be scaled down through a voltage divider. Reference input voltage must remain stable during measurement period.

**Pin 2 — Offset Voltage Output:** 0 to +2.490V is available with the addition of a  $\frac{1}{4}$ " 20K $\Omega$  to 100K $\Omega$  pot in the R15 position on the printed circuit board. The offset voltage is derived from the internal precision voltage reference and is available for applications requiring a zero offset such as 4~20mA receiver and temperature measurements.

**Pin 3 — Signal Low Input:** Pin 3 is the signal low input for all input signals. A special feature of the meter is the provision for dividing resistors to be mounted internally in the R1B and R2B positions. This enables low signal inputs up to 1200V max to be attenuated, which is particularly useful when measuring small differential signals with a large common mode voltage. Matched dividing resistors for the 20V (1/10), 200V (1/100) and 1200V (1/1000) ranges are available from Texmate. Differential current measurements up to 200mA may also be made by internally mounting shunt resistors in the R2B position. The current loop is then applied to Pin B and returned through Analog Common Pin C. When attenuation is not required the resistor position R1B must be shorted by a jumper.

**Pin 5 — Decimal Select Common:** Pin 5 is 180° out-of-phase with back plane output Pin H. Thus it serves as a common for the decimal select Pins D, E, F, 4 and 6. To turn on any required decimal point, connect the appropriate Decimal Select Pin to Decimal Select Common Pin 5.

**Pin 7 — Back Plane Input/Display Test:** Pin 7 is connected to the display's back plane which forms the common base of the LCD capacitance structure. Join Pin 7 to back plane output Pin H for normal operation. For Display Test connect Pin 7 instead to Power Ground Pin L and all operative segments will turn on, indicating +18888. **CAUTION:** The Display Test function is only intended for momentary operation. Continuous application of Display Test will, in time, damage the display. SEE PAGES 7 AND 8 FOR A DETAILED EXPLANATION OF LCD OPERATION.

**Pin 8 — Clock Input:** Normally Pin 8 is connected to the 100KHz clock output from Pin J, thereby providing the optimum rejection of 50/60 Hz noise. However, an external clock source may be used instead (5V referenced to power ground with a recommended duty cycle of 50%). Minimum frequency is 10KHz, and maximum frequency is 1MHz (12.5 readings per sec.). For inputs below 100KHz or above 300KHz, changes to the integrator time constant and some component values are necessary.

**Pin 9 — Busy Output:** Pin 9 goes to logic "1" at the beginning of the signal integration and remains at "1" until the first clock pulse after the zero-crossing is detected at the completion of deintegration. In addition to its use as a Busy or End-of-Conversion signal, the output on Pin 9 can be used in some control applications to indicate the digital reading of the meter as a function of time or clock pulses. Displayed Reading is equal to the total clock pulses during Busy less 10,000, or total elapsed time during Busy, less 100 milliseconds if the clock frequency is 100KHz.

**Pin 10 — Run/Hold:** If Pin 10 is left open (or connected to +5VDC System Power Input Pin K for logic control purposes), the meter will operate in a free-running mode. Under control of the internal 100KHz quartz crystal clock, readings will be updated every 400ms (2.5 per sec.). If Pin 10 is connected to Power Ground Input Pin L (logic low), the meter will continue the measurement cycle that it is doing, then latch up and continuously hold the reading obtained as long as Pin 10 is held low. If Pin 10 is released from Pin L (Pin 10 then goes logic high) for more than 300ns and returned to Pin L (logic low), the meter will complete one conversion, update, and then hold the new reading. For all practical purposes, a manually actuated normally closed pushbutton switch will provide sufficient timing for "press-to-update" operation.

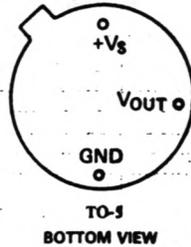
**High Precision  
10V IC Reference**

**AD581\***

**FEATURES**

- Laser-Trimmed to High Accuracy:  
10.000 Volts  $\pm 5\text{mV}$  (L and U)
- Trimmed Temperature Coefficient:  
5ppm/ $^{\circ}\text{C}$  max, 0 to  $+70^{\circ}\text{C}$  (L)  
10ppm/ $^{\circ}\text{C}$  max,  $-55^{\circ}\text{C}$  to  $+125^{\circ}\text{C}$  (U)
- Excellent Long-Term Stability:  
25ppm/1000 hrs. (Noncumulative)
- Negative 10 Volt Reference Capability
- Low Quiescent Current: 1.0mA max
- 10mA Current Output Capability
- 3-Terminal TO-5 Package

**AD581 FUNCTIONAL BLOCK DIAGRAM**



**PRODUCT DESCRIPTION**

The AD581 is a three-terminal, temperature compensated, monolithic band-gap voltage reference which provides a precise 10.00 volt output from an unregulated input level from 12 to 30 volts. Laser Wafer Trimming (LWT) is used to trim both the initial error at  $+25^{\circ}\text{C}$  as well as the temperature coefficient, which results in high precision performance previously available only in expensive hybrids or oven-regulated modules. The 5mV initial error tolerance and 5ppm/ $^{\circ}\text{C}$  guaranteed temperature coefficient of the AD581L represent the best performance combination available in a monolithic voltage reference.

The band-gap circuit design used in the AD581 offers several advantages over classical Zener breakdown diode techniques. Most important, no external components are required to achieve full accuracy and stability of significance to low power systems. In addition, total supply current to the device, including the output buffer amplifier (which can supply up to 10mA) is typically 750 $\mu\text{A}$ . The long-term stability of the band-gap design is equivalent or superior to selected Zener reference diodes.

The AD581 is recommended for use as a reference for 8-, 10- or 12-bit D/A converters which require an external precision reference. The device is also ideal for all types of A/D converters up to 14 bit accuracy, either successive approximation or integrating designs, and in general can offer better performance than that provided by standard self-contained references.

The AD581J, K, and L are specified for operation from 0 to  $+70^{\circ}\text{C}$ ; the AD581S, T, and U are specified for the  $-55^{\circ}\text{C}$  to  $+125^{\circ}\text{C}$  range. All grades are packaged in a hermetically-sealed three-terminal TO-5 metal can.

\*Covered by Patent Nos. 3,887,863; RE 30,586

**PRODUCT HIGHLIGHTS**

1. Laser trimming of both initial accuracy and temperature coefficient results in very low errors over temperature without the use of external components. The AD581L has a maximum deviation from 10.000 volts of  $\pm 7.25\text{mV}$  from 0 to  $+70^{\circ}\text{C}$ , while the AD581U guarantees  $\pm 15\text{mV}$  maximum total error without external trims from  $-55^{\circ}\text{C}$  to  $+125^{\circ}\text{C}$ .
2. Since the laser trimming is done on the wafer prior to separation into individual chips, the AD581 will be extremely valuable to hybrid designers for its ease of use, lack of required external trims, and inherent high performance.
3. The AD581 can also be operated in a two-terminal "Zener" mode to provide a precision negative 10 volt reference with just one external resistor to the unregulated supply. The performance in this mode is nearly equal to that of the standard three-terminal configuration.
4. Advanced circuit design using the band-gap concept allows the AD581 to give full performance with an unregulated input voltage down to 13 volts. With an external resistor, the device will operate with a supply as low as 11.4 volts.

**SPECIFICATIONS** (@  $V_{IN} = +15\text{V}$  and  $25^{\circ}\text{C}$ )

Model	AD581J			AD581K			AD581L			Units
	Min	Typ	Max	Min	Typ	Max	Min	Typ	Max	
OUTPUT VOLTAGE TOLERANCE (Error from nominal 10,000V output)	$\pm 30$			$\pm 10$			$\pm 5$			mV
OUTPUT VOLTAGE CHANGE Maximum Deviation from $+25^{\circ}\text{C}$ Value, $T_{min}$ to $T_{max}$ (Temperature Coefficient)	$\pm 13.5$ 30			$\pm 4.75$ 15			$\pm 2.25$ 5			mV ppm/ $^{\circ}\text{C}$
LINE REGULATION $15\text{V} \leq V_{IN} \leq 30\text{V}$  $13\text{V} \leq V_{IN} \leq 15\text{V}$	3.0 (0.002) 1.0 (0.005)			3.0 (0.002) 1.0 (0.005)			3.0 (0.002) 1.0 (0.005)			mV %/V mV %/V
LOAD REGULATION $0 \leq I_{OUT} \leq 5\text{mA}$	200	500		200	500		200	500		$\mu\text{V}/\text{mA}$
QUIESCENT CURRENT	0.75	1.0		0.75	1.0		0.75	1.0		mA
TURN-ON SETTLING TIME TO 0.1%	200			200			200			$\mu\text{s}$
NOISE (0.1 to 10Hz)	50			50			50			$\mu\text{V}/\text{p-p}$
LONG-TERM STABILITY	25			25			25			ppm/1000 hrs.
SHORT-CIRCUIT CURRENT	30			30			30			mA
OUTPUT CURRENT Source $I_{OUT} + 25^{\circ}\text{C}$ Source $T_{min}$ to $T_{max}$ Sink $T_{min}$ to $T_{max}$ Sink $-55^{\circ}\text{C}$ to $+85^{\circ}\text{C}$	10 5 5 -			10 5 5 -			10 5 5 -			mA mA mA mA
TEMPERATURE RANGE Specified Operating	0 -65	+70 +150		0 -65	+70 +150		0 -65	+70 +150		$^{\circ}\text{C}$ $^{\circ}\text{C}$
PACKAGE OPTION <sup>1</sup> TO-5 (H-03B)	AD581JH			AD581KH			AD581LH			

Model	AD581S			AD581T			AD581U			Units
	Min	Typ	Max	Min	Typ	Max	Min	Typ	Max	
OUTPUT VOLTAGE TOLERANCE (Error from nominal 10,000V output)	$\pm 30$			$\pm 10$			$\pm 5$			mV
OUTPUT VOLTAGE CHANGE Maximum Deviation from $+25^{\circ}\text{C}$ Value, $T_{min}$ to $T_{max}$ (Temperature Coefficient)	$\pm 30$ 30			$\pm 15$ 15			$\pm 10$ 10			mV ppm/ $^{\circ}\text{C}$
LINE REGULATION $15\text{V} \leq V_{IN} \leq 30\text{V}$  $13\text{V} \leq V_{IN} \leq 15\text{V}$	3.0 (0.002) 1.0 (0.005)			3.0 (0.002) 1.0 (0.005)			3.0 (0.002) 1.0 (0.005)			mV %/V mV %/V
LOAD REGULATION $0 \leq I_{OUT} \leq 5\text{mA}$	200	500		200	500		200	500		$\mu\text{V}/\text{mA}$
QUIESCENT CURRENT	0.75	1.0		0.75	1.0		0.75	1.0		mA
TURN-ON SETTLING TIME TO 0.1%	200			200			200			$\mu\text{s}$
NOISE (0.1 to 10Hz)	50			50			50			$\mu\text{V}/\text{p-p}$
LONG-TERM STABILITY	25			25			25			ppm/1000 hrs.
SHORT-CIRCUIT CURRENT	30			30			30			mA
OUTPUT CURRENT Source $I_{OUT} + 25^{\circ}\text{C}$ Source $T_{min}$ to $T_{max}$ Sink $T_{min}$ to $T_{max}$ Sink $-55^{\circ}\text{C}$ to $+85^{\circ}\text{C}$	10 5 200 5			10 5 200 5			10 5 200 5			mA mA mA mA
TEMPERATURE RANGE Specified Operating	55 65	+125 +150		55 65	+125 +150		55 65	+125 +150		$^{\circ}\text{C}$ $^{\circ}\text{C}$
PACKAGE OPTION <sup>2</sup> TO-5 (H-03B)	AD581SH			AD581TH			AD581UH			

NOTES  
<sup>1</sup>See Figure 7  
<sup>2</sup>See Section 13 for package outline information.  
Specifications subject to change without notice.

Specifications shown in boldface are tested on all production units at final electrical test. Results from those tests are used to calculate outgoing quality levels. All min and max specifications are guaranteed, although only those shown in boldface are tested on all production units.

**ABSOLUTE MAX RATINGS**

Input Voltage $V_{IN}$ to Ground	40V
Power Dissipation ( $I_{OUT} + 25^{\circ}\text{C}$ )	600mW
Operating Junction Temperature Range	$-55^{\circ}\text{C}$ to $+150^{\circ}\text{C}$
Lead Temperature (Soldering 10sec)	$+300^{\circ}\text{C}$
Thermal Resistance Junction-to-Ambient	150 $^{\circ}\text{C}/\text{W}$

## VOLTAGE VARIATION vs. TEMPERATURE

Some confusion exists in the area of defining and specifying reference voltage error over temperature. Historically, references have been characterized using a maximum deviation per degree Centigrade; i.e., 10ppm/°C. However, because of non-linearities in temperature characteristics, which originated in standard Zener references (such as "S" type characteristics) most manufacturers have begun to use a maximum limit error band approach to specify devices. This technique involves measurement of the output at 3, 5 or more different temperatures to guarantee that the output voltage will fall within the given error band. The temperature characteristic of the AD581 consistently follows the S-curve shown in Figure 4. Five-point measurement of each device guarantees the error band over the -55°C to +125°C range; three-point measurement guarantees the error band from 0 to +70°C.

The error band which is guaranteed with the AD581 is the maximum deviation from the initial value at +25°C; this error band is of more use to a designer than one which simply guarantees the maximum total change over the entire range (i.e., in the latter definition, all of the changes could occur in the positive direction). Thus, with a given grade of the AD581, the designer can easily determine the maximum total error from initial tolerance plus temperature variation (e.g., for the AD581T, the initial tolerance is ±10mV, the temperature error band is ±15mV, thus the unit is guaranteed to be 10.000 volts ±25mV from -55°C to +125°C).

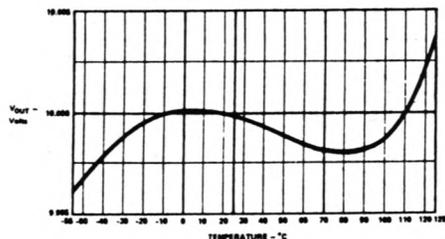


Figure 4. Typical Temperature Characteristic

## OUTPUT CURRENT CHARACTERISTICS

The AD581 has the capability to either source or sink current and provide good load regulation in either direction, although it has better characteristics in the source mode (positive current into the load). The circuit is protected for shorts to either positive supply or ground. The output voltage vs. output current characteristics of the device are shown in Figure 5. Source current is displayed as negative current in the figure; sink current is displayed as positive current in the figure; sink cur-

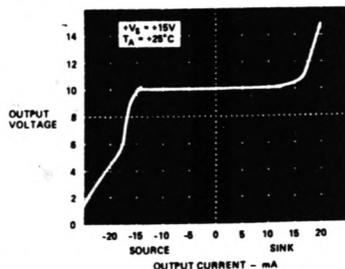


Figure 5. AD581 Output Voltage vs. Sink and Source Current

rent is positive. Note that the short circuit current (i.e., zero volts output) is about 28mA; when shorted to +15 volts, the sink current goes to about 20mA.

## DYNAMIC PERFORMANCE

Many low power instrument manufacturers are becoming increasingly concerned with the turn-on characteristics of the components being used in their systems. Fast turn-on components often enable the end user to keep power off when not needed, and yet respond quickly when the power is turned on for operation. Figure 6 displays the turn-on characteristic of the AD581. This characteristic is generated from cold-start operation and represents the true turn-on waveform after an extended period with the supplies off. The figure shows both the coarse and fine transient characteristics of the device; the total settling time to within ±1 millivolt is about 180µs, and there is no long thermal tail appearing after the point.



Figure 6. Output Settling Characteristic

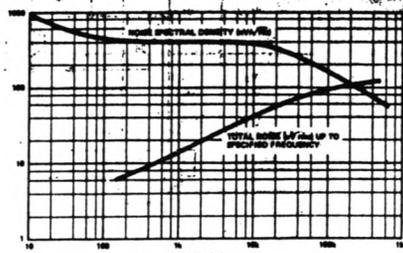


Figure 7. Spectral Noise Density and Total rms Noise vs. Frequency

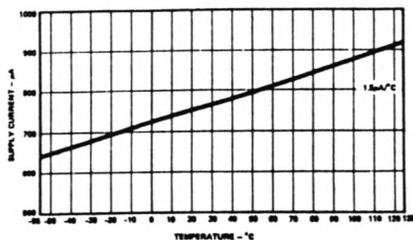


Figure 8. Quiescent Current vs. Temperature

## APPLYING THE AD581

The AD581 is easy to use in virtually all precision reference applications. The three terminals are simply primary supply, ground, and output, with the case grounded. No external components are required even for high precision applications; the degree of desired absolute accuracy is achieved simply by selecting the required device grade. The AD581 requires less than 1mA quiescent current from an operating supply range of 12 to 30 volts.

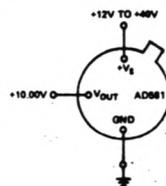


Figure 1. AD581 Pin Configuration (Top View)

An external fine trim may be desired to set the output level to exactly 10.000 volts within less than a millivolt (calibrated to a main system reference). System calibration may also require a reference slightly different from 10.00 volts. In either case, the optional trim circuit shown in Figure 2 can offset the output by up to ±30 millivolts (with the 22Ω resistor), if needed, with minimal effect on other device characteristics.

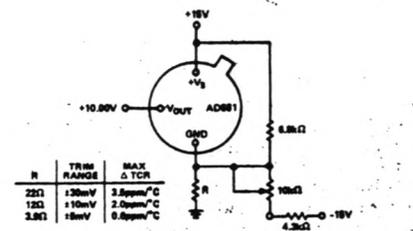


Figure 2. Optional Fine Trim Configuration

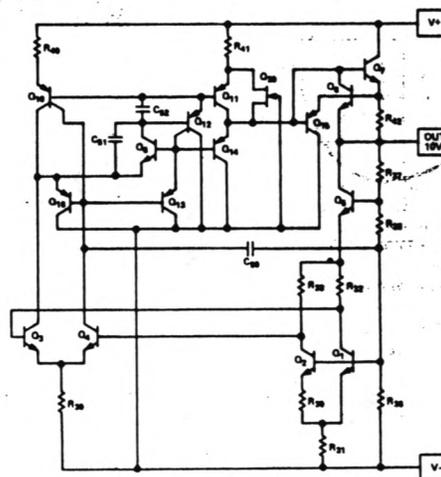


Figure 3. Simplified Schematic

### PRECISION HIGH CURRENT SUPPLY

The AD581 can be easily connected with power pnp or power darlington pnp devices to provide much greater output current capability. The circuit shown in Figure 9 delivers a precision 10 volt output with up to 4 amperes supplied to the load. The 0.1 $\mu$ F capacitor is required only if the load has a significant capacitive component. If the load is purely resistive, improved high frequency supply rejection results from removing the capacitor.

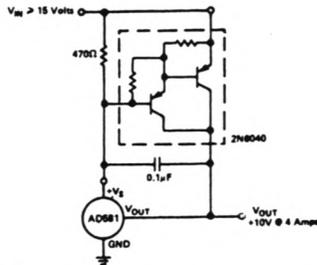


Figure 9. High Current Precision Supply

### CONNECTION FOR REDUCED PRIMARY SUPPLY

While line regulation is specified down to 13 volts, the typical AD581 will work as specified down to 12 volts or below. The current sink capability allows even lower supply voltage capability such as operation from 12V  $\pm$ 5% as shown in Figure 10. The 560 $\Omega$  resistor reduces the current supplied by the AD581 to a manageable level at full 5mA load. Note that the other bandgap references, without current sink capability, may be damaged by use in this circuit configuration.

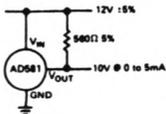


Figure 10. 12-Volt Supply Connection

### THE AD581 AS A CURRENT LIMITER

The AD581 represents an alternative to current limiter diodes which require factory selection to achieve a desired current. This approach often results in temperature coefficients of 1%/ $^{\circ}$ C. The AD581 approach is not limited to a defined set current limit; it can be programmed from 0.75 to 5mA with the insertion of a single external resistor. Of course, the minimum voltage required to drive the connection is 13 volts. The AD580, which is a 2.5 volt reference, can be used in this type of circuit with compliance voltage down to 4.5 volts.

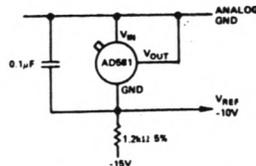


Figure 12. Two-Terminal -10 Volt Reference

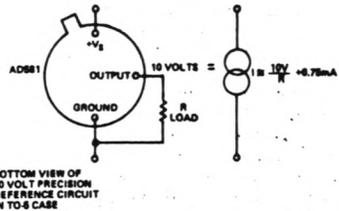


Figure 11. A Two-Component Precision Current Limiter

### NEGATIVE 10-VOLT REFERENCE

The AD581 can also be used in a two-terminal "Zener" mode to provide a precision -10.00 volt reference. As shown in Figure 13, the  $V_{IN}$  and  $V_{OUT}$  terminals are connected together to the high supply (in this case, ground). The ground pin is connected through a resistor to the negative supply. The output is now taken from the ground pin instead of  $V_{OUT}$ . With 1mA flowing through the AD581 in this mode, a typical unit will show a 2mV increase in output level over that produced in the three-terminal mode. Note also that the effective output impedance in this connection increases from 0.2 $\Omega$  typical to 2 ohms. It is essential to arrange the output load and the supply resistor,  $R_S$ , so that the net current through the AD581 is always between 1 and 5mA. The temperature characteristics and long-term stability of the device will be essentially the same as that of a unit used in the standard three-terminal mode. The operating temperature range is limited to -55 $^{\circ}$ C to +85 $^{\circ}$ C.

The AD581 can also be used in a two-terminal mode to develop a positive reference.  $V_{IN}$  and  $V_{OUT}$  are tied together and to the positive supply through an appropriate supply resistor. The performance characteristics will be similar to those of the negative two-terminal connection. The only advantage of this connection over the standard three-terminal connection is that a lower primary supply can be used, as low as 10.5 volts. This type of operation will require considerable attention to load and primary supply regulation to be sure the AD581 always remains within its regulating range of 1 to 5mA.

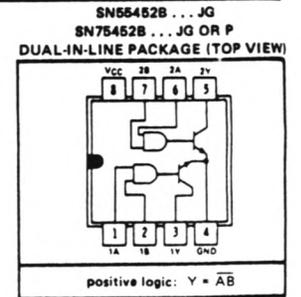
## TYPES SN55452B, SN75452B DUAL PERIPHERAL POSITIVE-NAND DRIVERS

logic

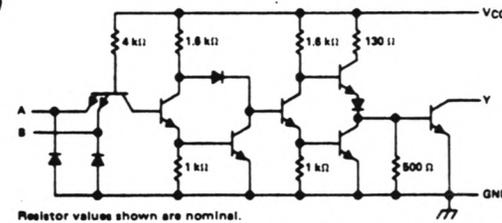
### FUNCTION TABLE (EACH DRIVER)

A	B	Y
L	L	H (off state)
L	H	H (off state)
H	L	H (off state)
H	H	L (on state)

H = high level, L = low level



schematic (each driver)



electrical characteristics over recommended operating free-air temperature range (unless otherwise noted)

PARAMETER	TEST CONDITIONS	SN55452B		SN75452B		UNIT
		MIN	TYP <sup>1</sup> MAX	MIN	TYP <sup>2</sup> MAX	
$V_{IH}$	High-level input voltage	2		2		V
$V_{IL}$	Low-level input voltage	0.8		0.8		V
$V_{IK}$	Input clamp voltage	-1.2 -1.5		-1.2 -1.5		V
$I_{OH}$	High-level output current	300		100		$\mu$ A
$V_{OL}$	Low-level output voltage	$V_{CC} = \text{MIN}$ , $V_{IH} = 2\text{V}$ , $I_{OL} = 100\text{mA}$		0.26	0.5	V
		$V_{CC} = \text{MAX}$ , $V_{IH} = 2\text{V}$ , $I_{OL} = 300\text{mA}$		0.5	0.8	
$I_I$	Input current at maximum input voltage	$V_{CC} = \text{MAX}$ , $V_I = 5.5\text{V}$		1		1 mA
$I_{IH}$	High-level input current	$V_{CC} = \text{MAX}$ , $V_I = 2.4\text{V}$		40		40 $\mu$ A
$I_{IL}$	Low-level input current	$V_{CC} = \text{MAX}$ , $V_I = 0.4\text{V}$		-1.1	-1.5	-1.1 -1.5 mA
$I_{CCH}$	Supply current, outputs high	$V_{CC} = \text{MAX}$ , $V_I = 0\text{V}$		11	14	11 14 mA
$I_{CCL}$	Supply current, outputs low	$V_{CC} = \text{MAX}$ , $V_I = 5\text{V}$		56	71	56 71 mA

<sup>1</sup>For conditions shown as MIN or MAX, use the appropriate value specified under recommended operating conditions.

<sup>2</sup>All typical values are at  $V_{CC} = 5\text{V}$ ,  $T_A = 25^{\circ}\text{C}$ .

switching characteristics,  $V_{CC} = 5\text{V}$ ,  $T_A = 25^{\circ}\text{C}$

PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
$t_{PLH}$	Propagation delay time, low-to-high-level output	26		35	ns
$t_{PHL}$	Propagation delay time, high-to-low-level output	24		35	ns
$t_{TLH}$	Transition time, low-to-high-level output	5		8	ns
$t_{THL}$	Transition time, high-to-low-level output	7		12	ns
$V_{OH}$	High-level output voltage after switching	$V_S = 20\text{V}$ , See Figure 4		$V_S - 6.5$	mV



## Voltage Comparators

### LM139/ 239/ 339, LM139A/239A/339A, LM2901, LM3302 Low Power Low Offset Voltage Quad Comparators General Description

The LM139 series consists of four independent precision voltage comparators with an offset voltage specification as low as 2 mV max for all four comparators. These were designed specifically to operate from a single power supply over a wide range of voltages. Operation from split power supplies is also possible and the low power supply current drain is independent of the magnitude of the power supply voltage. These comparators also have a unique characteristic in that the input common-mode voltage range includes ground, even though operated from a single power supply voltage.

Application areas include limit comparators, simple analog to digital converters; pulse, squarewave and time delay generators; wide range VCO; MOS clock timers; multivibrators and high voltage digital logic gates. The LM139 series was designed to directly interface with TTL and CMOS. When operated from both plus and minus power supplies, they will directly interface with MOS logic—where the low power drain of the LM339 is a distinct advantage over standard comparators.

#### Advantages

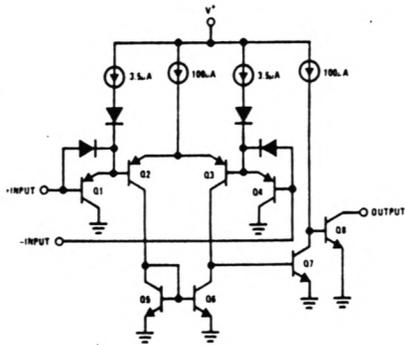
- High precision comparators
- Reduced  $V_{OS}$  drift over temperature

- Eliminates need for dual supplies
- Allows sensing near gnd
- Compatible with all forms of logic
- Power drain suitable for battery operation

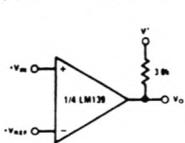
#### Features

- Wide single supply voltage range or dual supplies  
LM139 series,  $2 V_{DC}$  to  $36 V_{DC}$  or  
LM139A series, LM2901  $\pm 1 V_{DC}$  to  $\pm 18 V_{DC}$   
LM3302  $2 V_{DC}$  to  $28 V_{DC}$   
or  $\pm 1 V_{DC}$  to  $\pm 14 V_{DC}$
- Very low supply current drain (0.8 mA) — independent of supply voltage (2 mW/comparator at  $+5 V_{DC}$ )
- Low input biasing current  $25 \text{ nA}$
- Low input offset current  $\pm 5 \text{ nA}$   
and offset voltage  $\pm 3 \text{ mV}$
- Input common-mode voltage range includes gnd
- Differential input voltage range equal to the power supply voltage
- Low output saturation voltage  $250 \text{ mV}$  at  $4 \text{ mA}$
- Output voltage compatible with TTL, DTL, ECL, MOS and CMOS logic systems

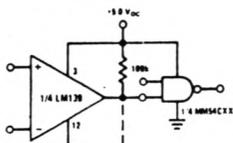
#### Schematic and Connection Diagrams



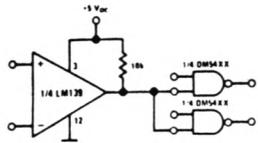
#### Typical Applications ( $V^+ = 5.0 V_{DC}$ )



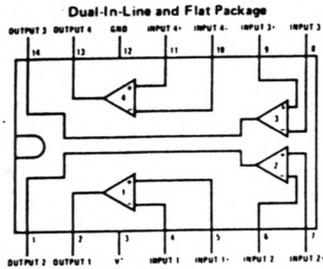
Basic Comparator



Driving CMOS



Driving TTL



Order Number LM139J, LM139AJ,  
LM239J, LM239AJ, LM339J,  
LM339AJ, LM2901J or LM3302J  
See NS Package J14A

Order Number LM339N, LM339AN,  
LM2901N or LM3302N  
See NS Package N14A

#### Electrical Characteristics ( $V^+ = 5 V_{DC}$ , Note 4)

PARAMETER	CONDITIONS	LM139A		LM239A, LM339A		LM139		LM239, LM339		LM2901		LM3302	
		MIN	TYP	MIN	TYP	MIN	TYP	MIN	TYP	MIN	TYP	MIN	TYP
Supply Voltage, $V^+$													
Differential Input Voltage													
Input Voltage													
Power Dissipation (Note 1)													
Molded DIP													
Cavity DIP													
Flat Pack													
Output Short-Circuit to GND, (Note 2)													
Input Current ( $V_{IN} < -0.3 V_{DC}$ , Note 3)													
Operating Temperature Range													
LM339A													
LM239A													
LM2901													
LM139A													
Storage Temperature Range													
Lead Temperature (Soldering, 10 seconds)													

PARAMETER	CONDITIONS	LM139A		LM239A, LM339A		LM139		LM239, LM339		LM2901		LM3302	
		MIN	TYP	MIN	TYP	MIN	TYP	MIN	TYP	MIN	TYP	MIN	TYP
Input Offset Voltage	$T_A = 25^\circ\text{C}$ , (Note 5) $I_{IN(+)}$ or $I_{IN(-)}$ with Output in Linear Range, $T_A = 25^\circ\text{C}$ , (Note 5)	$\pm 1.0$	$\pm 2.0$	$\pm 1.0$	$\pm 2.0$	$\pm 2.0$	$\pm 5.0$	$\pm 2.0$	$\pm 5.0$	$\pm 2.0$	$\pm 7.0$	$\pm 3.0$	$\pm 20$
Input Bias Current		25	100	25	250	25	100	25	250	25	250	25	500
Input Offset Current		$\pm 3.0$	$\pm 25$	$\pm 5.0$	$\pm 50$	$\pm 3.0$	$\pm 25$	$\pm 5.0$	$\pm 50$	$\pm 3.0$	$\pm 25$	$\pm 3.0$	$\pm 100$
Input Common-Mode Voltage Range	$T_A = 25^\circ\text{C}$ , (Note 6) $I_{IN(+)} - I_{IN(-)}$ , $T_A = 25^\circ\text{C}$	0	$V^+ - 1.5$	0	$V^+ - 1.5$	0	$V^+ - 1.5$	0	$V^+ - 1.5$	0	$V^+ - 1.5$	0	$V^+ - 1.5$
Supply Current	$R_L = \infty$ on all Comparators, $T_A = 25^\circ\text{C}$ $R_L = \infty$ , $V^+ = 30V$ , $T_A = 25^\circ\text{C}$ $R_L \geq 15 \text{ k}\Omega$ , $V^+ = 15 V_{DC}$ (To Support Large VO Swing), $T_A = 25^\circ\text{C}$ $V_{IN} = \text{TTL Logic Swing}$ , $V_{REF} =$ $1.4 V_{DC}$ , $V_{RL} = 5 V_{DC}$ , $R_L = 5.1 \text{ k}\Omega$ , $T_A = 25^\circ\text{C}$	0.8	2.0	0.8	2.0	0.8	2.0	0.8	2.0	0.8	2.0	0.8	2
Voltage Gain		200	200	50	200	200	200	200	200	25	100	2	30
Large Signal Response Time		300	300	300	300	300	300	300	300	300	300	300	300
Response Time	$V_{RL} = 5 V_{DC}$ , $R_L = 5.1 \text{ k}\Omega$ , $T_A = 25^\circ\text{C}$	1.3	1.3	1.3	1.3	1.3	1.3	1.3	1.3	1.3	1.3	1.3	1.3
Output Sink Current	$V_{IN(-)} \geq 1 V_{DC}$ , $V_{IN(+)} = 0$ , $V_{O} \leq 1.5 V_{DC}$ , $T_A = 25^\circ\text{C}$	6.0	16	6.0	16	6.0	16	6.0	16	6.0	16	6.0	16
Saturation Voltage	$V_{IN(-)} \geq 1 V_{DC}$ , $V_{IN(+)} = 0$ , $I_{SINK} \leq 4 \text{ mA}$ , $T_A = 25^\circ\text{C}$	250	400	250	400	250	400	250	400	250	400	250	500
Output Leakage Current	$V_{IN(+)} \geq 1 V_{DC}$ , $V_{IN(-)} = 0$ , $V_{O} = 5 V_{DC}$ , $T_A = 25^\circ\text{C}$	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1

Electrical Characteristics (Continued)

PARAMETER	CONDITIONS	LM139A		LM239A, LM339A		LM139		LM239, LM339		LM2901		LM3302		UNITS
		MIN	TYP	MAX	MIN	TYP	MAX	MIN	TYP	MAX	MIN	TYP	MAX	
Input Offset Voltage	(Note 9)	4.0		4.0		9.0		9.0		9		40		mVDC
Input Offset Current	$ I_{IN(+)} - I_{IN(-)} $	$\pm 100$		$\pm 150$		$\pm 100$		$\pm 150$		50		300		nADC
Input Bias Current	$ I_{IN(+)} $ or $ I_{IN(-)} $ with Output in Linear Range	300		400		300		400		200		500		nADC
Input Common-Mode Voltage Range		0	$V^+ - 2.0$	0	$V^+ - 2.0$	0	$V^+ - 2.0$	0	$V^+ - 2.0$	0	$V^+ - 2.0$	0	$V^+ - 2.0$	VDC
Saturation Voltage	$V_{IN(-)} \geq 1 \text{ VDC}; V_{IN(+)} = 0$ $I_{SINK} \leq 4 \text{ mA}$	700		700		700		700		400		700		mVDC
Input Leakage Current	$V_{IN(+)} \geq 1 \text{ VDC}; V_{IN(-)} = 0$ $V_O = 30 \text{ VDC}$	1.0		1.0		1.0		1.0		1.0		1.0		$\mu$ ADC
Differential Input Voltage	Keep all $V_{IN}'s \geq 0 \text{ VDC}$ (or $V^-$ if used). (Note 8)	36		36		36		36		0		36		VDC

Note 1: For operating at high temperatures, the LM339/LM339A, LM2901, LM3302 must be derated based on a 125°C maximum junction temperature and a thermal resistance of 175°C/W which applies for the device soldered in a printed circuit board, operating in a still air ambient. The LM239 and LM139 must be derated based on a 150°C maximum junction temperature. The low bias dissipation and the "ON-OFF" characteristic of the outputs keeps the chip dissipation very small (PD  $\leq 100 \text{ mW}$ ), provided the output transistors are allowed to saturate.

Note 2: Short circuits from the output to  $V^+$  can cause excessive heating and eventual destruction. The maximum output current is approximately 20 mA independent of the magnitude of  $V^+$ .

Note 3: This input current will only exist when the voltage at any of the input leads is driven negative. It is due to the collector-base junction of the input PNP transistors becoming forward biased and thereby acting as input diode clamps. In addition to this diode action, there is also lateral NPN parasitic transistor action on the IC chip. This transistor action can cause the output voltages of the comparators to go to the  $V^-$  voltage level (or to ground for a large overdrive) for the time duration that an input is driven negative. This is not destructive and normal output states will re-establish when the input voltage, which was negative, again returns to a value greater than  $-0.3 \text{ VDC}$  (at 25°C).

Note 4: These specifications apply for  $V^+ = 5 \text{ VDC}$  and  $-65^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$ , unless otherwise stated. With the LM239/LM239A, all temperature specifications are limited to  $-25^\circ\text{C} \leq T_A \leq +85^\circ\text{C}$ . The LM339/LM339A temperature specifications are limited to  $0^\circ\text{C} \leq T_A \leq +70^\circ\text{C}$  and the LM2901, LM3302 temperature range is  $-40^\circ\text{C} \leq T_A \leq +85^\circ\text{C}$ .

Note 5: The direction of the input current is out of the IC due to the PNP input stage. This current is essentially constant, independent of the state of the output so no loading change exists on the reference or input lines.

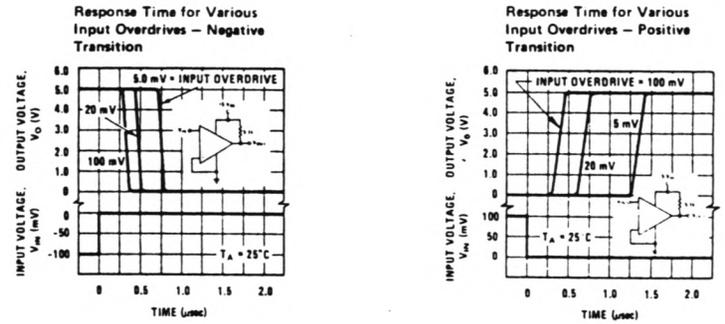
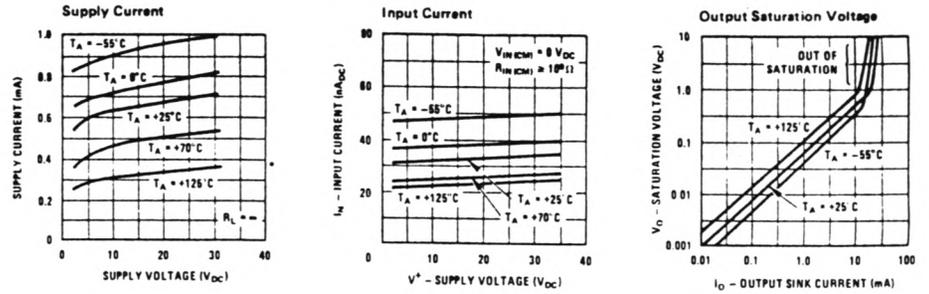
Note 6: The input common-mode voltage or either input signal voltage should not be allowed to go negative by more than 0.3V. The upper end of the common-mode voltage range is  $V^- - 1.5\text{V}$ , but either or both inputs can go to +30 VDC without damage (25V for LM3302).

Note 7: The response time specified is a 100 mV input step with 5 mV overdrive. For larger overdrive signals 300 ns can be obtained, see typical performance characteristics section.

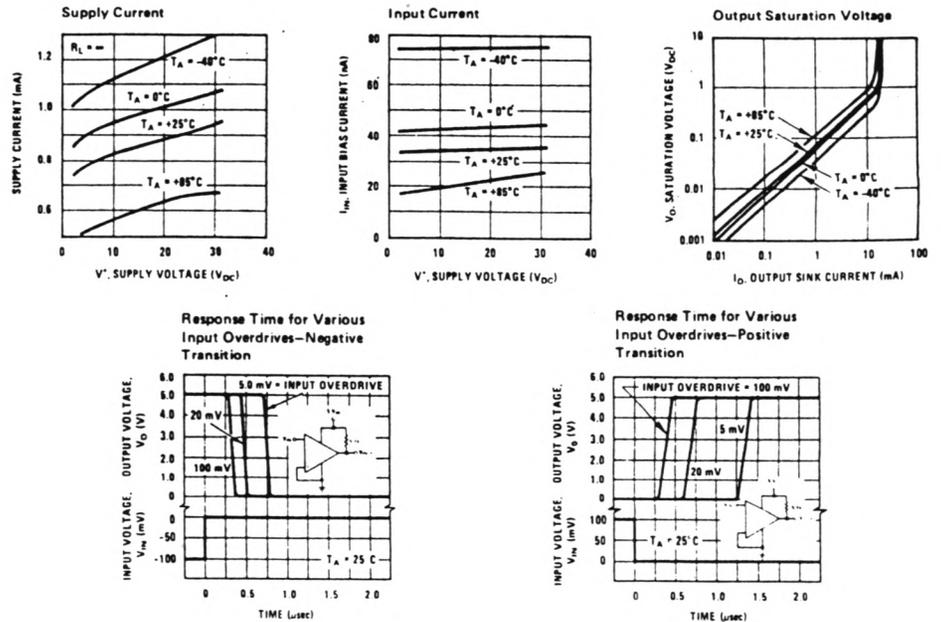
Note 8: Positive excursion of input voltage may exceed the power supply level. As long as the other voltage remains within the common-mode range, the comparator will provide a proper output state. The low input voltage state must not be less than  $-0.3 \text{ VDC}$  (or 0.3 VDC below the magnitude of the negative power supply, if used) (at 25°C).

Note 9: At output switch point,  $V_O \approx 1.4 \text{ VDC}$ ;  $R_S = 0\Omega$  with  $V^+$  from 5 VDC and over the full input common-mode range (0 VDC to  $V^- - 1.5 \text{ VDC}$ ).

Typical Performance Characteristics LM139/LM239/LM339, LM139A/LM239A/LM339A, LM3302



Typical Performance Characteristics LM2901





# TELEDYNE SOLID STATE

## SERENDIP® AC SOLID STATE RELAY

OPTICALLY ISOLATED  
1.0 A rms

### FEATURES/BENEFITS

- Optical isolation – Isolates control elements from load transients.
- Floating output – Eliminates ground loops and signal ground noise.
- Zero voltage turn on, Zero current turn off – Minimum switching transient noise and extremely low EMI.
- Low off state leakage current – For high off state impedances.
- Switches high and low voltages and currents – Switches voltages from 20 to 250 Vrms Switches currents from 10 to 1000 mArms
- High noise immunity – Control circuit cannot be triggered by output switching noise.
- High dielectric strength – For safety and for protection of control and signal level circuits.
- Meets design requirements of UL, CSA, and VDE 0884– Highest quality for commercial/Industrial part. Approval pending.
- Switches resistive or reactive loads to 0.2 P.F. – Broad Load Switching Capability.

### DESCRIPTION

The C45 Series employs back-to-back photo SCRs and a patented zero crossing circuit. The tight zero switch window ensures reliable transient free switching of AC loads and very low EMI and noise generation. Optical isolation of control from output prevents switching noise from coupling into signal, power and ground distribution systems for noise free power switching. This series of solid state relays will switch from 10 ma to 1.0 amp rms at 280 Vrms. The C45 is packaged in a low profile 16 pin Dual In-Line package for PC mounting with minimum space utilization.

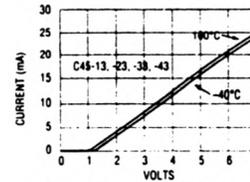
PART NUMBER	RELAY DESCRIPTION
C45	Solid State Relay with Terminals For Through Hole Mount
SC45	Solid State Relay with Terminals For Surface Mount

### ELECTRICAL SPECIFICATIONS (25°C UNLESS OTHERWISE SPECIFIED)

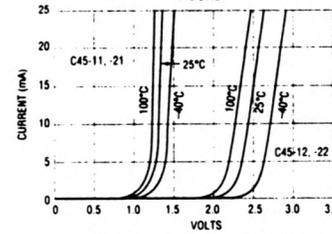
INPUT SPECIFICATIONS (See Figures 1 & 2)		MIN	MAX	UNITS
Input Current (See Note 4)	C45-11, -21	5.0	50.0	ma
	C45-12, -22	10.0	50.0	ma
	C45-13, -23	N/A		
Input Voltage (See Note 4)	C45-11, -21	N/A		
	C45-12, -22	N/A		
	C45-13, -23	3.5	7.0	volts
Turn Off Current	C45-11, -21		10.0	µA
	C45-12, -22			
Turn On Current	C45-11, -21	5.0	50.0	ma
	C45-12, -22	10.0	50.0	ma
Turn Off Voltage	C45-13, -23		0.5	volts
	C45-12, -22			
Turn On Voltage	C45-13, -23	3.5		volts
	C45-12, -22			
Reverse Voltage Protection			-7	volts
OUTPUT SPECIFICATIONS (See Notes 2 & 3)		MIN	MAX	UNITS
Load Current (See Figure 4)		0.01	1.0	Arms
Load Voltage Rating			280	Vrms
Frequency Range		47	650	Hz
On State Voltage Drop at Rated Current			1.5	Vrms
Zero Voltage Turn On			10	Vpeak
Surge Current Rating (non-repetitive 20 ms maximum) (See Figures 3 & Note 1)			8	A
Off State Leakage at Maximum Operating Voltage			1.0	mArms
Turn-On Time			1/2	cycle
Turn-Off Time			1/2	cycle
Over Voltage Rating	C45-11, -12, -13		400	Vpeak
	C45-21, -22, -23		500	Vpeak
Dielectric Strength (Input to Output)		4000		Vrms
Isolation (Input to Output)		10 <sup>8</sup>		Ohms
Capacitance (Input to Output)			10	pF
Off State dv/dt			100	V/µsec
Fusing (RT (1 ms))			5.0	A <sup>2</sup> S
Output SCR's Dissipation Factor			1.0	Watt/A
Output SCR Temperature (T <sub>J</sub> Maximum)			125	°C
Thermal Resistance	θ <sub>JA</sub>		60	°C/W
	θ <sub>JC</sub>		35	°C/W

### SERIES C45

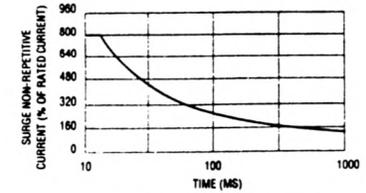
#### CHARACTERISTIC CURVES



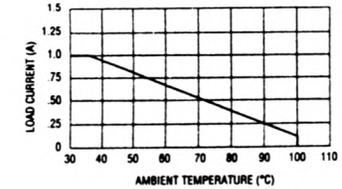
TYPICAL CONTROL CURRENT VS. VOLTAGE  
FIGURE 1



TYPICAL CONTROL CURRENT VS. VOLTAGE  
FIGURE 2

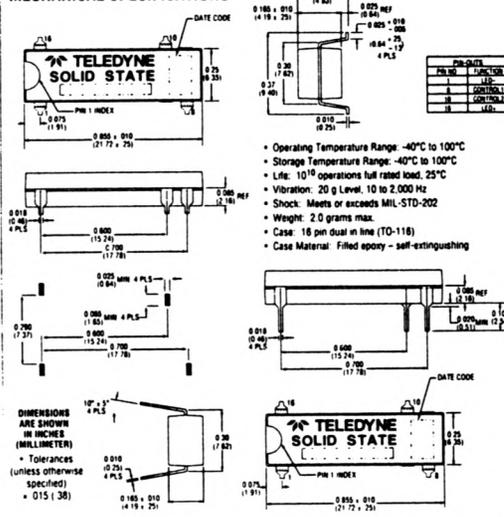


SURGE CURRENT VS. DURATION  
FIGURE 3



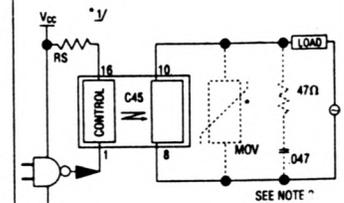
LOAD CURRENT VS. TEMPERATURE  
FIGURE 4

#### MECHANICAL SPECIFICATIONS



- Operating Temperature Range: -40°C to 100°C
- Storage Temperature Range: -40°C to 100°C
- Life: 10<sup>8</sup> operations full rated load, 25°C
- Vibration: 20 g Level, 10 to 2,000 Hz
- Shock: Meets or exceeds MIL-STD-202
- Weight: 2.0 grams max.
- Case: 16 pin dual in line (TO-118)
- Case Material: Filled epoxy - self-extinguishing

#### TYPICAL INTERFACE TO 5V LOGIC (with suggested transient voltage and dv/dt suppression, if required)



\*USE THE TABLE BELOW FOR SELECTION OF PROPER METAL OXIDE VARISTOR (MOV)

MAXIMUM CONTINUOUS LINE VOLTAGE RATING	TRANSIENT (PEAK) RATING OF RELAY	TELEDYNE MOV P/N
140 Vac	400	970-1
250 Vac	600	970-2

(SEE 970 SERIES DATA SHEET FOR FURTHER INFORMATION ON MOV'S)

FIGURE 5

#### NOTES:

- 1 SCR may lose blocking capability during and after surge until T<sub>J</sub> falls below 100°C maximum
- 2 RC snubber is recommended but is not required.
- 3 Minimum Load Power Factor = 0.2 (Capacitive or Inductive). Lower power factors will damage relay
- 4 Operation @ load frequencies above 70 Hz requires increased input signal. Minimum input voltage is 5 Vdc for C45-13, -23. Minimum input current is 7.5 ma for C45-11, -21 and minimum input current is 15 ma for C45-12, -22.

## LM193/LM293/LM393, LM193A/LM293A/LM393A, LM2903

### Low Power Low Offset Voltage Dual Comparators

#### General Description

The LM193 series consists of two independent precision voltage comparators with an offset voltage specification as low as 2.0 mV max for two comparators which were designed specifically to operate from a single power supply over a wide range of voltages. Operation from split power supplies is also possible and the low power supply current drain is independent of the magnitude of the power supply voltage. These comparators also have a unique characteristic in that the input common-mode voltage range includes ground, even though operated from a single power supply voltage.

Application areas include limit comparators, simple analog to digital converters; pulse, squarewave and time delay generators; wide range VCO; MOS clock timers; multivibrators and high voltage digital logic gates. The LM193 series was designed to directly interface with TTL and CMOS. When operated from both plus and minus power supplies, the LM193 series will directly interface with MOS logic where their low power drain is a distinct advantage over standard comparators.

#### Advantages

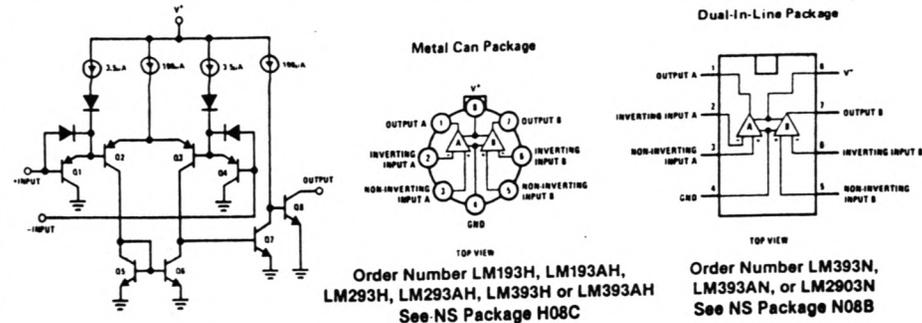
- High precision comparators
- Reduced  $V_{OS}$  drift over temperature

- Eliminates need for dual supplies
- Allows sensing near ground
- Compatible with all forms of logic
- Power drain suitable for battery operation

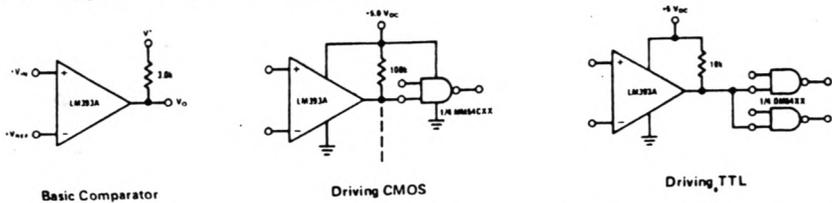
#### Features

- Wide single supply voltage range  
2.0 V<sub>DC</sub> to 36 V<sub>DC</sub>  
or dual supplies  $\pm 1.0$  V<sub>DC</sub> to  $\pm 18$  V<sub>DC</sub>
- Very low supply current drain (0.8 mA)—independent of supply voltage (1.0 mW/comparator at 5.0 V<sub>DC</sub>)
- Low input biasing current 25 nA
- Low input offset current  $\pm 5$  nA  
and maximum offset voltage  $\pm 3$  mV
- Input common-mode voltage range includes ground
- Differential input voltage range equal to the power supply voltage
- Low output saturation voltage 250 mV at 4 mA
- Output voltage compatible with TTL, DTL, ECL, MOS and CMOS logic systems

#### Schematic and Connection Diagrams



#### Typical Applications ( $V^+ = 5.0$ V<sub>DC</sub>)



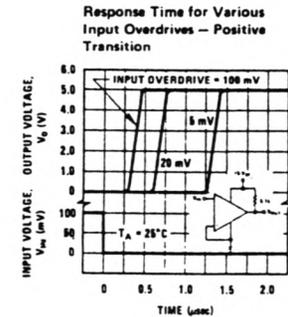
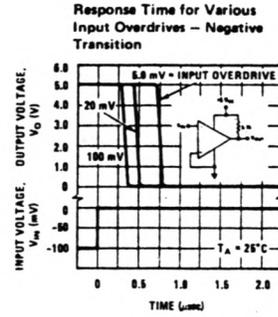
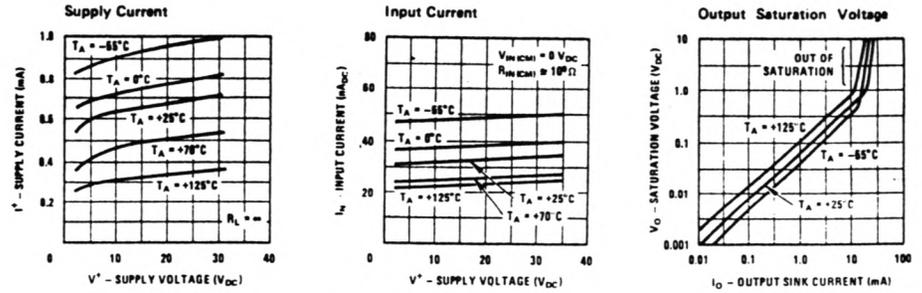
#### Electrical Characteristics ( $V^+ = 5$ V<sub>DC</sub>) (Note 4)

PARAMETER	CONDITIONS	LM193A			LM293A, LM393A			LM193			LM293, LM393			LM2903			UNITS
		MIN	TYP	MAX	MIN	TYP	MAX	MIN	TYP	MAX	MIN	TYP	MAX	MIN	TYP	MAX	
Input Offset Voltage	$T_A = 25^\circ\text{C}$ , (Note 9)	±1.0	±2.0	±2.0	±1.0	±2.0	±2.0	±1.0	±5.0	±1.0	±5.0	±2.0	±7.0	±2.0	±7.0	mV/DC	
Input Bias Current	$I_{IN+}$ or $I_{IN-}$ with Output in Linear Range, $T_A = 25^\circ\text{C}$ , (Note 5)	25	100	250	25	250	250	25	100	25	250	25	250	25	250	nA/DC	
Input Offset Current	$I_{IN+} - I_{IN-}$ , $T_A = 25^\circ\text{C}$	±3.0	±25	±50	±5.0	±50	±50	±3.0	±25	±3.0	±25	±5.0	±50	±5.0	±50	nA/DC	
Input Common-Mode Voltage Range	$T_A = 25^\circ\text{C}$ , (Note 6) $R_L = \infty$ on All Comparators, $T_A = 25^\circ\text{C}$ $R_L = \infty$ on All Amps, $V^+ = 30$ V <sub>DC</sub>	0	0.4	1	0	0.4	1	0	0.4	1	0	0.4	1	0	0.4	1	V/DC
Supply Current	$R_L \geq 15$ k $\Omega$ , $T_A = 25^\circ\text{C}$ , $V^+ = 15$ V <sub>DC</sub> (To Support Large VO Swing)	50	200	50	50	200	50	50	200	50	200	50	200	50	200	mA/DC	
Voltage Gain	$V_{IN} = \text{TTL Logic Swing}$ , $V_{REF} = 1.4$ V <sub>DC</sub> $V_{RL} = 5$ V <sub>DC</sub> , $R_L = 5.1$ k $\Omega$ , $T_A = 25^\circ\text{C}$ $V_{RL} = 5$ V <sub>DC</sub> , $R_L = 5.1$ k $\Omega$ , $T_A = 25^\circ\text{C}$ , (Note 7)	300	300	300	300	300	300	300	300	300	300	300	300	300	300	V/mV	
Large Signal Response Time	$V_{IN} \geq 1$ V <sub>DC</sub> , $V_{IN+} = 0$ , $V_O \leq 1.5$ V <sub>DC</sub> , $T_A = 25^\circ\text{C}$	6.0	16	6.0	6.0	16	6.0	6.0	16	6.0	16	6.0	16	6.0	16	nA/DC	
Response Time	$V_{IN} \geq 1$ V <sub>DC</sub> , $V_{IN+} = 0$ , $I_{SINK} \leq 4$ mA, $T_A = 25^\circ\text{C}$	250	400	250	250	400	250	250	400	250	400	250	400	250	400	$\mu\text{s}$	
Output Sink Current	$V_{IN} = 0$ , $V_{IN+} \geq 1$ V <sub>DC</sub> , $V_O = 5$ V <sub>DC</sub> , $T_A = 25^\circ\text{C}$	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	mA/DC	
Saturation Voltage																mV/DC	
Output Leakage Current																nA/DC	

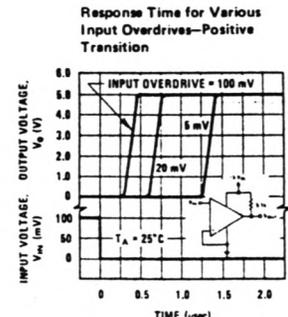
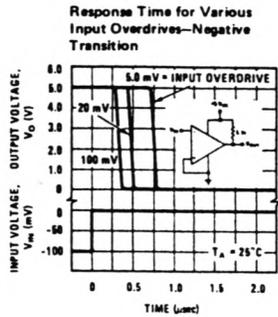
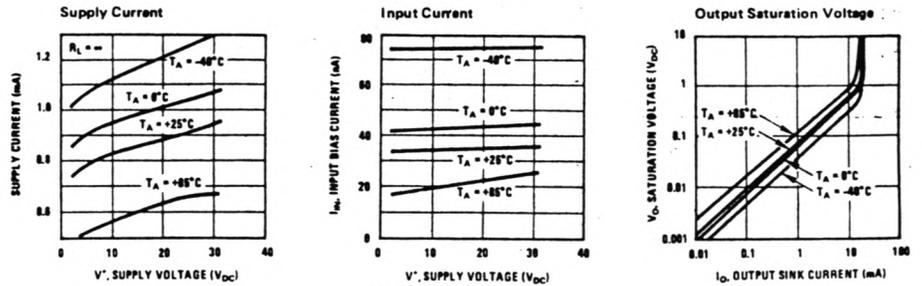
#### Absolute Maximum Ratings

Supply Voltage, $V^+$	36 V <sub>DC</sub> or 18 V <sub>DC</sub>
Differential Input Voltage	36 V <sub>DC</sub>
Input Voltage	-0.3 V <sub>DC</sub> to +36 V <sub>DC</sub>
Power Dissipation (Note 1)	570 mW
Molded Dip	830 mW
Metal Can	Continuous
Output Short-Circuit to Ground, (Note 2)	50 mA
Input Current ( $V_{IN} < -0.3$ V <sub>DC</sub> ), (Note 3)	
Operating Temperature Range	0°C to +70°C
LM293/LM393A	-25°C to +85°C
LM293/LM393A	-55°C to +125°C
LM193/LM193A	-40°C to +85°C
LM2903	-65°C to +150°C
Storage Temperature Range	300°C
Lead Temperature (Soldering, 10 seconds)	

Typical Performance Characteristics LM193/LM293/LM393, LM193A/LM293A/LM393A



Typical Performance Characteristics LM2903



Electrical Characteristics (Continued)

PARAMETER	CONDITIONS	LM193A		LM293A, LM393A		LM193		LM293, LM393		LM2903		UNITS
		MIN	TYP	MIN	TYP	MIN	TYP	MIN	TYP	MIN	TYP	
Input Offset Voltage	(Note 9)		4.0		4.0		9		9		15	mVDC
Input Offset Current	$I_{IN+} - I_{IN-}$		±100		±150		±100		±150		200	nADC
Input Bias Current	$I_{IN+}$ or $I_{IN-}$ with Output in Linear Range		300		400		300		400		500	nADC
Input Common-Mode Voltage Range			$V^+ - 2.0$		$V^+ - 2.0$		$V^+ - 2.0$		$V^+ - 2.0$		$V^+ - 2.0$	VDC
Saturation Voltage			700		700		700		700		700	mVDC
Output Leakage Current			1.0		1.0		1.0		1.0		1.0	µADC
Differential Input Voltage	(Note 8) $V_{IN+} \geq 1 \text{ VDC}$ ; $V_{IN-} = 0$ ; $I_{SINK} \leq 4 \text{ mA}$ . $V_{IN-} = 0$ ; $V_{IN+} \geq 1 \text{ VDC}$ ; $V_O = 30 \text{ VDC}$ . Keep All $V_{INi} \geq 0 \text{ VDC}$ (or $V^-$ , if Used).		36		36		36		36		28	VDC

Note 1: For operating at high temperatures, the LM393/LM393A and LM2903 must be derated based on a 125°C maximum junction temperature and a thermal resistance of 175°C/W which applies for the device soldered in a printed circuit board, operating in a still air ambient. The LM193/LM193A/LM293/LM293A must be derated based on a 150°C maximum junction temperature. The low bias dissipation and the "ON-OFF" characteristic of the outputs keeps the chip dissipation very small ( $P_D \leq 100 \text{ mW}$ ), provided the output transistors are allowed to saturate.

Note 2: Short circuits from the output to  $V^+$  can cause excessive heating and eventual destruction. The maximum output current is approximately 20 mA independent of the magnitude of  $V^+$ .  
Note 3: This input current will only exist when the voltage at any of the input leads is driven negative. It is due to the collector-base junction of the input PNP transistors becoming forward biased and thereby acting as input diode clamps. In addition to this diode action, there is also lateral NPN parasitic transistor action on the IC chip. This transistor action can cause the output voltages of the comparators to go to the  $V^-$  voltage level (or to ground for a large overdrive) for the time duration that an input is driven negative. This is not destructive and normal output states will re-establish when the input voltage, which was negative, again returns to a value greater than  $-0.3 \text{ VDC}$ .

Note 4: These specifications apply for  $V^+ = 5 \text{ VDC}$  and  $-55^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$ , unless otherwise stated. With the LM293/LM293A, all temperature specifications are limited to  $-25^\circ\text{C} \leq T_A \leq +85^\circ\text{C}$  and the LM393/LM393A temperature specifications are limited to  $0^\circ\text{C} \leq T_A \leq +70^\circ\text{C}$ . The LM2903 is limited to  $-40^\circ\text{C} \leq T_A \leq +85^\circ\text{C}$ .

Note 5: The direction of the input current is out of the IC due to the PNP input stage. This current is essentially constant, independent of the state of the output so no loading change exists on the reference or input lines.

Note 6: The input common-mode voltage or either input signal voltage should not be allowed to go negative by more than 0.3V. The upper end of the common-mode voltage range is  $V^+ - 1.5\text{V}$ , but either or both inputs can go to 30 VDC without damage.

Note 7: The response time specified is for a 100 mV input step with 5 mV overdrive. For larger overdrive signals, 300 ns can be obtained, see typical performance characteristics section.

Note 8: Positive excursions of input voltage may exceed the power supply level. As long as the other voltage remains within the common-mode range, the comparator will provide a proper output state. The low input voltage state must not be less than 0.3 VDC (or 0.3 VDC below the magnitude of the negative power supply, if used).

Note 9: At output switch point,  $V_O$  is 1.4 VDC;  $R_S = 0.1 \Omega$  with  $V^-$  from 5 VDC to 30 VDC; and over the full input common-mode range (0 VDC to  $V^+ - 1.5 \text{ VDC}$ ).



# DI CMOS Protected Analog Switches

## AD7510DI/AD7511DI/AD7512DI

### FEATURES

- Latch-Proof
- Overvoltage-Proof:  $\pm 25V$
- Low  $R_{ON}$ :  $75\Omega$
- Low Dissipation:  $3mW$
- TTL/CMOS Direct Interface
- Monolithic Dielectrically Isolated CMOS
- Standard 14/16-pin DIPs and 20-Terminal Surface Mount Packages

### GENERAL DESCRIPTION

The AD7510DI, AD7511DI and AD7512DI are a family of latch-proof dielectrically isolated CMOS switches featuring overvoltage protection up to  $\pm 25V$  above the power supplies. These benefits are obtained without sacrificing the low "ON" resistance ( $75\Omega$ ) or low leakage current ( $500pA$ ), the main features of an analog switch.

The AD7510DI and AD7511DI consist of four independent SPST analog switches packaged in either a 16-pin DIP or a 20-terminal surface mount package. They differ only in that the digital control logic is inverted. The AD7512DI has two independent SPDT switches packaged in either a 14-pin DIP or a 20-terminal surface mount package.

Very low power dissipation, overvoltage protection and TTL/CMOS direct interfacing are achieved by combining a unique circuit design and a dielectrically isolated CMOS process. Silicon nitride passivation ensures long term stability while monolithic construction provides reliability.

### ORDERING INFORMATION<sup>1</sup>

Temperature Range and Package		
0 to +70°C	-25°C to +85°C	-55°C to +125°C
Plastic DIP	Hermetic	Hermetic
AD7510DIJN	AD7510DIJQ	AD7510DISQ
AD7510DIKN	AD7510DIKQ	AD7510DITQ
AD7511DIJN	AD7511DIJQ	AD7511DITQ
AD7511DIKN	AD7511DIKQ	AD7512DISQ
AD7512DIJN	AD7512DIJQ	AD7512DITQ
AD7512DIKN	AD7512DIKQ	
PLCC <sup>2</sup>		LCCC <sup>3</sup>
AD7510DIJP		AD7510DISE
AD7510DIKP		AD7511DISE
AD7511DIJP		AD7511DITE
AD7511DIKP		AD7512DISE
AD7512DIJP		AD7512DITE
AD7512DIKP		

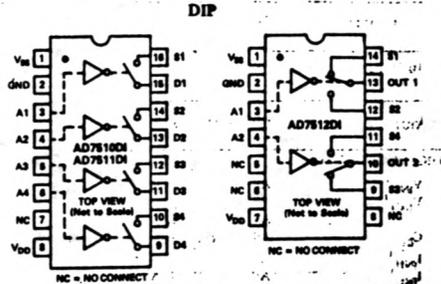
### NOTES

<sup>1</sup>To order MIL-STD-883, Class B processed parts, add/883B to part number. See Analog Devices' 1987 Military Product Databook military data sheet.

<sup>2</sup>PLCC: Plastic Leaded Chip Carrier.

<sup>3</sup>LCCC: Leadless Ceramic Chip Carrier.

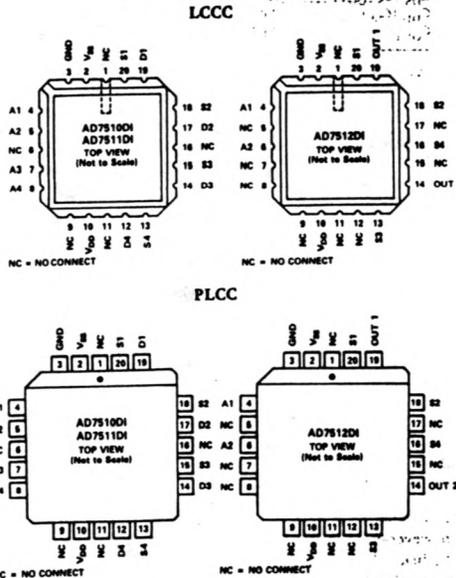
### AD7510DI/AD7511DI/AD7512DI FUNCTIONAL BLOCK DIAGRAMS AND PIN CONFIGURATIONS



### CONTROL LOGIC

- AD7510DI: Switch "ON" for Address "HIGH"
- AD7511DI: Switch "ON" for Address "LOW"
- AD7512DI: Address "HIGH" makes S1 to Out 1 and S3 to Out 2

### PIN CONFIGURATIONS



## SPECIFICATIONS ( $V_{DD} = +15V, V_{SS} = -15V$ unless otherwise noted)

PARAMETER	MODEL	VERSION	COMMERCIAL AND INDUSTRIAL VERSIONS (J, K)		TEST CONDITIONS
			+25°C (N, P, Q, E)	0 to +70°C (N, P) -25°C to +85°C (Q)	
<b>ANALOG SWITCH</b>					
$R_{ON}$	All	J, K	75Ω typ, 100Ω max	175Ω max	$-10V \leq V_D \leq +10V$
$R_{ON}$ vs $V_D$ ( $V_S$ )	All	J, K	20% typ		$I_{DS} = 1.0mA$
$R_{ON}$ Drift	All	J, K	+0.5%/°C typ		$V_D = 0, I_{DS} = 1.0mA$
$R_{ON}$ Match	All	J, K	1% typ		
$R_{ON}$ Drift Match	All	J, K	0.01%/°C typ		
$I_D$ ( $I_S$ )OFF <sup>1</sup>	All	J, K	0.5nA typ, 5nA max	500nA max	$V_D = -10V, V_S = +10V$ and $V_D = +10V, V_S = -10V$
$I_D$ ( $I_S$ )ON <sup>1</sup>	All	J, K	10nA max		$V_S = V_D = +10V$ $V_S = V_D = -10V$
$I_{OUT}$ <sup>1</sup>	AD7512DI	J, K	15nA max	1500nA max	$V_{S1} = V_{OUT} = \pm 10V, V_{S2} = \mp 10V$ and $V_{S2} = V_{OUT} = \pm 10V, V_{S1} = \mp 10V$
<b>DIGITAL CONTROL</b>					
$V_{NH}$ <sup>1</sup>	All	J, K		0.8V max	
$V_{NL}$ <sup>1</sup>	All	J		3.0V min	
	All	K		2.4V min	
$C_{IN}$	All	J, K	7pF typ		
$I_{NH}$ <sup>1</sup>	All	J, K	10nA max		$V_{NH} = V_{DD}$
$I_{NL}$ <sup>1</sup>	All	J, K	10nA max		$V_{NL} = 0$
<b>DYNAMIC CHARACTERISTICS</b>					
$t_{ON}$	AD7510DI	J, K	180ns typ		$V_{NH} = 0$ to +3.0V
	AD7511DI	J, K	350ns typ		
	AD7510DI	J, K	350ns typ		
	AD7511DI	J, K	180ns typ		
$t_{TRANSITION}$	AD7512DI	J, K	300ns typ		
$C_{OFF}$ ( $C_{OFF}$ )	All	J, K	8pF typ		
$C_{ON}$ ( $C_{ON}$ )	All	J, K	17pF typ		
$C_{DS}$ ( $C_{S-OUT}$ )	All	J, K	1pF typ		$V_D$ ( $V_S$ ) = 0V
$C_{DD}$ ( $C_{SS}$ )	All	J, K	0.5pF typ		
$C_{OUT}$	AD7512DI	J, K	17pF typ		
$Q_{NJ}$	All	J, K	30pC typ		Measured at S or D terminal. $C_L = 1000pF, V_{NH} = 0$ to 3V, $V_D$ ( $V_S$ ) = +10V to -10V
<b>POWER SUPPLY</b>					
$I_{DQ}$ <sup>1</sup>	All	J, K	800μA max	800μA max	All digital inputs = $V_{NH}$
$I_{SS}$ <sup>1</sup>	All	J, K	800μA max	800μA max	
$I_{DQ}$ <sup>1</sup>	All	J, K	500μA max	500μA max	All digital inputs = $V_{NL}$
$I_{SS}$ <sup>1</sup>	All	J, K	500μA max	500μA max	
<b>PACKAGE OPTIONS<sup>2</sup></b>					
Plastic (N-14)		AD7512DIJN/KN			
Plastic (N-16)		AD7510DIJN/KN			
		AD7511DIJN/KN			
Cerdip (Q-14)		AD7512DIJQ/KQ			
Cerdip (Q-16)		AD7510DIJQ/KQ			
		AD7511DIJQ/KQ			
PLCC (P-20A)		AD7510DIJP/KP			
		AD7511DIJP/KP			
		AD7512DIJP/KP			

### NOTES

<sup>1</sup>100% tested.  
<sup>2</sup>See Section 13 for package outline information.

Specifications subject to change without notice.

### CAUTION:

ESD (Electro-Static-Discharge) sensitive device. The digital control inputs are diode protected; however, permanent damage may occur on unconnected devices subjected to high energy electrostatic fields. Unused devices must be stored in conductive foam or shunts. The foam should be discharged to the destination socket before devices are removed.



EXTENDED VERSIONS (S, T)

PARAMETER	MODEL	VERSION	+25°C	-55°C to +125°C	TEST CONDITIONS
<b>ANALOG SWITCH</b>					
$R_{ON}^1$	All	S, T	100Ω max	175Ω max	$-10V \leq V_D \leq +10V$ $I_{DS} = 1mA$
$I_D (I_S)_{OFF}^1$	All	S, T	3nA max	200nA max	$V_D = -10V, V_S = +10V$ and $V_D = +10V, V_S = -10V$
$I_D (I_S)_{ON}^1$	All	S, T	10		$V_S = V_D = +10V$ and $V_S = V_D = -10V$
$I_{OUT}^1$	AD7512DI	S, T	9nA max	600nA max	$V_{S1} = V_{OUT} = \pm 10V$ $V_{S2} = \mp 10V$ and $V_{S2} = V_{OUT} = \pm 10V$ $V_{S1} = \mp 10V$
<b>DIGITAL CONTROL</b>					
$V_{INL}^1$	All	S, T		0.8V max	
$V_{INH}^{1,2}$	AD7510DI	S		2.4V min	
	AD7511DI	T		2.4V min	
	AD7512DI	T		2.4V min	
	AD7511DI	S		3.0V min	
	AD7512DI	S		3.0V min	
$I_{IN1}^1$	All	S, T	10nA max		$V_{IN} = V_{DD}$
$I_{INL}^1$	All	S, T	10nA max		$V_{IN} = 0$
<b>DYNAMIC CHARACTERISTICS</b>					
$t_{ON}^3$	AD7510DI	S	1.0μs max		$V_{IN} = 0$ to +3V
	AD7511DI	S, T	1.0μs max		
$t_{OFF}^3$	AD7510DI	S, T	1.0μs max		
	AD7511DI	S, T	1.0μs max		
$t_{TRANSITION}^3$	AD7512DI	S, T	1.0μs max		
<b>POWER SUPPLY</b>					
$I_{DD1}^1$	All	S, T		800μA max	All digital inputs = $V_{INH}$
$I_{SS}^1$	All	S, T		800μA max	
$I_{DD2}^1$	All	S, T		500μA max	All digital inputs = $V_{INL}$
$I_{SS2}^1$	All	S, T		500μA max	
<b>PACKAGE OPTIONS<sup>4</sup></b>					
Cerdip (Q-14)	AD7510DISQ				
Cerdip (Q-16)	AD7511DISQ/TQ				
	AD7512DISQ/TQ				
LCCC (E-20A)	AD7510DISE				
	AD7511DISE/TE				
	AD7512DISE/TE				

NOTES

- <sup>1</sup> 100% tested.
  - <sup>2</sup> A pullup resistor, typically 1-2kΩ is required to make AD7511DISQ and AD7512DISQ TTL compatible.
  - <sup>3</sup> Guaranteed, not production tested.
  - <sup>4</sup> See Section 13 for package outline information.
- Specifications subject to change without notice.

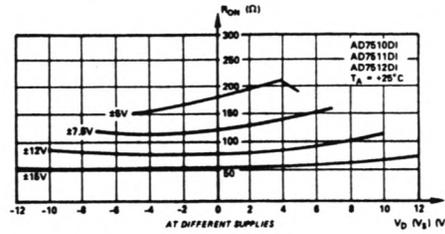
ABSOLUTE MAXIMUM RATINGS\*

$V_{DD}$ to GND	+17V
$V_{SS}$ to GND	-17V
Overvoltage at $V_D (V_S)$	
(1 second surge)	$V_{DD} + 25V$ or $V_{SS} - 25V$
(Continuous)	$V_{DD} + 20V$ or $V_{SS} - 20V$
Switch Current ( $I_{DS}$ , Continuous)	50mA
Switch Current ( $I_{DS}$ , Surge)	
1ms Duration, 10% Duty Cycle	150mA
Digital Input Voltage Range	0V to $V_{DD} + 0.3V$
Power Dissipation (Any Package)	

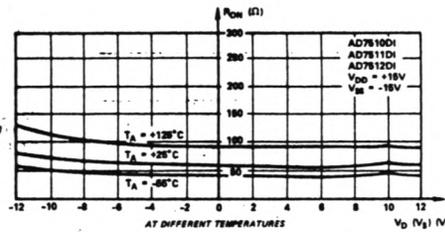
Up to +75°C . . . . . 450mW  
 Derates above +75°C by . . . . . 6mW/°C  
 Lead Temperature (Soldering, 10sec) . . . . . +300°C  
 Storage Temperature . . . . . -65°C to +150°C  
 Operating Temperature  
 Commercial (JN, KN, JP, KP Versions) . . . . . 0 to +70°C  
 Industrial (JQ, KQ Versions) . . . . . -25°C to +85°C  
 Extended (SQ, TQ, SE, TE Versions) . . . . . -55°C to +125°C

\*Stresses above those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. This is a stress rating only and functional operation of the device at these or any other conditions above those indicated in the operational sections of this specification is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

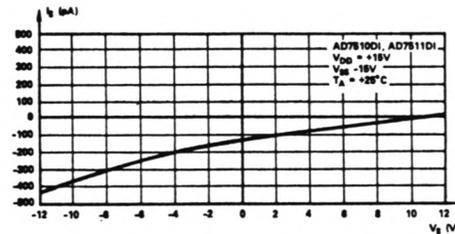
Typical Performance Characteristics



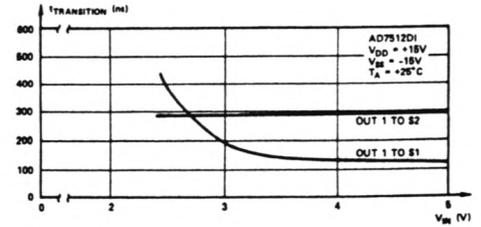
$R_{ON}$  as a Function of  $V_D (V_S)$



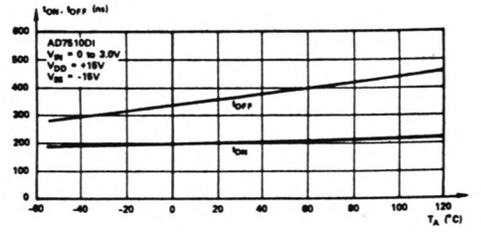
$R_{ON}$  as a Function of  $V_D (V_S)$



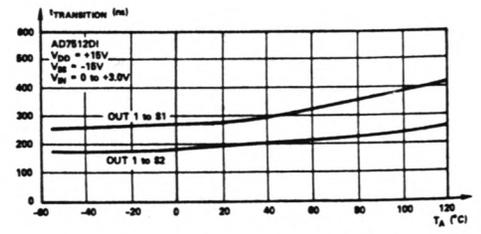
$I_S (I_{DD})_{OFF}$  vs  $V_S$



$t_{TRANSITION}$  as a Function of Digital Input Voltage



$t_{ON}, t_{OFF}$  as a Function of Temperature



$t_{TRANSITION}$  as a Function of Temperature

# LM135/LM235/LM335, LM135A/LM235A/LM335A Precision Temperature Sensors

## General Description

The LM135 series are precision, easily-calibrated, integrated circuit temperature sensors. Operating as a 2-terminal zener, the LM135 has a breakdown voltage directly proportional to absolute temperature at +10 mV/°K. With less than 1Ω dynamic impedance the device operates over a current range of 400 μA to 5 mA with virtually no change in performance. When calibrated at 25°C the LM135 has typically less than 1°C error over a 100°C temperature range. Unlike other sensors the LM135 has a linear output.

Applications for the LM135 include almost any type of temperature sensing over a -55°C to +150°C temperature range. The low impedance and linear output make interfacing to readout or control circuitry especially easy.

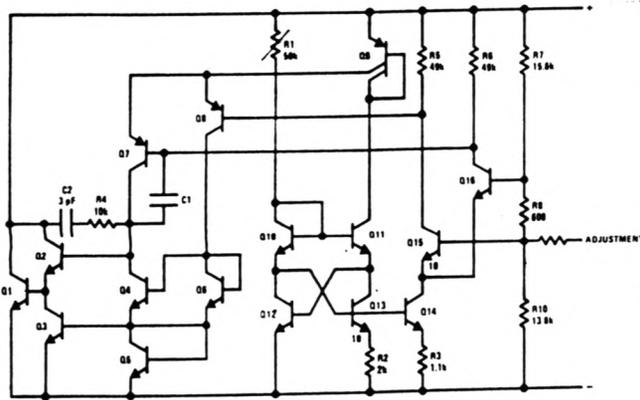
The LM135 operates over a -55°C to +150°C temperature range while the LM235 operates over a -40°C

to +125°C temperature range. The LM335 operates from -40°C to +100°C. The LM135/LM235/LM335 are available packaged in hermetic TO-46 transistor packages while the LM335 is also available in plastic TO-92 packages.

## Features

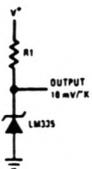
- Directly calibrated in °Kelvin
- 1°C initial accuracy available
- Operates from 400 μA to 5 mA
- Less than 1Ω dynamic impedance
- Easily calibrated
- Wide operating temperature range
- 200°C overrange
- Low cost

## Schematic Diagram

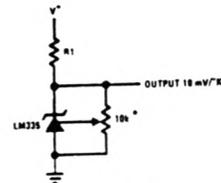


## Typical Applications

Basic Temperature Sensor

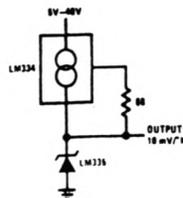


Calibrated Sensor



\* Calibrate for 2.982V at 25°C

Wide Operating Supply



## Absolute Maximum Ratings

Reverse Current	15 mA
Forward Current	10 mA
Storage Temperature	
TO-46 Package	-60°C to +180°C
TO-92 Package	-60°C to +150°C

### Specified Operating Temperature Range

	Continuous	Intermittent (Note 2)
LM135, LM135A	-55°C to +150°C	150°C to 200°C
LM235, LM235A	-40°C to +125°C	125°C to 150°C
LM335, LM335A	-40°C to +100°C	100°C to 125°C
Lead Temperature (Soldering, 10 seconds)		300°C

## Temperature Accuracy LM135/LM235, LM135A/LM235A (Note 1)

PARAMETER	CONDITIONS	LM135A/LM235A			LM135/LM235			UNITS
		MIN	TYP	MAX	MIN	TYP	MAX	
Operating Output Voltage	T <sub>C</sub> = 25°C, I <sub>R</sub> = 1 mA	2.97	2.98	2.99	2.95	2.98	3.01	V
Uncalibrated Temperature Error	T <sub>C</sub> = 25°C, I <sub>R</sub> = 1 mA		0.5	1		1	3	°C
Uncalibrated Temperature Error	T <sub>MIN</sub> < T <sub>C</sub> < T <sub>MAX</sub> , I <sub>R</sub> = 1 mA		1.3	2.7		2	5	°C
Temperature Error with 25°C Calibration	T <sub>MIN</sub> < T <sub>C</sub> < T <sub>MAX</sub> , I <sub>R</sub> = 1 mA		0.3	1		0.5	1.5	°C
Calibrated Error at Extended Temperatures	T <sub>C</sub> = T <sub>MAX</sub> (Intermittent)		2			2		°C
Non-Linearity	I <sub>R</sub> = 1 mA		0.3	0.5		0.3	1	°C

## Temperature Accuracy LM335, LM335A (Note 1)

PARAMETER	CONDITIONS	LM335A			LM335			UNITS
		MIN	TYP	MAX	MIN	TYP	MAX	
Operating Output Voltage	T <sub>C</sub> = 25°C, I <sub>R</sub> = 1 mA	2.95	2.98	3.01	2.92	2.98	3.04	V
Uncalibrated Temperature Error	T <sub>C</sub> = 25°C, I <sub>R</sub> = 1 mA		1	3		2	6	°C
Uncalibrated Temperature Error	T <sub>MIN</sub> < T <sub>C</sub> < T <sub>MAX</sub> , I <sub>R</sub> = 1 mA		2	5		4	9	°C
Temperature Error with 25°C Calibration	T <sub>MIN</sub> < T <sub>C</sub> < T <sub>MAX</sub> , I <sub>R</sub> = 1 mA		0.5	1		1	2	°C
Calibrated Error at Extended Temperatures	T <sub>C</sub> = T <sub>MAX</sub> (Intermittent)		2			2		°C
Non-Linearity	I <sub>R</sub> = 1 mA		0.3	1.5		0.3	1.5	°C

## Electrical Characteristics (Note 1)

PARAMETER	CONDITIONS	LM135/LM235 LM135A/LM235A			LM335 LM335A			UNITS
		MIN	TYP	MAX	MIN	TYP	MAX	
Operating Output Voltage Change with Current	400 μA < I <sub>R</sub> < 5 mA At Constant Temperature		2.5	10		3	14	mV
Dynamic Impedance	I <sub>R</sub> = 1 mA		0.5			0.8		Ω
Output Voltage Temperature Drift			+10			+10		mV/°C
Time Constant	Still Air		80			80		sec
	100 ft/Min Air		10			10		sec
	Stirred Oil		1			1		sec
Time Stability	T <sub>C</sub> = 125°C		0.2			0.2		°C/khr

Note 1: Accuracy measurements are made in a well-stirred oil bath. For other conditions, self heating must be considered.

Note 2: Continuous operation at these temperatures for 10,000 hours for H package and 5,000 hours for Z package may decrease life expectancy of the device.



Precision Monolithics Inc.

# OP-10

DUAL MATCHED INSTRUMENTATION OPERATIONAL AMPLIFIER

## FEATURES

- Extremely Tight Matching
- Excellent Individual Amplifier Parameters
- Offset Voltage Match ..... 0.18mV Max
- Offset Voltage Match vs Temp. .... 0.8μV/°C Max
- Common-Mode Rejection Match ..... 114dB Min
- Power Supply Rejection Match ..... 100dB Min
- Bias Current Match ..... 3.0nA Max
- Low Noise ..... 0.6μV<sub>p-p</sub> Max
- Low Bias Current ..... 3.0nA Max
- High Common-Mode Input Impedance .... 200GΩ Typ
- Excellent Channel Separation ..... 126dB Min

## ORDERING INFORMATION†

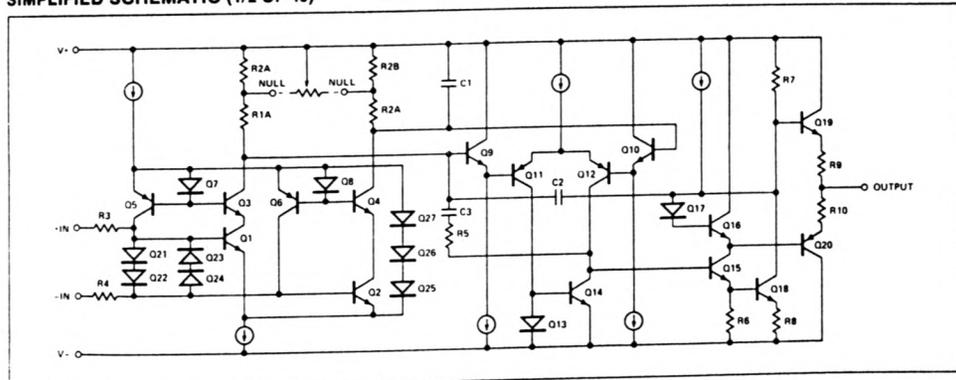
T <sub>A</sub> = 25°C V <sub>OS</sub> MAX (mV)	HERMETIC DIP 14-PIN	OPERATING TEMPERATURE RANGE
0.5	OP10AY*	MIL
0.5	OP10EY	COM
0.5	OP10Y*	MIL
0.5	OP10CY	COM

\* For devices processed in total compliance to MIL-STD-883, add /883 after part number. Consult factory for 883 data sheet.  
† Burn-in is available on commercial and industrial temperature range parts in CerDIP, plastic DIP, and TO-can packages. For ordering information, see 1990/91 Data Book, Section 2.

## GENERAL DESCRIPTION

The OP-10 series of dual-matched instrumentation operational amplifiers consists of two independent monolithic high-performance operational amplifiers in a single 14-pin dual-in-line package. Tight matching of critical parameters

## SIMPLIFIED SCHEMATIC (1/2 OP-10)

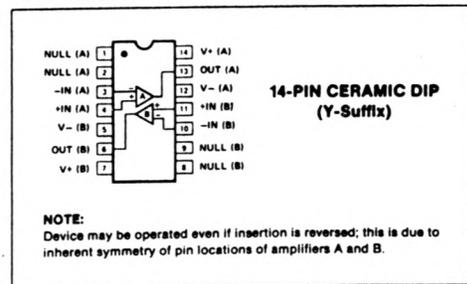


is provided between channels of the dual operational amplifier.

The excellent specifications of the individual amplifiers and tight matching over temperature enable construction of high-performance instrumentation amplifiers. The designer can achieve the guaranteed specifications because the common package eliminates temperature differentials which occur in designs using separately housed amplifiers.

Matching between channels is provided on all critical parameters including offset voltage, tracking of offset voltage vs. temperature, noninverting bias currents, and common-mode and power-supply rejection ratios. The individual amplifiers feature extremely low offset voltage, offset voltage drift, low noise voltage, low bias current, internal compensation and input/output protection.

## PIN CONNECTIONS



OP-10 DUAL MATCHED INSTRUMENTATION OPERATIONAL AMPLIFIER

## ABSOLUTE MAXIMUM RATINGS

Supply Voltage	±22V
Differential Input Voltage	±30V
Input Voltage (Note 1)	±22V
Output Short-Circuit Duration	Indefinite
Storage Temperature Range	-65°C to +150°C
Operating Temperature Range	
OP-10A, OP-10	-55°C to +125°C
OP-10E, OP-10C	0°C to +70°C

DICE Junction Temperature (T<sub>J</sub>) ..... -65°C to +150°C  
Lead Temperature Range (Soldering, 60 sec) ..... +300°C

PACKAGE TYPE	θ <sub>JA</sub> (NOTE 2)	θ <sub>JC</sub>	UNITS
14-Pin Hermetic DIP (Y)	108	16	°C/W

## NOTES:

1. For supply voltages less than +22V, the absolute maximum input voltage is equal to the supply voltage.
2. θ<sub>JA</sub> is specified for worst case mounting conditions, i.e. θ<sub>JA</sub> is specified for device in socket for CerDIP package.

## INDIVIDUAL AMPLIFIER CHARACTERISTICS at V<sub>S</sub> = ±15V, T<sub>A</sub> = 25°C, unless otherwise noted.

PARAMETER	SYMBOL	CONDITIONS	OP-10A			OP-10			UNITS
			MIN	TYP	MAX	MIN	TYP	MAX	
Input Offset Voltage	V <sub>OS</sub>		-	0.2	0.5	-	0.2	0.5	mV
Long-Term Input Offset Voltage Stability	ΔV <sub>OS</sub> /Time	Notes 1, 2	-	0.25	1.0	-	0.25	1.0	μV/Mo
Input Offset Current	I <sub>OS</sub>		-	1.0	2.8	-	1.0	2.8	nA
Input Bias Current	I <sub>B</sub>		-	±1	±3	-	±1	±3	nA
Input Noise Voltage	e <sub>np-p</sub>	Note 2 0.1Hz to 10Hz	-	0.35	0.6	-	0.35	0.6	μV <sub>p-p</sub>
Input Noise Voltage Density	e <sub>n</sub>	Note 2: f <sub>O</sub> = 10Hz f <sub>O</sub> = 100Hz f <sub>O</sub> = 1000Hz	-	10.3	18.0	-	10.3	18.0	nV/√Hz
Input Noise Current	i <sub>np-p</sub>	Note 2: 0.1Hz to 10Hz	-	14	30	-	14	30	pA <sub>p-p</sub>
Input Noise Current Density	i <sub>n</sub>	Note 2: f <sub>O</sub> = 10Hz f <sub>O</sub> = 100Hz f <sub>O</sub> = 1000Hz	-	0.32	0.80	-	0.32	0.80	pA/√Hz
Input Resistance — Differential-Mode	R <sub>IN</sub>	Note 3	20	60	-	20	60	-	MΩ
Input Resistance — Common-Mode	R <sub>INCM</sub>		-	200	-	-	200	-	GΩ
Input Voltage Range	IVR		±13	±14	-	±13	±14	-	V
Common-Mode Rejection Ratio	CMRR	V <sub>CM</sub> = ±13V	110	126	-	110	126	-	dB
Power Supply Rejection Ratio	PSRR	V <sub>S</sub> = ±3V to ±18V	-	4	10	-	4	10	μV/V
Large-Signal Voltage Gain	A <sub>VO</sub>	R <sub>L</sub> ≥ 2kΩ, V <sub>O</sub> = ±10V R <sub>L</sub> ≥ 500Ω, V <sub>O</sub> = ±0.5V, V <sub>S</sub> = ±3V, Note 3	200	500	-	200	500	-	V/mV
Output Voltage Swing	V <sub>O</sub>	R <sub>L</sub> ≥ 10kΩ R <sub>L</sub> ≥ 2kΩ R <sub>L</sub> ≥ 1kΩ	±12.5	±13.0	-	±12.5	±13.0	-	V
Slew Rate	SR	R <sub>L</sub> ≥ 2kΩ	-	0.17	-	-	0.17	-	V/μs
Closed-Loop Bandwidth	BW	A <sub>VCL</sub> = +1.0	-	0.6	-	-	0.6	-	MHz
Open-Loop Output Resistance	R <sub>O</sub>	V <sub>O</sub> = 0, I <sub>O</sub> = 0	-	60	-	-	60	-	Ω
Power Consumption	P <sub>D</sub>	Each Amplifier V <sub>S</sub> = ±3V	-	90	120	-	90	120	mW
Offset Adjustment Range	R <sub>P</sub>	R <sub>P</sub> = 20kΩ	-	±4	-	-	±4	-	mV
Input Capacitance	C <sub>IN</sub>		-	8	-	-	8	-	pF

## NOTES:

1. Long-Term Input Offset Voltage Stability refers to the averaged trend line of V<sub>OS</sub> vs. Time over extended periods after the first 30 days of operation. Excluding the initial hour of operation, changes in V<sub>OS</sub> during the first 30 operating days are typically 2.5μV — refer to typical performance curves
2. Sample tested.
3. Guaranteed by design.



## 5.0 APPENDIX

List of Relevant NRAO Technical Reports and Technical Memoranda.

VLBA Technical Report No. 1, Low-Noise, 8.4 GHz Cryogenic GASFET Front-End, S. Weinreb, H. Dill and R. Harris, August 29, 1984.

Electronics Division Internal Report No. 204, Temperature Readout Unit for Lake Shore Cryotronics Silicon Diode Sensors (DT-500 Series), Michael Balister, May 1980.

Calibration of the vacuum sensors on VLBA and JPL Front-Ends, Harry Dill, Jan 26, 1987. (This memorandum follows this list.)

VLBA Technical Report No. 22, FRONT-END CONTROL MODULE, Module Type F117, Paul Lilie, Larry May and David Weber, January 1993.

VLA Technical Report No. 68, FRONT-END CONTROL INTERFACE, Module Type F14, David Weber, 5/15/1992.

Post-It™ brand fax transmittal memo 7671		# of pages > 3
To	Gerry Petencin	From S. Grayson
Co.		Co.
Dept.		Phone #
Fax #		Fax #

NATIONAL RADIO ASTRONOMY  
Socorro, New Mexico

January 26, 1987

TO: VLBA Front End Maintenance Personnel

FROM: Harry Dill

SUBJECT: Calibration of the vacuum sensors on VLBA and JPL front ends.

TOOLS REQD: Small flat bladed screw driver.

The vacuum sensor circuits in the field have a tendency to drift upward over time. The cause of this is possibly contamination of the thermocouple. The extent of this problem needs to be determined, and can be done by keeping accurate field repair records.

Two circuits exist for sensing vacuum. Vd-dewar vacuum and Vp-pump vacuum. These circuits are on the sensor card, which is the second from the top in the card cage. Each circuit has two potentiometers for setting a zero point and an atmosphere point. These two set points are coupled together so that changing one, will alter the other slightly.

Outlined here is a procedure for calibration of the vacuum sensors in the field. If these do not work, than the unit should be returned to maintenance. When ever this field calibration is performed a proper maintenance report form should be filed. This is the only way that data on this problem can be accumulated.

#### PROCEDURE

- 1) The Vp and Vd thermocouple gauges on the front end will be used as the reference points for ATM and ZERO. For this to work the front end must be cold, T15<25K.
- 2) Note the readings of Vd, Vp, T15, T50, T300 from the readout panel and record them on the maintenance sheet.
- 3) To ensure that the solenoid or the refrigerator will not be disturbed during the calibration process, the AC power plug, connected to J-1, should be connected directly to the refrigerator power receptacle. This removes power to the solenoid, and bypasses the control card for powering the refrigerator.

- 4) Disconnect the vacuum hose from the front end and seal it off at the pump end such that other front ends can use the pump if required. (During the calibration the pump will turn on an off depending the Vd reading.)
- 5) Remove the cover to the card cage (two thumb screws located on either side of the readout panel) and locate the sensor card (second from the top). Then locate four trim pots labeled D ZERO, D ATM, P ZERO and P ATM. Do not turn any other trim pots as they may effect the calibration of the receiver.
- 6) With the Vx, Vx is either Vd or Vp depending upon which circuit is being calibrated, plug connected to the Vp thermocouple the reading for Vx should be 10.0. Turning the multiturn trim pot X ATM, again X is either P or D, should bring the readout to 10.0 if required. Note that the readout takes several seconds to stabilize after turning the trim pot, so turn it slowly.
- 7) Connect the Vx plug to the Vd thermocouple. The reading for Vx should be 0.0. Adjust X ZERO to bring this reading to 0.0 +/- .005.
- 8) Recheck the ATM reading and ZERO reading by repeating steps 6 and 7.
- 9) Reconnect the vacuum line. reconnect plugs Vp and Vd properly. Replace the card cage cover and reconnect the AC power to J-1 and the refrigerator AC power to itself.

## NOTES

- a) A reading of Vd >.400 will activate a pump request. This will be activated at all times unless the front end is commanded to the OFF mode. If the front end is issuing a pump request and is cold and running properly then this indicates that the vacuum sensor has drifted upward.

